UNCLASSIFIED

AD NUMBER

AD029196

CLASSIFICATION CHANGES

TO: unclassified

FROM: confidential

LIMITATION CHANGES

TO:

Approved for public release, distribution unlimited

FROM:

Distribution authorized to U.S. Gov't. agencies and their contractors; Administrative/Operational Use; 23 APR 1954. Other requests shall be referred to National Aeronautics and Space Administration, Washington, DC.

AUTHORITY

NASA TR Server website; NASA TR Server website

Armed Services Technical Information Agency

Because of our limited supply, you are requested to return this copy WHEN IT HAS SERVED YOUR PURPOSE so that it may be made available to other requesters. Your cooperation will be appreciated.

AD

NOTICE: WHEN GOVERNMENT OR OTHER DRAWINGS, SPECIFICATIONS OR OTHER DATA ARE USED FOR ANY PURPOSE OTHER THAN IN CONNECTION WITH A DEFINITELY RELATED GOVERNMENT PROCUREMENT OPERATION, THE U. S. GOVERNMENT THEREBY INCURS NO RESPONSIBILITY, NOR ANY OBLIGATION WHATSOEVER; AND THE FACT THAT THE GOVERNMENT MAY HAVE FORMULATED, FURNISHED, OR IN ANY WAY SUPPLIED THE SAID DRAWINGS, SPECIFICATIONS, OR OTHER DATA IS NOT TO BE REGARDED BY IMPLICATION OR OTHERWISE AS IN ANY MANNER LICENSING THE HOLDER OR ANY OTHER PERSON OR CORPORATION, OR CONVEYING ANY RIGHTS OR PERMISSION TO MANUFACTURE, USE OR SELL ANY PATENTED INVENTION THAT MAY IN ANY WAY BE RELATED THERETO.

Reproduced by DOCUMENT SERVICE CENTER KNOTT BUILDING, DAYTON, 2, 0HIO

NOTICE: THIS DOCUMENT CONTAINS INFORMATION AFFECTING THE NATIONAL DEFENSE OF THE UNITED STATES WITHIN THE MEANING OF THE ESPIONAGE LAWS, TITLE 18, U.S.C., SECTIONS 793 and 794. THE TRANSMISSION OR THE REVELATION OF ITS CONTENTS IN ANY MANNER TO AN UNAUTHORIZED PERSON IS PROHIBITED BY LAW.

FILE COPY

RM A53L29



RESEARCH MEMORANDUM

PRESSURES OF A FOUR-ENGINE TRACTOR AIRPLANE CON-FIGURATION HAVING A WING WITH 40° OF SWEEPBACK By Carl D. Kolbe and Frederick W. Boltz

Ames Aeronautical Laboratory Moffett Field, Calif.

CLASSIFIED DOCUMENT

This material contains information affecting the National Defense of the United States within the meaning of the espionage laws, Title 18, U.S.C., Secs. 798 and 794, the transmission or revelation of which in any meaning of the approximate sense is a substituted by law.

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

WASHINGTON

April 23, 1954

CONFIDENTIAL

54AA-28988

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESEARCH MEMORANDUM

EFFECTS OF OPERATING PROPELLERS ON THE WING-SURFACE

PRESSURES OF A FOUR-ENGINE TRACTOR AIRPLANE CONFIGURATION HAVING A WING WITH 40° OF SWEEPBACK

By Carl D. Kolbe and Frederick W. Boltz

SUMMARY

An investigation has been made to evaluate the effects of operating propellers and of nacelles on the wing-surface pressures on a semispan model of a four-engine tractor airplane configuration having a wing with 40° of sweepback and an aspect ratio of 10. The model represented the right-hand side of the airplane and had single-rotation right-hand propellers. The tests were conducted at Reynolds numbers of 4,000,000 and 8,000,000 at low speed and at Reynolds numbers of 1,000,000 and 2,000,000 for Mach numbers from 0.60 to 0.90.

At high thrust coefficients and a Mach number of 0.082, the propeller slipstream caused large changes in the spanwise distribution of loading over the region of the wing immersed in the propeller slipstream. The strong rotational components within the slipstream were responsible for inflections in the spanwise distribution of loading, there being large increases with increasing thrust coefficient in the normal force of those wing stations behind the up-going propeller blades with relatively small changes for sections behind the down-going blades. Consequently, the center of pressure moved inward with increasing thrust coefficient. At high subsonic Mach numbers, the over-all effects of operating propellers were not large when compared with the low-speed case.

The section data indicate that for most subsonic Mach numbers the addition of the nacelles (propellers removed) caused an increase in the normal-force curve slopes and an increase in the angle of attack for zero section lift.

INTRODUCTION

The aerodynamic problems associated with long-range airplanes designed to fly at high subsonic speeds have been the subject of a series of investigations in the Ames 12-foot pressure wind tunnel. These investigations (refs. 1 to 8) have dealt with the aerodynamic characteristics of several combinations of the components of a hypothetical airplane configuration with a sweptback wing, including the effects of operating propellers on the longitudinal characteristics (refs. 7 and 8). Measurements of the distribution of pressure over the wing have been included in these studies to provide loads data and to facilitate an understanding of the local flow phenomena on the wing. Pressure-distribution data for the wing without nacelles have been presented and analyzed in reference 3.

The present report is concerned with the effects on the wing-surface pressures of operating propellers, as well as the effects of adding nacelles and an extended split flap. The results of pressure-distribution measurements at nine semispan stations of the wing are presented and analyzed in the present report.

NOTATION

- a mean-line designation, fraction of chord over which the design load is uniform
- $\frac{b}{2}$ wing semispan, perpendicular to the plane of symmetry
- b* propeller-blade width
- C_L lift coefficient, $\frac{1ift}{qS}$
- $\Delta C_{\rm L}$ change in lift coefficient
- ΔC_{L_B} change in lift coefficient attributable to the propeller slipstream (based on the total lift of the model with propellers operating less the lift component of the direct propeller force)
- C_m pitching-moment coefficient about quarter point of the mean aerodynamic chord, pitching moment (See fig. 1(a).)
- ΔC_m change in pitching-moment coefficient
- ΔC_{m_S} change in pitching-moment coefficient attributable to the propeller slipstream (based on the total pitching moment of the model with propellers operating less the pitching moment due to the direct propeller force)
- cx longitudinal-force coefficient, parallel to free-stream direction and positive in the dragwise direction, longitudinal force

- c local wing chord, parallel to plane of symmetry
- c' local wing chord, perpendicular to the reference sweep line
- c_{av} average wing chord, parallel to the plane of symmetry, $\frac{2S}{b}$
- mean aerodynamic chord, $\frac{\int_0^{b/2} c^2 dy}{\int_0^{b/2} c dy}$
- c_{l_4} wing-section design lift coefficient
- cm section pitching-moment coefficient, cn (0.25 c.p.)
- c_n section normal-force coefficient, section normal force
- Δc_{n_g} change in section normal-force coefficient attributable to the propeller slipstream
- c.p. section center of pressure
- D propeller diameter
- h maximum thickness of propeller-blade section
- J propeller advance ratio, $\frac{V}{nD}$
- M free-stream Mach number
- n propeller rotational speed
- P pressure coefficient, $\frac{p_1 p}{q}$
- p, local static pressure
- p free-stream static pressure
- q free-stream dynamic pressure
- R Reynolds number, based on the wing mean aerodynamic chord
- R' propeller-tip radius
- r propeller-blade-section radius
- S area of semispan wing
- T thrust per propeller, parallel to air stream

- T_c thrust coefficient per propeller, $\frac{T}{\rho V^2 p^2}$
- t section maximum thickness
- V free-stream velocity
- y lateral distance from the plane of symmetry
- a angle of attack of the wing chord at the plane of symmetry (referred to herein as the wing-root chord)
- angle of attack of the wing-root chord at the plane of symmetry, uncorrected for tunnel-wall interference and angle-of-attack counter correction
- β propeller-blade angle, measured at 0.70 of the tip radius
- β' propeller-blade-section angle
- δ flap angle, measured relative to the local chord in planes normal to the reference sweep line
- angle of twist, measured in planes parallel to the plane of symmetry, positive for washin
- η fraction of semispan, $\frac{2y}{h}$
- $\eta_{c,p}$ spanwise location of the center of pressure, fraction of semispan
- ρ air density

MODEL

The semispan model represented the right-hand side of a hypothetical airplane. The geometry of the model is given in figure 1 and table I. The selection of the geometric properties and the details of the construction of the wing, fuselage, upper-surface fences, nacelles, and flaps have been discussed in references 1 through 4. Four upper-surface wing fences, as shown in figure 1(c), were used throughout the present investigation.

The wing was equipped with nine rows of pressure orifices on both the upper and lower surfaces (fig. 1(c)). The orifices were distributed along the chord from the leading edge to the 95-percent-chord point and were staggered one-eighth inch on either side of the station planes. There were no orifices in the extended trailing-edge flap.

Each propeller in the two different sets used in this investigation had three blades and right-hand rotation. The propellers used for the tests at high subsonic Mach numbers (M = 0.60 and above) were the NACA 1.167-(0)(03)-058 supersonic propellers. For the tests at low subsonic Mach numbers, a thicker propeller, the NACA 1.167-(0)(05)-058, was used to withstand the very high blade loadings that accompany low-speed, high-density, wind-tunnel operation. The characteristics of these propellers and details of the motor-gearbox combination used to drive them are given in reference 6. Blade-form curves of the propellers are presented in figure 2 of this report.

Figure 3 is a photograph of the model mounted in the wind tunnel. The turntable upon which the model was mounted is directly connected to the force-measuring apparatus.

TESTS

The pressure-distribution data presented in this report were obtained simultaneously with the wind-tunnel balance measurements of the total lift, longitudinal force, and pitching moment on the model. Tests were made with the propellers operating and with the propellers removed, covering the range of conditions indicated in table II.

With the propellers operating, the Mach number, Reynolds number, and angle of attack were maintained constant while data were obtained at several selected thrust coefficients, T_c. Selection of the propeller rotational speeds to provide these thrust coefficients was based upon a previous propeller calibration in which the thrust characteristics of the propeller in the presence of the spinner and nacelle forebody were measured for the range of test conditions covered in tests of the complete model (see ref. 6). The results of the calibrations of the two different propellers that are pertinent to this report are presented in figures 4 and 5.

CORRECTIONS

The dynamic pressure, Mach number, and pressure coefficients have been corrected for constriction effects due to the presence of the tunnel walls by the method of reference 9. The force data have been corrected for tunnel-wall-interference effects originating from lift on the model and for drag tares caused by aerodynamic forces on the exposed portion of the turntable on which the model was mounted. The corrections that were applied to data obtained with propellers operating were the same as those reported in references 7 and 8. The corrections used

for the configuration with propellers removed are given in references 2 and 5.

The pressure data and the coefficients derived therefrom are presented in this report for values of uncorrected angle of attack $\alpha_{\rm U}$. The relation between the corrected and uncorrected angle of attack is as follows:

$$\alpha = 0.99 \alpha_0 + \Delta \alpha$$

The constant 0.99 is the ratio between the geometric angle of attack and the uncorrected reading of the angle-of-attack counter. The correction for the tunnel-wall interference is $\Delta \alpha$, and is defined as follows:

$$\Delta \alpha = 0.377 \, C_{Lwing}$$

where

$$C_{Lwing} = C_{Ltotal} - \Delta C_{Lp}$$

and ΔC_{Lp} is the increment of lift coefficient due to propeller thrust and propeller normal force (obtained during the tests reported in ref. 6).

RESULTS AND DISCUSSION

The results of this investigation include a considerable amount of data obtained with the propellers removed, many of which serve as a base for comparison with comparable data obtained with propellers operating. It is convenient, therefore, to defer discussion of the effects of operating propellers until the propellers-off data have been presented and discussed. The latter data include the effects of nacelles and of an extended trailing-edge flap on both the local wing pressures and on the coefficients of lift, drag, and pitching moment.

Tabulated pressure data for nine spanwise stations of the wing (with and without operating propellers) are presented in tables III through XIX. Table II is an index to these data.

A portion of the lift, longitudinal-force, and pitching-moment data at Mach numbers of 0.86 and 0.90 were faired with dotted curves to indicate data obtained under conditions in which the wind tunnel may have been partially choked. It is to be understood that the corresponding pressure data fall within the same limitations of reliability.

Effects of Nacelles (Propellers Off)

Low speed. - The chordwise distributions of pressure coefficient in the region of the nacelles for a Mach number of 0.165 and a Reynolds number of 8,000,000 are compared with those of the wing-fuselage configuration (ref. 3) in figure 6. The corresponding coefficients of section normal force and section pitching moment, and of the total lift, longitudinal force, and pitching moment are presented in figure 7. The data in figure 6 indicate an increase in velocity over the lower surface of those stations in the vicinity of the nacelles. This increase in velocity became smaller with increasing angle of attack. As can be seen in figure 7, these velocity changes contributed to a reduction in the section loading for low angles of attack, an increase in the slopes of the lift and section normal-force curves, and an increase in the angle of attack for zero section lift. References 10 through 12 indicate the same effects for similar configurations. Data obtainable from table XV indicate that this effect diminished toward the wing tip. Further inspection of figure 6 reveals that, with the addition of nacelles to the wing, flow separation occurred on the upper surface at a lower angle of attack, with the attendant decrease in lift-curve slope and increase in drag (fig. 7).

The effect of the nacelles on the spanwise distribution of loading coefficient is shown in figure 8. The general nature of the inflection in the spanwise distribution of loading due to the nacelles is discernible; however, lack of pressure data over the nacelles prevents an accurate estimate of the changes in the location of the spanwise center of pressure. It is apparent, though, that such changes were small.

High speed.— The effects of the nacelles on the over-all force characteristics and section characteristics for Mach numbers ranging from 0.60 to 0.90 and a constant Reynolds number of 2,000,000 are shown in figures 9 through 12, respectively. Cognizance should be taken of the difference in Reynolds number between this and the preceding section. It was noted in reference 3 that for a Mach number of 0.25 the effect of this same change in Reynolds number was not large. A cross plot of the section normal-force data from these figures is presented in figure 13 as a function of Mach number.

In general, the effects of the addition of the nacelles for a Mach number of 0.60 were similar to those at low speed. The effects of increasing Mach number, however, were to reduce slightly the effect of the nacelles on both the section normal-force curve slopes and the angle of attack for zero lift.

Effects of Flaps

The effects of an extended trailing-edge flap ($\delta = 30^{\circ}$) on the over-all force characteristics and on the section characteristics of the wing-fuselage-nacelles combination at a Mach number of 0.082 and a Reynolds number of 4,000,000 are shown in figure 14. Since no pressure measurements were made over the flap itself, estimates of the chordwise pressure distributions, similar to those shown in figure 15, were used to obtain the section coefficients. The effects of the flaps on the spanwise distribution of loading are shown in figure 16. It is evident that the flaps not only caused large increases in normal forces at those sections within the flap span ($\eta = 0.07$ to $\eta = 0.46$) but also caused substantial increases in loading over the outer portion of the wing. The center of pressure obviously moved inward a considerable distance when the flaps were deflected (fig. 16). Reference to figure 14(c) reveals that there was a large rearward movement of the section center of pressure in the region of the flaps. These changes had little effect on the wing pitching moments (fig. 14(a)).

Effects of Operating Propellers

Low speed. - The effects of operating propellers on the chordwise distribution of pressure coefficient in the region of the nacelles at a Mach number of 0.082 and a Reynolds number of 4,000,000 are shown in figure 17. The corresponding over-all force characteristics1 and section characteristics are shown in figure 18. Inspection of the data in figure 17 reveals that at the highest thrust coefficients ($T_c = 0.8$) the pressure distributions changed radically from those which existed with the propellers operating at $T_c = 0$ or with the propellers removed. Furthermore, increasing Tc also caused large changes in the stagnation pressure at the leading edge. Figure 18(b) shows that the propeller slipstreams caused large changes in the section normal-force coefficients and that those changes were not symmetrical over the portion of the wing immersed in the slipstreams as would be expected from simple axial-momentum theory. The asymmetrical effects of the operating propellers are further illustrated in figure 19 wherein the change in section normal-force coefficient due to propellers, $\Delta c_{n_{s}}$, is shown as a function of Tc. It may be seen that there were large increases in Δc_{ns} with increasing T_c at wing stations behind the up-going propeller blades (stations $\eta = 0.19$ and $\eta = 0.44$) at all angles of attack from 40 to 160. At wing stations behind the down-going ¹Cognizance should be taken of the fact that the total force and moment data in this and later similar figures include the effects of the pro-

CONFIDENTIAL

propeller slipstream. (See refs. 7 and 8.)

peller thrust and propeller normal force as well as the effects of the

propeller blades (η = 0.31 and η = 0.56), $\Delta c_{\rm ns}$ decreased with increasing $T_{\rm c}$ at angles of attack below about $8^{\rm o}$ and increased only slightly with increasing $T_{\rm c}$ at higher angles of attack. These effects are indicative of the strong rotational components within the slipstream which change the effective angle of attack of the wing sections immersed in the propeller slipstream.

Figure 20 shows the effect of operating propellers on the spanwise distribution of the loading coefficient $c_n \frac{c}{c_{av}}$ for several angles of attack. The pronounced distortion of the spanwise distribution of load associated with increasing T_c is apparent. The effect of propeller operation on the spanwise center of pressure $\eta_{c.p.}$ is shown in figure 21. These data were obtained by integrating the loading data presented in figure 20, utilizing a straight-line fairing between the data points adjacent to the nacelles. The center of pressure moved inward with increasing T_c , the amount decreasing as the angle of attack was increased to 12° .

Figure 22 shows the importance of these aforementioned pressure-distribution changes with regard to the changes in the total lift and pitching-moment coefficients attributable to the operating propellers. It can be seen that the lift due to the propeller slipstream (ΔC_{L_B}) accounted for about 60 percent of the total change in lift with varying angle of attack; whereas the slipstream contribution to the change in pitching moment (ΔC_{m_B}) was apparently unaffected by increasing angle of attack.

High speed.- The effects of the operating propellers on the over-all force characteristics and section characteristics for Mach numbers from 0.70 to 0.90 for a constant Reynolds number of 1,000,000 are presented in figures 23 to 26. It is evident from the data in these figures that the effects of the operating propellers were not large compared to the propeller effects for the low-speed case. This is a consequence of the fact that the thrust coefficient is decreased considerably for the same power input.

The effects of increasing $T_{\rm c}$ on the chordwise distribution of pressure in the region of the nacelles are shown in figure 27 for a Mach number of 0.80. At the higher angles of attack, the apparent increase in pressure recovery for those stations between the nacelles might have been due to an increase in stagnation pressure caused by the operating propellers.

As indicated in figure 28, the effects of slipstream rotation at a Mach number of 0.80 on the spanwise distribution of loading were much less pronounced than in the previously cited low-speed case due to the lower values of thrust coefficient.

CONCLUDING REMARKS

Measurements of the surface pressures and forces on a semispan model of a wing-fuselage-nacelles combination representing the right-hand side of a hypothetical four-engine airplane have been presented. The effects of single-rotation right-hand propellers, of nacelles, and of extended trailing-edge flaps on the wing-surface pressures have been discussed.

At high thrust coefficients and a Mach number of 0.082, the propeller slipstream caused large changes in the spanwise distribution of loading over the region of the wing immersed in the propeller slipstream. The strong rotational components within the slipstream were responsible for inflections in the spanwise distribution of loading, there being large increases with thrust coefficient in the normal force of wing sections behind the up-going propeller blades with relatively small changes for sections behind the down-going blades. As a result, the center of pressure moved inward with increasing thrust coefficient.

At high subsonic Mach numbers, the over-all effects of operating propellers were not large when compared with the low-speed case for the same power input; this is a direct consequence of the large reductions in thrust coefficient with increases in free-stream velocity.

The addition of the nacelles to the plain wing (propellers removed) increased the velocity over the lower surface at those stations in the vicinity of the nacelles. These velocity changes contributed to an increase in the slopes of the lift and normal-force curves and a general increase in the angle of attack for zero lift.

Deflection of extended trailing-edge flaps ($\delta = 30^{\circ}$) over the inner 46 percent of the wing semispan (propellers removed) produced substantial gains in section lift over the complete semispan. The wing pitching moments were little affected by the flap deflection.

REFERENCES

- 1. Edwards, George G., Tinling, Bruce E., and Ackerman, Arthur C.: The Longitudinal Characteristics at Mach Numbers up to 0.92 of a Cambered and Twisted Wing Having 40° of Sweepback and an Aspect Ratio of 10. NACA RM A52F18, 1952.
- 2. Tinling, Bruce E.: The Longitudinal Characteristics at Mach Numbers up to 0.9 of a Wing-Fuselage-Tail Combination Having a Wing with 40° of Sweepback and an Aspect Ratio of 10. NACA RM A52119, 1952.

- 3. Boltz, Frederick W., and Shibata, Harry H.: Pressure Distribution at Mach Numbers up to 0.90 on a Cambered and Twisted Wing Having 40° of Sweepback and an Aspect Ratio of 10, Including the Effects of Fences. NACA RM A52K20, 1953.
- 4. Tinling, Bruce E., and Lopez, Armando E.: The Effects of Nacelles and of Extended Split Flaps on the Longitudinal Characteristics of a Wing-Fuselage-Tail Combination Having a Wing With 40° of Sweepback and an Aspect Ratio of 10. NACA RM A53D06, 1953.
- 5. Lopez, Armando E., and Dickson, Jerald K.: The Effects of Compressibility on the Upwash at the Propeller Planes of a Four-Engine Tractor Airplane Configuration Having a Wing With 40° of Sweepback and an Aspect Ratio of 10. NACA RM A53A30a, 1953.
- 6. Demele, Fred A., and Otey, William R.: Investigation of the NACA 1.167-(0)(03)-058 and NACA 1.167-(0)(05)-058 Three-Blade Propellers at Forward Mach Numbers to 0.92, Including Effects of Thrust-Axis Inclination. NACA RM A53F16, 1953.
- 7. Edwards, George G., Buell, Donald A., and Dickson, Jerald K.: The Results of Wind-Tunnel Tests at Low Speeds of a Four-Engine Propeller-Driven Airplane Configuration Having a Wing With 40° of Sweepback and an Aspect Ratio of 10. NACA RM A53128, 1953.
- 8. Sutton, Fred B., and Demele, Fred A.: The Effects of Operating Propellers On the Longitudinal Aerodynamic Characteristics at High Subsonic Speeds of a Four-Engine Tractor Airplane Configuration Having a Wing With 40° of Sweepback and an Aspect Ratio of 10. NACA RM A53J23, 1953.
- Herriot, John G.: Blockage Corrections for Three-Dimensional Flow Closed-Throat Wind Tunnels, With Consideration of the Effect of Compressibility. NACA Rep. 995, 1950. (Formerly NACA RM A7B28)
- 10. McLellan, Charles, and Cangelosi, John I.: Effects of Nacelle Position on Wing-Nacelle Interference. NACA TN 1593, 1948.
- 11. Hartley, D. E.: Low Speed Wind Tunnel Tests on Asymmetrically Situated Circular Cylindrical Bodies on a Straight and a 45° Sweptback Wing. British, R.A.E. Rep. No. Aero. 2349, Dec. 1949.
- 12. Martina, Albert P.: The Interference Effects of a Body on the Spanwise Load Distributions of Two 45° Sweptback Wings of Aspect Ratio of 8 From Low-Speed Tests At a Reynolds Number of 4x10°.

 NACA RM L51K23, 1952.

TABLE 1.- GEOMETRIC PROPERTIES OF THE MODEL

Wing
Reference sweepline: locus of the quarter chords of sections inclined 40° to the plane of symmetry
Aspect ratio
Frontal area (each)
Propellers
Diameter
For low speed tests

TABLE I. - GEOMETRIC PROPERTIES OF THE MODEL - Concluded

Finales		TO THE MAN TO THE TOTAL OF THE	
Fuselage			
Fineness ratio Frontal area (semis Fuselage coordinate	pan model)	• • • • • • • • • • • • • • • • • • • •	0.273 ft ²
	Distance from nose, in. 0 1.27 2.54 5.08 10.16 20.31 30.47 39.44 50.00 60.00 70.00 76.00 82.00 88.00 94.00	Radius, in. 0 1.04 1.57 2.35 3.36 4.44 4.90 5.00 5.00 5.00 5.00 4.96 4.83 4.61 4.27	
	100.00 106.00 126.00	3.77 3.03 0	

TABLE II. - INDEX OF TABULATED PRESSURE COEFFICIENTS

Table No.	R × 10 ⁻⁶	M	$\mathtt{T}_{\mathbf{c}}$	Configuration	au	range
III	4.0	0.082	0	Wing-fuselage-nacelles	20	to 16°
IV			.2	1		i
V			.4		1	1
VI		J.	.6 .8		1	1
VII	•	V			۱.	• - · ·
VIII	1.0	.80	0		20	to 10°
IX		.80	•04		20	to 100
X	1	.90	0	•	20	to 8°
XI	₩	.90	.03		20	to 80
XII	4.0	.082	Props off		20	to 20°
XIII	1.0	.80	t t		-2°	to 20°
VIX	1.0	.90			- 2°	to 10°
XV	8.0	.165			-2°	to 20°
IVX	2.0	.80			-2°	to 20°
XVII	2.0	.90		V	-2°	to 100
XVIII	8.0	.165		Wing-fuselage	-2°	to 20°
XIX	4.0	.082	₩	Wing-fuselage-nacelles	20	to 20°
				plus extended split		
}				trailing-edge flap	ŀ	

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0$ (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10° , 12°

	Jur-			Upper				П				surface		
Spanwise stations	east short	20	Į0	Angle o	attack	100	120		20	Į0	Angle	f attack	100	120
0.10 b/2	0 1.7 4.0 7.0 10.0 20.0 30.0 60.0 70.0 80.0 90.0	0.97 07 24 32 35 37 36 26 25 27 27	0.56 1.57 1.551 1.551 1.551 1.59 1.39 1.39 1.30 1.06	0.12 73 75 75 69 59 51 37 33 28 07	0.13 -1.14 -1.03 96 83 75 70 59 50 41 36 29 22 07	-0.30 -1.66 -1.35 -1.17 -1.03 90 81 68 56 44 39 32 23 09 03	-0.84 -2.18 -1.66 -1.41 -1.20 -1.05 93 75 61 50 41 24 10		0.05 15 18 19 18 19 16 12 10 05	0,51 .09 05 07 07 06 07 06 01	0.50 .28 .27 .04 .00 .04 .03 .02	0.61 .43 .18 .14 .09 .06 .05	0.66 .55 .29 .24 .18 .13 .10 .11	0.65 .64 .47 .42 .33 .25 .22 .15 .15
0.19 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	- 64 - 23 - 39 - 39 - 50 - 39 - 33 - 33 - 25 - 18 - 06 0	49 68 72 70 69 64 31 46 39 31 26 20 07	.12 -1.22 -1.06 94 87 77 58 50 43 35 29 21 09 01	49 -1.84 -1.45 -1.16 -1.09 92 68 55 44 37 30 07	-1.45 -2.61 -1.70 -1.48 -1.33 -1.11 74 61 49 41 31 20 08	-2.57 -3.39 -2.25 -1.76 -1.55 -1.24 80 53 40 30 30 30		08 09 31 35 29 18 06 01	.43 .20 01 11 18 11 04 .01	.59 .42 .20 .07 02 07 06 01 .03	.61 .56 .38 .23 .11 .02 .01	.50 .64 .52 .38 .24 .11 .07	.26 .64 .63 .51 .37 .21 .14 .09 .10
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	. 19 12 35 10 13 13 13 28 25 29 20 0	.49 50 63 61 61 57 49 39 39 32 28 21 08	.3h 92 9h 89 83 79 70 57 52 44 37 31 09 01	.03 -1.42 -1.26 -1.17 -1.02 93 83 67 77 49 39 33 23 08	-, k1 -2.05 -1.68 -1. k3 -1.26 -1.13 -1.00 77 66 55 -, kk 35 2k 08	-1.02 -2.69 -2.05 -1.73 -1.51 -1.30 -1.14 87 73 59 46 35 25 07		.09 22 25 26 24 21 16 11	.25 .04 07 13 10 11 11 10 06	.48 .26 .08 .02 .04 04	.62 .44 .23 .13 .12 .08 .05 .05	.71 .58 .36 .26 .23 .16 .12 .10 .07	.72 .70 .49 .37 .34 .20 .16 .13
0.375 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-53 1h 30 h0 h3 h5 h5 31 27 28 19 06	.49 62 64 66 64 60 37 37 31 25 19 05	.19 -1.20 -1.00 97 86 80 72 52 43 35 20 05	k1 -1.89 -1.37 -1.25 -1.15 -1.00 89 60 50 k0 31 21 05	-1.33 -2.76 -1.87 -1.61 -1.41 -1.20 -1.05 67 53 42 32 20 05	-2.47 -3.65 -2.36 -1.97 -1.40 -1.20 74 -57 57 21 06 01		02 21 24 23 20 16 07 03	.31 .08 04 10 09 10 07 03 .01	.52 .31 .08 .09 .01 .01 .01 .05	.58 .47 -28 .23 .14 .09 .07 -07 .08	.51 .57 41 .31 .26 .19 .16 .13 .11	.18 .15 .10
0.44 3/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.63 26 39 50 50 50 44 38 32 27 23 05	. 49 79 76 79 68 61 53 45 38 31 29 09	.02 -1.43 -1.17 -1.09 83 75 61 51 42 35 27 27 05	81 -e.17 -1.56 -1.39 -1.22 -1.01 90 71 87 87 29 29 20 05	-2.06 -3.10 -2.09 -1.78 -1.52 -1.23 -1.04 80 63 51 40 29 17 05 01	-3.6e -3.93 -2.6e -2.1k -1.79 -1.k2 -1.19 69 5k 69 5k 05 06		-13 09 24 30 36 29 19 11 05 .01	.46 .22 .02 .09 16 17 13 06 01 .04	.60 .46 .25 .12 .01 .06 .06 .03 .06	.55 .59 .39 .42 .27 .17 .06 .03 .04 .05 .07	.32 .64 .56 .43 .32 .16 .10 .10 .10	10 59 67 56 46 27 18 15 14 14

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0$ - Continued (a) $\alpha_u = 2^{\circ}$, 4° , 6° , 8° , 10° , 12° - Concluded

	Der-		···	Upper	surface				r		Lover	surface		
Spanvise	cont			Angle o	f attack							of attack		
stations	chord	50	70	60	80	100	120	ĺ	50	fo-	60	1 80	100	120
0.56 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.46 10 31 37 41 80 35 29 24 20 16	0.48 50 59 62 60 57 46 41 35 29 24 18	0.31 93 91 90 81 76 63 75 48 41 33 26 20	-0.03 -1.48 -1.28 -1.19 -1.03 79 66 57 50 38 30 22 06	-0.61 -2.14 -1.70 -1.47 -1.32 -1.13 94 76 64 53 41 32 06	-1.31 -2.81 -2.10 -1.80 -1.58 -1.32 -1.10 87 72 58 35 35 22 05		-0.10 26 26 27 27 18 14 01 01	0.24 0 10 10 11 11 09 07	0.48 .23 .07 .02 .01 01 01 02 .05	0.63 .41 .22 14 .10 .06 .05 .04	0.70 .56 .26 .22 .15 .14 .10	0.71 .68 .48 .37 .25 .21 .19 .12 .10
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0		-34 -36 -37 -57 -57 -57 -59 -45 -39 -34 -27 -21 -15 -01	.33 91 88 80 77 66 56 47 40 31 16 01	21 -1.58 -1.41 -1.24 -1.06 95 70 57 36 27 37 37	-1.08 -2.40 -1.87 -1.53 -1.35 -1.16 -1.018252382715	-2.31 -3.34 -2.39 -1.94 -1.66 -1.40 -1.20 94 71 96 39 26 11		17 27 25 22 17 14 09	.23 .03 .04 07 08 09 02	.48 .27 .12 .08 .06 .06 .03 .05 .07 .09 .10 .10	.55 .44 .26 .19 .14 .10 .10 .10	.50 .54 .38 .29 .26 .20 .17 .15 .14 .10	.31 .58 .49 .39 .35 .27 .24 .19 .15 .15
0.80 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 50.0 70.0 90.0 95.0	-53 -05 -13 -24 -31 -30 -36 -35 -26 -25 -26 -11 -30 -30 -30 -30 -30 -30 -30 -30 -30 -30	-53 -36 -44 -50 -51 -50 -46 -41 -35 -35 -25 -25 -25 -25	- 91 - 91 - 84 - 72 - 70 - 57 - 46 - 36 - 36 - 30 - 15 - 01	-, 43 -1.57 -1.27 -1.14 -1.00 86 75 61 52 44 36 26 27	-1.43 -2.36 -1.67 -1.45 -1.86 -1.96 91 71 79 46 37 25 14	-2.73 -3.30 -2.20 -1.81 -1.56 -1.28 -1.07 82 66 52 38 25 11 03 01		22 26 25 20 17 13 05 0 .06 .06	.20 .01 06 09 05 05 05 .05 .05 .06 .09 .09	.46 .26 .26 .11 .07 .05 .03 .03 .06 .06 .08	.56 .42 .25 .19 .14 .13 .10 .11 .10 .10	.53 .53 .53 .36 .28 .24 .18 .15 .11 .13 .11	.27 .57 .47 .39 .33 .25 .18 .17 .15 .13
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 60.0 70.0 80.0 90.0 95.0	0.38 .16 04 15 20 22 25 25 23 21 21 14 10 0	0.56 18 31 40 40 39 39 31 26 22 16 11	0.14 -63 -65 -65 -60 -75 -14 -33 -30 -20 -12 -05	0 -1.19 -1.039581675544302012 0 .04	75 -1.96 -1.40 -1.21 -1.048771554737322110	-1.81 -2.26 -1.85 -1.54 -1.28 -1.05 85 64 55 40 32 20 10			.01 09 11 10 06 04 0 .06 .08	.3k -10 .0k .01 -01 -01 -01 0 -07 .05 .06	.50	.53 .29 .29 .22 .18 .11 .10 .09 06	. 44 48 . 39 . 32 . 24 . 18 . 11 . 11 08 . 07

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = $\frac{4}{1000000}$, T_C = 0 - Continued (b) α_u = $1\frac{4}{10000}$, 16000

	Per-			Upper	surface	 			Lover	surface	
Spanwise stations	comt			Angle o	attack					f attack	
0.10 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	14° -1.52 -2.80 -2.03 -1.68 -1.41 -1.20 -1.0483665343241107	16° -2.30 -3.46 -2.38 -1.94 -1.60 -1.34 -1.159070554435251209				0.59 .71 .56 .47 .39 .21 .20 .20	16°			
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	-3.97 -4.14 -2.73 -2.07 -1.80 -1.41 70 56 43 30 30 07	-5.51 -5.02 -3.19 -2.01 -1.55 74 56 42 29 16 06 05				09 -60 -72 -62 -69 -30 -19 -12 -12 -04 02	52 .49 .78 .70 .57 .37 .25 .16 .15			
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-1.78 -3.41 -2.49 -2.05 -1.77 -1.51 -1.30 98 64 90 38 25 06	-2.64 -4.13 -2.89 -2.39 -2.01 -1.70 -1.44 -1.07 87 54 39 25 39				.68 .78 .59 .49 .41 .33 .27 .24 .18	.55 .80 .67 .56 .50 .40 .34 .28			
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-3.91 -4.70 -2.91 -2.34 -2.00 -1.62 -1.36 81 63 50 36 29 10	-5.55 -5.75 -3.44 -2.71 -2.29 -1.82 -1.51 87 66 54 54 14 05				.01 .57 .58 .52 .54 .36 .29 .23 .19	-, 42 .47 .63 .57 .52 .37 .27 .27 .29			
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	-5.54 -5.00 -3.20 -2.54 -2.11 -1.61 -1.33 76 76 76 30 17 06	-7.60 -6.05 -3.76 -2.90 -2.84 -1.79 -1.46 -1.02 78 29 18 07				67 .89 .74 .67 .57 .38 .26 .20 .16 .15	-1.38 .30 .76 .74 .67 .44 .32 .25 .20 .19			

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0 - Concluded (b) α_u = 14°, 16° - Concluded

	Per-		Upper	surface	 			Lover	eurface	
Spenvice	cest			fattack					f attack	
stations	obord		16°		7-	140	16°			
0.56 b/2	1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-3.58 -4.57 -2.16 -4.85 -4.53 -1.53 -1.59 -1.59 -1.54 -5.50 -3.77 -2.55 -1.06	38 3.04 2.51 2.13 1.73 1.42 1.10 97 70 70 53 40			0.65 .77 .58 .50 .41 .32 .28 .24	0.50 .79 .66 .56 .50 .40 .34 .30			
0. 69 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	-1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65 -1.65	0.55 0.65 0.75 2.75 2.32 2.32 2.36 1.55 1.86 1.55 1.84 1.75 1.84 1.75 1.84 1.75 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85			02 .56 .55 .44 .41 .32 .38 .19 .17 .11	50 .46 .58 .53 .49 .39 .39 .25 .29 .19			
o .Ro t /2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-3.97 -1.74 -2.20 -1.81 -1.51 -1.51 -1.51 -1.52 -1.57 -1.50 -1.57 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50	6.07 4.91 2.27 2.16 1.71 1.39 1.01 75 40 26 16			.10 .56 .53 .48 .39 .30 .22 .20 .16 .14 .09	1.29 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30			
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	-2.85 -2.31 -2.36 -2.31 -2.32 -2.33 -2.34 -2.30 -2.31 -2.00 -2.31 -2.00 -2.31 -2.00 -2.31 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00 -2.00	5.70 3.62 2.78 2.78 2.79 1.76 1.13 81 81 81 84 34 20 20 15 12			.25 .52 .45 .38 .30 .23 .16 .14				

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0.2$ (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10° , 12°

	Per-			Upper	surface					Lover	urface		
Spanwise	cent				f attack						fattack		
stations	chord	20	¥0	6°	80	10°	12°	20	Į,O	6°	go	10°	120
0. 10 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	0.57 1.08 1.08 1.08 1.08 1.08 1.08 1.08 1.08	0.56 	0.40 -74 -75 -75 -69 -63 -59 -53 -45 -34 -27 -21 -06 -01	0.06 -1.20 -1.03 99 87 77 61 38 31 38 31 39 08	-0.45 -1.78 -1.43 -1.20 -1.93 84 70 60 49 41 33 24 07	1.06 -0.33 -1.74 -1.26 -1.26 -1.26 -1.35 -1.35 -1.35 -1.35 -1.35 -1.35 -1.35	0.08 10 13 13 11 11 09 07 06 0	0.34 .14 .02 0 0 03 01 01 01 01	0.53 .33 .13 .13 .08 .07 .06 .07 .06 .07	0.63 .48 .25 .21 .15 .14 .11 .10	0.66 .59 .36 .31 .24 .22 .19 .15	0.63 .67 .53 .46 .39 .30 .26 .23 .20 .19
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 70.0 80.0 95.0	%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%	.60 -1.06 -1.99 -1.79 -1.77 -1.77 -1.78 -1.08 -1.08 -1.08	.01 -1.97 -1.97 -1.97 -1.97 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1.98 -1	82 -2.69 -1.91 -1.55 -1.40 -1.1576614939322106 .01	-2.00 -3.69 -2.50 -1.97 -1.73 -1.39 66 -53 52 33 21 06 .01	-3.57 -4.57 -4.39 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55	.67 .34 0 18 29 28 15	.92 .63 .26 .04 10 16 09 01	1.04 .84 .89 .08 .00 .00 .00 .00 .00	1.03 1.00 .69 .43 .23 .07 .05 .05 .08	.94 1.10 .87 .60 .38 .15 .14 .11 .16	.81 1.18 1.03 .76 .51 .26 .18
0,31 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	6.19.3% 6.20.20.20.20.20.20.20.20.20.20.20.20.20.	.80 -15-147 -57 -57 -57 -57 -49 -440 -39 -30 -30 -30	.84 55 79 83 80 77 60 55 39 24 24	.73 99 -1.14 -1.09 89 70 65 55 45 26 26	.51 -1.62 -1.59 -1.45 -1.19 -1.06 84 74 60 49 29 06	21 2.17 -1.95 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56 -1.5	50 61 53 50 36 36 24 19 10	04 26 30 32 26 20 16 13 08	188 888868 8 8 8 8	.62 .31 .09 .02 .04 .03 .03 .03 .04	.86 .53 .25 .13 .16 .14 .12 .11	1.04 .74 .41 .27 .26 .21 .19 .16
0.375 b/2	0 1.5 k.0 7.0 10.0 15.0 20.0 30.0 k0.0 50.0 60.0 70.0 90.0	.50 20 32 36 40 40 40 40 40	-53 -551 -55 -58 -58 -55 -37 -31 -26 -19 -04	.20 -1.11 91 90 84 78 71 54 37 37 30 22 06	43 -1.83 -1.21 -1.21 -1.21 -1.00 90 63 52 42 34 08	-1.43 -2.74 -1.86 -1.63 -1.42 -1.07 74 59 49 37 26 10	-2.61 -3.55 -2.50 -1.95 -1.15 -1.85 -1.85 -1.86 -1.53 -1.88 -1.53 -1.88 -1.88 -1.88 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80	09 24 21 20 15 05 01	.29 .09 04 05 06 05 06 07	.53 .35 .19 .19 .19 .09 .05 .07	59 .52 36 .27 .22 .15 .14 11 .12	.50 .60 48 .38 .33 .25 .20 16 .15	.27 .61
0.44 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	1.00 63 64 72 66 61 55 40 33 27 22 16 03	.63 -1.33 -1.10 -1.07 93 83 71 59 47 39 31 25 16 01	-10 -2.18 -1.60 -1.44 -1.24 -1.05 -91 71 76 46 36 28 20 03	-1.21 -3.12 -2.13 -1.86 -1.56 -1.28 -1.09 84 65 52 41 31 20 03	-2.79 -4.39 -4.38 -1.57 -1.57 73 73 45 21 05	-4.43 -5.43 -3.50 -2.83 -2.83 -1.79 -1.48 -1.64 50 36 21 05		.93 .60 .29 .08 80 15 09 02 .04 .10	1.04 .86 .54 .30 .12 .02 .04 .07 .11	.97 1.03 	.73 1.13 	1.13 .86 .65 .36 .24 .19 .18 .20

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0.2$ - Continued (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10° , 12° - Concluded

	Per-	~		Upper	surface			Г	<u> </u>		Lower	surface		
Spanwise stations	cent			Angle o	of attack						Angle	of attack		
acresome .	obord	20	fo.	60	80	10°	120		50	30	60	80	100	120
0.56 b/2	0 1.5 7.0 15.0 15.0 20.0 30.0 50.0 50.0 60.0 90.0	. 11111111 Roinburgerersche	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.86 52 74 80 57 57 55 36 36 36	0.75 -1.01 -1.12 -1.04 84 84 83 84 85 86	0,49 -1.65 -1.58 -1.19 -1.38 -1.21 -1.00847259472706	0.15 -2.26 -1.98 -1.80 -1.81 -1.81 -1.81 -1.81 -1.85 85 85 85 81 07		-0.66 77 61 50 48 36 26 21 01 01	-0.15 37 35 35 25 17 13 01 -03 -03	0.29 05 18 17 17 15 09 07 07	0.62 .23 .02 01 05 05 02 0	0.78 .46 .18 .11 .09 .07 .06 .07	1.07 .67 .36 .24 .19 .13 .14 .13
0.68 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 50.0 90.0	******************	*************	%884664855%8882566	256 256 256 256 256 256 256 256 256 256	-1.18 -2.48 -1.89 -1.39 -1.36 -1.19 -1.04 82 51 37 26	-2.54 -3.50 -2.45 -1.98 -1.74 -1.45 -1.26 97 74 58 43 29 14		89 30 26 20 10 10 01 03 07	.18 01 07 09 06 05 02 02	.47 .26 .12 .05 .04 .02 .05 .08 .08 .11	.57 .45 .27 .20 .16 .12 .12 .12 .12 .11	.49 .54 .40 .31 .27 .21 .19 .16 .15 .15	.26 .58 .51 .42 .36 .23 .23 .15 .15 .15 .15 .10
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 90.0 95.0	%1888888884 11111111111	538.927 - 1.45 -	.23 82 72 56 46 45 28 23 20	- 47 -1.59 -1.28 -1.10 -1.01 - 65 - 74 - 60 - 51 - 34 - 25 - 101 - 04	-1.59 -2.45 -1.75 -1.49 -1.30 -1.06 -2.71 -1.46 -1.55 -1.46 -1.55 -1.46 -1.55 -1.46 -1.55 -1.46 -1.55 -1.46 -1.55 -1.46 -1.55 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46 -1.46	-2.97 -3.46 -4.27 -4.86 -4.34 -4.11 85 67 53 39 26 12 05		28 33 28 22 17 13 05 .01 .04 .09	.18 0 07 08 06 05 05 .01 .02 .06 .09	.46 .26 .27 .07 .06 .04 .08 .09 .10	.58 .44 .26 .20 .16 .13 .11 .11 .11 .11 .10 .10	 .52 .53 .36 .29 .26 .20 .16 .15 .15	 .33 .57 .40 .34 .27 .20 .19 .15 .13
0.94 3/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	55.19 -01.16 -22.4 -22.4 -22.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6 -23.6	.55 -55 -57 -57 -57 -57 -57 -57 -57 -57 -	-63 -65 -65 -57 -54 -44 -32 -26 -18 -11 0	-1.05 -69 -69 -56 -34 -38 -22 -34 -38 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36	86 -2.07 -1.45 -1.23 -1.06 87 71 54 36 36 30 21	-1.96 -2.28 -1.87 -1.57 -1.57 -1.57 87 69 50 41 22 20 10 0			09 11 11 10 06 03 01	.34 .12 .06 .09 .01 0 .03 .06 .08 .09	.51 .28 .19 .13 .10 .06 .06 .07 .07 .08	.53 .40 .32 .23 .19 .13 .11 .10 .09 .08	. 12 . 17 . 10 . 32 . 24 . 19 . 11 . 11 . 09 . 07

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4 ,000,000; T_c = 0.2 - Continued (b) α_u = 14° , 16°

	Per-				surface		L			surface	
Spanwise stations	oeat obord	- 110	1 1/0	Angle o	f attack	·		- 40	Angle	f attack	
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	14° -1.87 -3.04 -2.15 -1.76 -1.48 -1.29 -1.887057465525106	16° -2.72 -3.72 -2.57 -2.05 -1.70 -1.40 -1.21957599473526				14° 0.54 .73 .63 .54 .38 .39 .29 .25 .24	166 0.40 .74 .68 .58 .53 .43 .38 .34 .29 .26			
0 .19 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	-1.60 -3.60 -2.69 -2.77 -1.75 -1.02 -1.48 -1.35 -1.07 -1.00	-6.61 -6.59 -1.17 -3.07 -2.55 -1.52 -1.08 81 64 49 32 15 02				1.18 .86 .64 .36 .26	-38 .80 .71 .71 .42 .32 .24 .25 -11			
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-21 -2.85 -3.41 -2.08 -1.64 -1.43 -1.43 -1.59 -59 -3.77 -3.66	74 -3.54 -2.84 -2.45 -1.87 -1.61 -1.21 -1.04 82 64 50 14				1.20 .92 .34 .40 .36 .31 .26 .25	1.25 1.20 1.50 .46 .39 .35 .32 -28			
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-4.23 -4.58 -2.86 -2.34 -2.01 -1.66 -1.42 90 -71 56 43 30 10	-6.05 -5.63 -3.43 -2.75 -2.30 -1.57 77 59 -44 -30 -311				09 .55 .56 .56 .50 .41 .36 27 .25				
0.44 6/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 90.0	-6.76 -6.67 -4.22 -3.31 -2.01 -4.01 -1.15 -56 -51 -51 -51	-9.56 -7.86 -3.76 -3.76 -2.23 -1.78 -1.29 68 18 18				-57 .72 1.16 .64 .76 .44 .33 .25 .24 .24	-1.62 .51 .83 .68 .45 .37 .30 .27 .26			

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.2 - Concluded (b) α_u = 14°, 16° - Concluded

	Per-			Upper	surface	 	T -		Lower	gurface	
Spamwise stations	cent				f attack				Angle o	f attack	
10011000	oberd	140	160				140	160			
0.56 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 50.0 50.0 60.0 80.0 90.0	\$5.\$5.54.88.93.58.88.68.68.68.68.68.68.68.68.68.68.68.68	179997777111111108				1.21 .85 .50 .38 .31 .24 .23 .20 .02 .22 .19	1.26 .97 .98 .41 .98 .88 .88 .88 .88 .88			
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	4.25 -1.25 -1.69 -1.69 -1.68 -1.68 -1.68 -1.13 00	6.21 -5.42 -3.72 -2.89 -1.95 -1.00 -1.86 -1.45 -1.11 -1.10				12 .54 .57 .51 .45 .35 .31 -25 .22 .20	67 .42 .59 .55 .50 .44 .37 .30 .25 .16 .10			
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	4.69 4.85 4.85 4.85 4.85 4.85 4.85 4.85 4.13 6.86 6.86	-6.73 -5.23 -3.46 -2.70 -2.25 -1.76 -1.43 -1.03 76 39 27 21 16				.02 .54 .57 .50 .41 .34 .21 .20 .15	-,45 .45 .58 .53 .48 .40 .29 .25 .21 .16			
0.9 4 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-3.39 -e.97 -e.37 -1.90 -1.23 -1.01 -72 -57 -41 -18 -09 -04	-5.08 -3.79 -2.88 -2.24 -1.80 -1.40 -1.14 80 60 43 34 22 17 15 14				.21 .54 .67 .80 .22 .24 .19 .14 .10 .07	 13 -57 -53 .47 .36 .29 .23 .19 .07			aca,

TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0.4$ (a) $\alpha_U = 2^{\circ}$, 4° , 6° , 8° , 10° , 12°

	Per-				surface			П				surface		
Spanvise stations	eport eport	20	Į0	Angle o	f attack	100	150		20	Į.o	Angle o	f attack	100	120
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 95.0	0.56 0.18 0.18 0.18 0.18 1.34 1.33 1.33 1.33 1.33 1.33 1.33 1.33	0.56 34 43 47 47 45 31 28 28 28	0.40 72 73 74 68 59 53 46 33 20 05	0.03 -1.21 -1.03 97 85 77 62 53 38 30 23 07	-0.50 -1.81 -1.44 -1.22 -1.07 95 86 71 60 50 42 33 24 08	-1.16 -2.39 -1.77 -1.50 -1.29 -1.12 99 81 54 55 35 25 10		0.09 07 09 10 09 07 07 04 .01	0.36 .17 .07 .04 .01 .01 .01 .02 .05	0.54 .36 .36 .18 .15 .10 .09 .07	0.64 .51 .36 .30 .25 .20 .17 .14 .13 .13	0.66 .61 .47 .40 .34 .28 .24 .20 .18	0,61 .70 .49 .42 .35 .30 .25 .23 .20
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 70.0 80.0 95.0	1.17 98 90 81 77 68 46 42 35 29 24 13 0	.67 -1.66 -1.32 -1.12 -1.02 88 56 57 34 28 18 18	02 -2.46 -1.80 -1.48 -1.31 -1.09 56 43 35 21 06	98 -3.32 -2.30 -1.85 -1.59 -1.30 64 49 39 30 21 06	-2.23 -6.80 -2.96 -2.29 -1.97 -1.57 9 71 55 43 21 06 .01	-3.60 -5.42 -3.53 -2.68 -2.78 -1.78 -1.02 79 60 46 37 20		1.14 .73 .24 06 24 26 13 01 .11	1.36 1.01 	1.46 1.23 .74 .38 .15 02 .03 .08 .15	1.44 1.39 -59 .31 .11 .10 -12 .18	1.36 1.52 1.15 .77 .46 .19 .18 .15 .24	1.22 1.62 1.34 .94 .60 .30 .25
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	.69 .41 09 26 35 40 41 35 36 36 32 27 20 01	1.00 .12 36 50 57 60 57 47 41 35 30 22 02	1.15 26 68 78 79 80 76 59 49 30 30	1.13 73 -1.04 -1.04 -1.06 -1.09 77 69 57 47 41 29	1.03 -1.28 -1.49 -1.30 -1.23 -1.11 80 66 53 44 32	.85 -1.84 -1.87 -1.72 -1.47 -1.31 -1.03 91 75 59 49 35 06					.53 .13 07 12 06 03 0 .02 .05	.84 .40 	1.13 .65 .29 .16 .18 .11 .15 .16 .16 .16 .11
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	.48 .08 12 27 34 35 30 25 20 02	.54 39 44 50 51 52 51 43 36 31 25 18 04	.27 96 82 83	32 -1.67 -1.23 -1.15 -1.07 96 87 52 43 34 24 06	-1.19 -2.53 -1.75 -1.57 -1.38 -1.21 -1.08 74 60 50 39 28 10 .03	-2.34 -3.34 -2.23 -1.91 -1.69 -1.45 -1.27 57 57 42 30 10		15 26 24 20 18 12 05 .01		.53	.60 .54 .40 .29 .28 .20 .17 .14 .15	.52 .62 .51 .39 .36 .25 .25 .19 .19	.32 .61 .59 .51 .48 .39 .34 .26 .25
0.44 6/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	1.28 98 84 97 59 56 46 40 33 32 25 12	0.75 -1.80 -1.33 -1.26 -1.09 93 76 61 47 39 31 25 20 06	15 -e.76 -1.90 -1.73 -1.44 -1.20	-1.40 -3.82 -2.53 -2.20 -1.80 -1.45 -1.20 89 66 52 40 30 17	-3.10 -5.16 -3.33 -2.79 -2.26 -1.78 -1.44 -1.07 78 61 46 35 20 05	-5.00 -6.51 -4.11 -3.32 -2.67 -2.04 -1.64 -1.17 86 67 51 36 21 05		1.09 .63 07 29 16 06 .03 .12	1.37 .97 .97 .53 .21 01 13 06 .01 .06 .01 .09 .09	1,45 1,25 .80 .46 .21 .01	1.38 1.43 	1.17 1.56 	.93 1.66 1.45 1.07 .78 .41 .32 .28 .27 .30

TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0.4$ - Continued (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10° , 12° - Concluded

	Per-		-	Upper	surface						Lover	surface		
Spanwise stations	taeo				f attack							of attack		
	ehord	20	\$°	೯	80	10°	120	<u> </u>	20	40	6°	80	200	120
0.56 8/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	0.47 .45 24 34 36 35 35 25 25 29 19	0.90 .16 -31 50 56 50 45 38 38 32 26 21	1.1k 2k 6k 76 81 76	1.20 71 99 -1.0h -1.07 96 85 73 67 54 36 27 05	1.10 -1.30 -1.47 -1.46 -1.42 -1.25 -1.05 89 79 64 51 43 32 06	0.88 -1.90 -1.89 -1.69 -1.67 -1.25 -1.04 91 72 57 34 07		-1.18 -1.16 78 66 50 34 25 01 01	-0.56 76 64 57 48 38 25 19 01 .03 .06	0.01 35 42 10	0.48 01 20 19 14 07 03 20	0.83 .26 02 04 05 05 .01 .03 05 .01 .02 .16 .15	1.13 .53 .10 .08 .04 .09 .10
o.68 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 70.0 80.0 90.0 90.0	3399988888559958	.55 23 43 47 50 46 46 41 33 30 24 19 12	80 87 81 	16 -1.52 -1.34 -1.19 -1.02 91 83 83 83 24 13	-1.15 -2.45 -1.87 -1.56 -1.19 -1.03 82 51 38 51 38 51	-2.5% -3.50 -2.45 -1.70 -1.44 -1.22957355402711 .01		36 40 33 28 20 16 10 10	.15 09 10 09 06 03 04 .05 .09 .10	.45	.57 .45 .27 .20 .18 .14 .14 .14 .14	.50 .55 .80 .31 .29 .21 .19 .18 .15 .15	.26 .58 .51 .43 .39 .31 .27 .23 .20 .19 .14
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	50 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12	.56 28 39 45 45 45 37 31 26 22 18 12 01	.25 87 80 77	& 4 -1.57 -1.26 -1.23 98 84 71 57 50 40 22 13 .01	-1.60 -2.47 -1.75 -1.49 -1.31 -1.09 92 71 59 46 36 25 25 25 25	-3.04 -3.50 -2.29 -1.87 -1.62 -1.32 -1.11 83 65 50 36 23 10 03 01		31 35 30 23 18 14 04 0	.17 0 07 06 04 04 05 .01 .05 .09 .10	.47 .26 12 .06 .06 .05 07 .08 .10 .10	.59 .45 .27 .23 .17 .13 .11 .12 .12 .11	.52 .54 .39 .31 .26 .21 .16 .15 .15 .14	.33 .58 .49 .42 .35 .29 .20 .20 .16 .15
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	.33 .21 .01 10 16 19 21 20 20 20 11 08	.56 13 28 35 35 35 35 27 27 25 20 15 09	.45 61 63 56 53 40 31 28 25 17 10	01 -1.19 -1.04 95 80 67 55 43 39 33 28 19 10	87 -2.08 -1.45 -1.24 -1.06 86 71 55 37 30 20 11	-2.02 -2.29 -1.90 -1.58 -1.31 -1.06 86 65 51 10 31 19 09		 52 29 30 24 19 14 06 03 03 01	08 08 12 10 09 09 02 0 08 .10	34 12 .06 01 .01 .04 06 .08 .09 .10	.52 -29 .20 .15 .10 .07 .08 .08 .09 .09	.53 	

TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.4 - Continued (b) α_u = 14°, 16°

	Per-			Upper	surface				Lower	surface		
Spanwise stations	eest ebord	110	1.70	Angle o	fattack		140	1/2	Angle o	fattack		
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-2.01 -3.13 -2.20 -1.81 -1.52 -1.30 -1.13 91 74 59 48 37 26 11	16° -3.00 -3.82 -2.64 -2.12 -1.75 -1.46 -1.25 -1.0079635138271510				0.52 .74 .45 .45 .49 .40 .40 .35 .31 .26 .25	16° 0.30 .7170 .60 .55 .44 .41 .36 .31 .3015				
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	7.09 6.78 1.18 1.59 1.19 1.11 1.65 1.39 1.65 1.39 1.66 1.66	-6.72 -7.77 -3.57 -3.57 -2.93 -2.20 -1.21 56 54 66 56				1.09 1.69 1.48 1.08 .74 .41 .32 	.11 1.54 1.53 1.10 .83 .49 .39 .39				
0.31 b /2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 60.0 70.0 90.0 95.0	.57 -2.49 -2.33 -2.08 -1.72 -1.51 -1.16 -1.04 67 53 39 06	.20 -3.16 -2.78 -2.48 -2.22 -2.00 -1.75 -1.32 -1.15 72 78 74 58 41 05 .15				1.36 .88 .45 .29 .29 .24 .24 .24	1.51 1.06 -57 .40 .39 .34 .31 .30 -28				
0.375	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 70.0 80.0 95.0	-3.85 -4.30 -2.77 -2.31 -2.67 -1.46 -1.75 60 -1.47 33 33 33	75.69 75.34 -3.34 -2.34 -1.66 -1.66 -1.66 -1.65 -1.53 -1.53 -1.53									
0. 44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	-6.84 -7.93 -3.86 -3.86 -3.86 -3.86 -3.86 -3.89 -1.81 -1.86 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70 -3.70	-10.19 -9.25 -9.68 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50				1.57 1.14 .92 .53 .39 .35 .35 .35 .35	-1.49 .77 .79 .92 .93 .56 .47 .39 .35 .35			Z	

TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.4 - Concluded (b) α_U = 140, 160 - Concluded

	Per-			Upper	surface	 			Lover	surface	
Spannice	cent				f attack				Angle	f attack	
stations	obort	140	16°				140	16			
0 .56 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	0.55 -2.58 -2.36 -2.19 -1.73 -1.75 -1.17 -1.01 81 63 51 36 06	0.11 -3.30 -2.87 -2.59 -2.59 -1.59 -1.34 -1.14 90 71 56 56				1.37 .77 .35 .22 .20 .14 .18 .17 .10 .26 .24	1.53 .93 .93 .28 .21 .25 .23 .30 .30			
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	+ 32 + 30 - 3,11 - 2,14 - 2,06 - 1,69 - 1,69	-6.40 -5.50 -3.79 -2.45 -1.63 -1.89 -1.89 -1.32 -1.32 -1.31 -1.11				-14 -54 -58 -52 -36 -36 -34 -27 -24 -21 -15	74 .40 .56 .51 .44 .38 29 .26 .24 .16			
0.80 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-1.87 -2.90 -2.99 -1.95 -1.27 71 53 37 22 06 06	-6.98 -5.35 -3.52 -2.73 -2.79 -1.45 -1.55 -1.55 29 21 21				02 .54 .56 .50 .34 25 .21 .20 .14 .10	50 .43 .57 .55 .48 .39 .28 .24 .21 .16			
0.9 4 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	-3.51 -3.01 -2.61 -1.94 -1.57 -1.29 -1.02 74 57 61 31 17 10 05	-5.28 -3.86 -2.92 -2.82 -1.82 -1.15 81 61 43 35 25 27 16				.19 .53 .48 .41 .34 .25 .19 .15				

TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.6 (a) α_u = 2°, 4°, 6°, 8°, 10°, 12°

				Doner	Surface						Lower	surface		——
Spanvise	Per-		Angle of attack 20 to 60 80 100 1									f attack		
stations	ehord	50	ţo	60	80	100	150		20	fo	60	90	100	120
0.10 p/s	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	0.57 .015 .221 .226 .30 .286 .221 .217 .217 .213 .06	0.56 - 32 - 42 - 44 - 44 - 44 - 36 - 30 - 26 - 16 - 01	0.40 -71 -71 -64 -60 -57 -52 -44 -37 -33 -26 -20 -06	0.02 -1.20 -1.03 94 62 76 69 61 51 42 36 28 21 06	-0.51 -1.80 -1.42 -1.05 94 84 72 50 50 54 08	1.24 -1.48 -1.80 -1.47 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -1.08 -		0.10 06 07 06 07 00 00 00 00	0.36 .18 .09 .07 .08 .09 .06 .09 .09 .09	0.55 .36 .24 .20 .18 .13 .12 .10 .10 .10	0.64 .53 .39 .32 .30 .25 .29 .16 .17	0.66 .63 .50 .42 .39 .32 .28 .24 .20 .20	0.60 .71 .60 .51 .48 .39 .39 .28 .27
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 90.0 95.0	1.30 -1.38 -1.14 87 76 76 74 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 75 -	.73 -2.12 -1.60 -1.33 -1.17 98 58 36 33 26 14 01	07 -3.01 -2.12 -1.47 -1.47 -1.20 72 55 41 35 20 05	-1.12 -3.99 -2.70 -2.13 -1.81 -1.45 63 46 36 28 19 05	-2.41 -5.12 -3.35 -2.59 -1.71 96 72 55 42 31 04	-3.92 -6.28 -4.04 -3.04 -2.52 -1.94 -1.08 -7.79 -3.33 -1.91 -0.05		1.59 1.11 -06 -17 -08 -09 1.19 -10 -06	1.78 1.38 71 .27 .03 13 01 01 02	1.91 1.63 .98 .50 .23 .01 .05 	1.90 1.81 	1.82 1.97 1.44 .93 .56 .25 .25 .25 .25	1.66 2.07 1.64 1.13 .72 .37 .37 .33 .42
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	.76 .57 .04 .26 .30 .39 .39 .39 .39 .23 .23 .18	1.14 .32 -30 -51 -58 -56 -46 -47 -40 -31 +29 -21 0	1.36 -02 61 76 80 79 60 51 41 36 28 23	1.44 48 97 -1.06 -1.01 95 75 70 57 46 39 28 01	1.43 -1.00 -1.36 -1.35 -1.30 -1.22 -1.13 86 89 54 55 31 02	1.34 -1.54 -1.80 -1.72 -1.57 -1.46 -1.32 -1.01 75 58 47 33		-1.29 -1.33 -1.02 92 62 44 29 21 09 18	72 91 76 73 47 33 22 14 05	15 49 49 39 24 14 09 02	.34 10 28 30 16 08 02 .03 17 .25	.73 .22 06 13 0 .05 .09 .11 16	1.10 .53 13 .02 .14 .16 .17 .19 22
0.375 Б/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-16 -04 -18 -22 -31 -31 -30 -26 -21 -01 -07	.56 29 36 47 49 47 42 36 31 26 19 03	-31 -84 -72 -75 -77 -71 -66 -53 -45 -31 -31 -24 -06	15 -1.52 -1.15 -1.10 -1.02 94 86 	91 -2.29 -1.63 -1.48 -1.36 -1.19 -1.06 76 61 51 39 28 07	-1.98 -3.14 -2.13 -1.86 -1.67 -1.45 -1.28 71 57 44 31 09 .06			.24 .08 04 01 03 01 02 .05	.52 .37 .16 .14 .10 .10 .10 .11 .14 .14	.64 .56 .43 .32 .30 .21 .20	.60 .66 .54 .44 .43 .31 .30 .24 .24	.46 .68 .57 .58 .55 .45 .39 .31 .31
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	1.48 -1.35 -1.04 -1.07 -86 63 51 37 37 30 21 03	.81 -2.27 -1.60 -1.53 -1.03 83 64 49 39 34 29	-21 -3.34 -2.21 -2.00 -1.52 -1.06 -35 -35 -26 -20 -30 -30	-1.59 -1.54 -2.96 -2.95 -1.62 -1.31 99 54 54 30 19 01	-3.36 -5.93 -3.77 -3.15 -2.50 -1.95 -1.54 -1.10 81 61 46 32 19 01 .06	-7.48 -7.48 -4.69 -3.79 -2.25 -1.77 -1.24 68 50 36 02		1.54 .98 .05 21 27 15 03 .05 .16	1.80 1.35 -74 .33 .05 10 04 .05 .11 .21	1.90 1.65 	1.82 1.86 	1.66 2.01 1.58 1.08 .74 .36 .27 .27 .29 .34	1.34 2.11 1.78 1.29 .93 .49 .36 .36 .35

TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0.6$ - Continued (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10° , 12° - Concluded

	Per-			Upper	eurface			Τ		Lower	surface		
Spanwise stations	cent				f attack						f attack		
0.00.000	chart	20	10	6°	80	10°	120	_2°	,0	6°	go	100	120
0.56 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 50.0 50.0 60.0 70.0 80.0 95.0	0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43	0.97 .38 46 59 59 59 59 59 39 39 14	1.32 .01 -57 -78 -79 -70 -59 -59 -59 -34 -27 -34	1.49 48 93 -1.01 90 80 59 49 41 59	1.52 -1.02 -1.36 -1.42 -1.10 28 -1.10 85 68 56 46 35 07	1.42 -1.58 -1.82 -1.80 -1.72 -1.53 -1.99 77 61 50 37 06	-1.66 -1.56 -1.56 -1.20 -1.02 85 40 30 30 01 .04	-1.00 -1.14 92 82 66 51 30 22 03 .04	-0.35 70 59 49 39 22 16	0.23 31 44 40 35 27 16 09 02 .13 .15	0.68 .01 24 23 20 16 05 01 03 .18 .26	1.08 .33 01 06 06 05 04 .23 .33
o.68 ъ/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 95.0	.29 .20 .20 .20 .20 .20 .20 .20 .20 .20 .20	56994446554988872886728867	TP&FPGGRAPACHTS	1.48 1.17 1.90 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.8	1.10 4.39 1.58 1.34 1.15 1.00 1.86 1.36 1.36 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30	-2.53 -3.47 -2.43 -1.67 -1.41 -1.20 94 71 55 39 25 11	42 44 35 29 23 18 12 01 .02 .06 .09		144 198888 19777	.58 .45 .28 .20 .17 .13 .13 .13 .14	.51 .55 .40 .32 .29 .24 .19 .17 .17	.27 .60 .51 .44 .39 .31 .29 .24 .22 .20 .15
o.80 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	. 49 . 16 . 04 . 15 . 12 . 28 . 28 . 16 . 11 . 10 . 10 . 11 . 10 . 10 . 10 . 10	.57 27 38 45 45 45 45 29 29 21 17 11 0	.26 84 78 75 53 43 32 27 20 13 0	48 -1.57 -1.26 -1.07998472585040322413 .01	-1.61 -2.45 -1.73 -1.47 -1.30 -1.08 91 70 57 45 34 24 13 01	-3.10 -3.51 -2.29 -1.87 -1.61 -1.31 -1.09 80 50 50 35 21 09 00		.15 02 09 08 09 04 01 .01 .07 .08 .10	.46 .26 .29 .09 .06 .05 .05 .09 .10 .10	.59 .45 .28 .22 .19 .15 .13 .14 .14 .13	.53 .54 40 .31 .27 .21 17 .15 .15 .14 .11	.32 .58 51 .45 .36 .29 21 .20 .18 .11
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 90.0	.32 .22 .02 .06 -11 -16 -19 -20 -17 -17 -17 -17 -17 -06 .09	.56 -13 -28 -33 -33 -33 -33 -33 -26 -22 -20 -13 -07	.46 58 62 63 52 39 41 30 27 24 16 10	01 -1.19 -1.03 94 76 65 53 41 37 31 26 17 10	89 -2.08 -1.45 -1.0586715436301810 .02	-2.06 -1.57 -1.57 -1.06 85 51 39 39 30 18 06			 .34 .06 .03 .01 .01 .04 .08 .09 .10	.52 -31 .24 .15 .12 .09 .09 .09 .09 .09	.53 .43 .25 .20 .15 .12 .11 .09 .09	41 55 . 47 . 35 . 28 . 20 . 15 . 14 10 . 09 . 06

TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.6 - Continued (b) α_u = 14°, 16°

	fer-			Upper	surface				Lower	surface		
Spanwise stations	cest			Angle o	fattack	,			Angle o	f attack		
Feetal	short	14°	16°				140	16°				
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0	4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.75 4.20 2.20 2.75 4.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20	-3.20 -3.86 -3.86 -3.69 -4.14 -1.76 -1.46 -1.26 -1.80 80 38 27 15				0.47 .74 	0.25 .71 .63 .59 .50 .45 .34 .36 .34				!
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-5.5% -7.56 -4.79 -3.53 -2.91 -2.20 -1.86 56 50 50 03 03	-7.33 -8.91 -5.57 -3.28 -2.45 -1.31 95 71 54 23 06 02				1.46 2.14 1.79 1.26 .87 .49 .47 .40 .44	.92 2.09 1.87 1.34 .98 .58 .50 .43				
0.31 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	1.16 -2.17 -2.26 -2.09 -1.87 -1.71 -1.53 -1.15 -1.04 85 53 53 53	.89 4.82 4.71 4.83 4.05 -1.81 -1.20 75 61 03				1.40 .79 .31 .16 .25 .26 .28	1.64 1.01 46 .28 .34 .30 .31 .32				
0.37 5 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-3.39 -4.11 -2.71 -2.89 -2.01 -1.72 -1.51 -1.51 -1.66 -50 -36 -36 -36 -36	-5.15 -5.13 -3.28 -2.70 -2.36 -1.98 -1.72 -1.15 91 74 55 13 .05				.17 .66 .76 .70 .65 .75 .35 .37	-29 .53 -30 .77 .74 .63 .55 -15 .41				
0.44 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-7.61 -9.10 -5.37 -3.51 -2.55 -1.96 -75 -75 -75 -75 -75 -75 -75 -75 -75 -75	-10.63 -10.68 -6.45 -6.45 -3.79 -3.77 -6.12 -1.42 -1.42 -1.58 58 27 08				.80 2.13 1.85 1.40 1.06 .61 .50 .81 .39 .81	81 1.61 1.79 1.29 1.13 .70 .96 .46 .44			Z	

TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.6 - Concluded (b) α_u = 14°, 16° - Concluded

	Per-			Upper	ourface	 	T -		Lover	purface		
Spanwise	cent			Angle o	f attack	 			Angle (of attack		
stations	short	170	160				140	160				
0.56 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 70.0 90.0 90.0	14444444444444444444444444444444444444	0.88 9.80 9.80 9.80 9.74 1.29 1.29 1.29 1.29 1.29 1.29 1.29 1.29				1.12 .60 .09 .09 .04 .11 .12 .03 .28	1.63 .81 .31 .17 .16 .11 .20 .19 .04 .33 .29				
0.68 b/2	0 1.5 4.0 70.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	**************************************	**************************************				14 24 59 53 46 36 33 26 24 22 16	75 .40 .57 .54 .45 .39 .39 .29 .19				
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 90.0 95.0	***************************************	-7.14 -5.41 -3.54 -2.74 -2.80 -1.46 -1.04 -1.55 -1.20 -1.20 -1.20					-57 -38 -36 -50 -40 -29 -26 -21 -16 -10				
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	-3.58 -3.59 -3.49 -4.55 -4.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55 -1.55	-5.36 -3.88 -2.92 -2.26 -1.81 -1.14 79 60 34 24 24 16				.17 .60 .54 .41 .35 .27 .20 .18 				2	

TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.8 (a) α_u = 2°, 4°, 6°, 8°, 10°, 12°

				Upper	surface			_			Lower	aurface		
Spanwise	Per-				f attack							f attack		
stations	ebord	20	40	6°	80	10°	120		50	40	60	80	100	12°
0 .10 b /2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	0.57	0.57	0.40 69 66 60 55 51 44 35 25 17 04	0.02 -1.20 -1.02 92 84 75 70 61 92 42 36 29 21	-0.58 -1.83 -1.41 -1.22 -1.06 95 73 61 49 41 33 10	-1.30 -2.47 -1.80 -1.51 -1.30 -1.12 -1.00 83 68 76 36 25 36		0.10	0.37 .20 .11 .09 .09 .07 .07	0.55 .40 .26 .22 .18 .16 .15 .15 .15	0.65 .55 .41 .35 .33 .26 .24 .20 .18 .19	0.65 .65 .45 .40 .34 .30 .24 .24	0.58 .71 .61 .53 .49 .41 .36 .33 .29 .27
9 .10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	1.38 -1.80 -1.37 -1.13 98 80	.70 -2.62 -1.86 -1.52 -1.27 -1.07 49 37 30 23 15	17 -3.59 -2.43 -1.94 -1.62 -1.30 74 54 40 33 25 15 05	-1.26 -4.63 -3.05 -2.38 -1.97 -1.56 87 46 36 29 20 05	-2.65 -5.87 -3.93 -2.91 -2.39 -1.86 	-4.16 -7.14 -4.54 -3.39 -2.77 -2.11 		2.05 1.50 .67 .19 11 24	2,24 1,79 .97 .44 .12 .08 0	2.34 2.05 1.24 .31 .04 .12 .18 .30	2.33 2.24 1.51 .49 .18 .20 .21 .34	2.24 2.39 1.73 1.10 .67 .30 .29 .40	2.14 2.53 1.94 1.30 .85 .44 .39
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	.81 .74 01 28	1,26 .52 25 51 55 63 61 41 35 31 24 .03	1.55 .20 56 76 76 81 79 60 61 59 41 35 25 .03	1.68 23 -1.90 -1.05 -1.09 -1.06 -1.00 75 61 50 41	1.72 78 -1.34 -1.36 -1.31 -1.21 99 72 58 50 36 03	1.71 -1.30 -1.74 -1.72 -1.66 -1.56 -1.44 -1.11 -1.01 84 66 55 04 04		-1.77 -1.75 -1.28 -1.16	-1.10 -1.26 -1.03 94 64 45 27 20	- 46 - 81 - 75 - 70 - 45 - 29 - 115 - 08 - 08	.12 -35 -48 -30 -16 -06 0	.61 .05 .24 .29 .15 .06 .01 .05	1.02 .27 02 13 02 .04 .07 .10
0.375 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	.38 .24 .04 09 17 27 27 31 28 25 20 15 .01	-5915273741454545413630251901	.46 70 62 68 67 65 	.05 -1.34 -1.04 -1.03 97 91 85 	67 -2.12 -1.55 -1.44 -1.31 -1.18 -1.07786352402906 .09	-1.60 -2.93 -2.05 -1.84 -1.66 -1.47 -1.31 74 60 46 32 08		30 35 26 24 25 17 12 05 .02	.20 .05 .01 .02 .01 .01 .03 .07	.51 .34 .25 .19 .18 .12 .11 .10 .12	.67 .56 .36 .35 .26 .24 .18 .20	.69 .69 .50 .48 .37 .34 .29 .28	.60 .76 .73 .64 .60 .49 .44 .38 .35
0.44 b/2	0. 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	1.61 -1.77 -1.25 -1.25 98 83 65 92 94 38 25 17 07	.82 -2.76 -1.86 -1.73 -1.36 -1.11 86 65 49 40 34 24 11	29 -3.95 -2.54 -2.28 -1.78 -1.44 -1.13 82 98 46 36 26 16 01	-1.78 -5.23 -3.33 -2.85 -2.23 -1.76 -1.38 99 54 39 28 17 01	-3.65 -6.72 -4.22 -3.72 -2.12 -1.64 -1.62 62 45 -33 -20 0	-5.84 -8.47 -5.20 -4.19 -3.25 -2.47 -1.91 -1.32 70 72 37 22 03 .08		2.00 1.39 65 .19 15 25 13 0 .09 .21	2,24 1.75 1.01 .50 .15 06 0 .10 .15 .28	2.34 2.06 1.34 .80 .41 .10 .12 .18 .22 .32	2,24 2,28 1,63 1,07 ,67 ,28 ,25 ,25 ,30 ,37	2.02 2.45 1.88 1.29 .86 .42 .33 .35 .36 .42	1.75 2.57 2.57 2.11 1.50 1.08 .58 .47 .42 .41 .46 .16

TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.8 - Continued (a) α_u = 2°, 4°, 6°, 8°, 10°, 12° - Concluded

	Per-			Upper	ourface						Lover	ourface		
Spanwise stations	cont				f attack			1				f attack		
	201	20	10	60	80	105	150	Ц	20	40	6°	80	10°	120
0.% b/2	0. 1.5 4.0 7.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	0.38 .77 .09 .18 .34 .37 .36 .37 .36 .34 .30 .26	1.00 .59 .15 .44 .58 .51 .51 .36 .31 .27 .03	1.45 .24 .63 .73 .83 .76 .65 .45 .38 .32	1.71 22 87 -1.06 -1.14 -1.20 95 85 79 62 51 43	1.83 78 -1.32 -1.44 -1.47 -1.33 -1.15 99 91 72 79 49 39	1.85 -1.33 -1.76 -1.80 -1.76 -1.38 -1.16 -1.05 -83 67 56 10		-2.20 -1.95 -1.47 -1.25 96 75 45 33 03 .01	-1.47 -1.54 -1.05 85 64 36 26 26	-0.74 -0.78 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83 -0.83	-0.05 -63 -70 -60 -53 -37 -22 -14 -12 -15 -28	0.05 -24 -36 -36 -26 -26 -27 -39 -39 -39	0.96 .10 .25 .22 .17 .05 .01
o.68 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.24 .26 .20 .10 .23 .26 .20 .15 .20 .15 .20 .20 .20 .20 .20 .20 .20 .20 .20 .20	-56 -13 -35 -40 -42 -41 -36 -26 -20 -10 -20	. 46 - 68 - 78 - 74 - 65 - 57 - 50 - 35 - 26 - 20 - 21 - 20 - 21	08 -1.k3 -1.28 -1.13 97 86 76 65 22 41 31 23 11	-1.04 -2.33 -1.78 -1.49 -1.31 -1.15 -99 -79 -61 -49 -35 -24 -11 .04	29 39 39 39 39 39 39 39 39 39 39 39 39 39		- 446 - 46 - 31 - 31 - 24 - 19 - 12 - 01 - 03 - 06 - 10 - 11	.08 .08 .08 .13 .12 .09 .06 .02 .07 .07 .11 .11	.23 .09 .05 .04 .04 .06 .10 .10 .13 .12	.58 .55 .27 .20 .17 .13 .14 .14 .15 .14	.56 .56 .33 .29 .24 .20 .19 .18 .17	.29 .60 .52 .44 .39 .26 .24 .20 .20 .15
0.80 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.48 .19 .02 -13 -22 -24 -23 -22 -21 -15 -10 .01	.58 -24 -35 -37 -42 -40 -35 -29 -25 -20 -16 -10 0	.28 81 76 74 65 52 43 34 26 21	- 43 -1 - 55 -1 - 24 -1 - 03 - 96 - 84 - 70 - 96 - 48 - 40 - 30 - 23 - 12 0	-1.60 -2.44 -1.72 -1.47 -1.29 -1.07 90 70 45 45 24 21	-3.13 -3.72 -2.30 -1.87 -1.33 -1.11 83 51 36 23 10 04		37 38 31 24	.15 .02 .06 .05 .03 .01 .05 .07 .09 .10	.46 .26 .12 .10 .07 .06 .10 .11 .11 .12	.59 .45 .28 .22 .18 .15 .12 .14 .13	.52 .55 .33 .27 .22 .17 .16 .15 .11	.32 .58 .51 .43 .36 .30 .22 .20 .18
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.31 .24 .04	.56 11 25 32 33 33 33 24 21 19 13 06 06	. 57 61 60 53 36 37 29 25 22 15 04	14 -1.18 -1.02 92 76 54 41 36 26 18 11	89 -2.05 -1.44 -1.24 -1.05 86 70 54 45 35 30 19 06	-2.10 -2.29 -1.91 -1.59 -1.31 -1.06 66 63 51 18 09 01		24	01 07 09 09 05 01 01 06 09	.34 .15 .09 .02 .02 .04 .05 .05 .08	.92 .30 .23 .15 .11 .09 .09 .09	.53 .12 .34 .26 .21 .15 .12 .11 .09 .09	.40 .51 .44 .34 .29 .21 .15 .14

TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; PROPELLERS REMOVED - Continued (a) α_u = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-	L		Upper	surface			T	T		Lovez	surface		
Spanwise stations	cent			Angle	of attack			1				of attack		
	chord	-20	00	50	10	60	8°	1	-50	on	S _Q	40	60	8°
0.56 b 2	0 1.5 4.0 7.0 • 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0	0.21 .31 .09 05 14 21 26 27 25 24 19 15	0.35 .19 .09 -19 -29 -35 -35 -35 -31 -26 -24	0.50 06 31 46 58 55 51 46 46 35 24 17	0.54 38 59 74 81 81 71 51 51 35 26 18	0.49 66 85 94 -1.01 -1.14 -1.07 60 45 36 31	0.41 89 -1.04 -1.09 -1.15 -1.26 -1.20 -1.15 57 57 50 41 28 13		-0.69 90 95 83 83 52 31 31	-0.51 75 66 57 45 57 45 29	-0.06 31 37 36 32 28 24 21 11	0.24 01 13 16 15 14 12 11	0.43 .20 .04 .01 .01 .04 .04 .05	0.54 .2') .14 .07 .04 .01 0
0.68 b-2	95.0 0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 60.0 70.0 80.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0	.05 06 .50 .25 .11 .02 07 14 20 21 19 15	.04 .13 .39 .0905142227313128242116 0	.05 .46 .13 71 35 43 46 51 44 33 70 15	-03 -08 -25 -59 -83 -78 -74 -60 -75 -62 -39 -31 -24 -15	09 .01 .04 66 -1.09 -1.11 -1.09 -1.07 40 30 21 11	13 05 86 -1.12 -1.05 -1.05 -1.03 99 81 66 76 37 30 21		-1.15 -1.21 -1.11 -1.05 66 41 25 07 02	90 -1.02 86 71 50 32 22 07 01 .08	21363530231701040911	.01 .05 .23 .01 .10 .11 .12 .11 .06 .03 .10	.03 .05 .05 .01 .01 .01 .01 .03 .06 .10 .10	01 .01 52 .33 18 .10 .08 .05 .05 .05 .05 .06 .09
0.84 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	.19 .50 .30 .16 .08 .03 .08 .13 .17 .17 .15 .19 .09	.35 .42 .17 .04 09 15 21 24 19 16 15 11	.60 .12 13 27 41 44 40 37 34 28 25 15	.62 29 51 61 66 70 66 56 51 45 30 21 13	.47 74 89 -1.00 -1.06 91 92 57 38 29 10	.33 -1.00 -1.17 -1.18 -1.11 -1.06 -1.06 72 55 43 24 24 24		89 82 73 66 54 31 21 11	-1.02 91 68 42 27 11 04 .02 .07 .10	26 36 31 26 19 04 0 .04 .09 .11	.21 .01 10 11 10 06	.43 .24 .08 .03 .03 .01 .04 .06 .08 .10	.53 .35 .10 .10 .00 .00 .00 .00 .00 .00 .00
0.9 4 b/2	0 1.5 h.0 7.0 10.0 15.0 20.0 30.0 ho.0 50.0 60.0 70.0 80.0 95.0	.05 .30 .33 .03 .03 05 16 18 11 11	.12 .44 .26 .02 .06 12 19 20 20 16 11	. 17 .20 .01 24 29 33 34 30 26 21 16 05	.63 15 34 45 51 52 45 40 34 26 15 08	-54 -62 -76 -88 -81 -76 -68 -40 -31 -24 -17 -08	.\$3 -1.00 -1.05 -1.06 -1.03 96 96 90 59 31 22 14 06		54 54 53 50 45 36 36 20 15 11	99 91 85 63 46 34 19 09		.06 10 13 14 12 06 03 03	.36 .11 .05 0 01 01 01 01	. 48 .23 .25 .09 .05 .03 .04 .05 .05 .05

TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; PROPELLERS REMOVED - Continued (b) α_U = 10°, 12°, 14°, 16°, 18°, 20°

	Per-				surface						eurface		
Spanwise stations	cent	10°	120	Angle o	f attack	180	200				fattack		
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	10° 0.49 -1.00 -1.04 -1.15 -1.10 -1.08 -1.00956670432520	0.39 -1.20 -1.26 -1.34 -1.26 -1.29 -1.11 71 71 75 75 38	0.26 -1.36 -1.50 -1.42 -1.41 -1.43 -1.22 -1.07 86 81 84 76 55	160 0.14 -1.43 -1.43 -1.36 -1.37 -1.30 -1.24 -1.16 -1.06 -1.00 -93 89 81 66	0.01 -1.40 -1.38 -1.3k -1.3k -1.29 -1.26 -1.21 -1.16 -1.11 -1.05 -1.00 76 68	20° -0.11 -1.40 -1.36 -1.36 -1.32 -1.30 -1.25 -1.26 -1.09 -1.039482	10° 0.74 .54 .35 .27 .23 .16 .10 .09 .07 .01	0.81 .65 .45 .37 .32 .24 .18 .11 .11	0.85 .72 .53 .43 .38 .29 .24 .18 .14 .13	0.90 .81 .61 .52 .45 .30 .25 .20 .18	18° 0.92 .86 .68 .57 .52 .42 .39 .24 .2001	20° 0.93 .91 .74 .62 .56 .40 .31 .27 .25
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.28 -1.18 -1.27 -1.20 -1.16 -1.10 -1.01 88 76 60 47 36	01 -1.25 -1.22 -1.07 -1.06 -1.06 -1.06 -1.04 95 87 74 62	21 -1.25 -1.27 -1.04 -1.03 -1.02 -1.05 -1.05 99 94 81 72 60 56	37 -1.21 -1.20 -1.04 -1.02 -1.04 -1.01 97 78 78 73	57 -1.14 -1.13 -1.09 -1.10 -1.10 -1.11 -1.12 -1.00 89 85 83 75 71	76 -1.15 -1.14 -1.12 -1.13 -1.13 -1.13 -1.16 -1.17 -1.0591898078	.74 .66 .45 .25 .04 .05 .03 .01 .03	.76 .74 .57 .39 .16 .03 .03	.75 .19 .46 .26 .10 .05 .01	.74 .84 .73 .57 .37 .19 .11 .04 .04	.69 .86 .64 .45 .25 .17 .08 .05	.65 .87 .85 .71 .53 .31 .22 .10 .06
0.31 p/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.36 -1.00 -1.30 -1.36 -1.32 -1.28 -1.30 -1.14 -1.00 85 59 59 24	.26 -1.12 -1.21 -1.18 -1.17 -1.16 -1.12 -1.00928175555543	.1b -1.16 -1.13 -1.06 -1.06 -1.06 -1.04 98 89 77 70 61 50	.05 -1.06 -1.0h -1.0h -1.0h 93 89 87 80 76 67 57	09 -1.00 98 -1.02 -1.01 84 82 80 79 76 76 71 62 65	16 -1.06 -1.00 -94 86 84 81 79 79 75 68	.65 .49 .30 .21 .18 .11 .06 .02 06	.73 .59 .31 .25 .18 .11 .06	.76 .66 .38 .32 .24 .15 .10	.80 .73 .56 .47 .41 .31 .23 .15	.81 .80 .64 .53 .46 .36 .26 .20	.84 .85 .69 .59 .54 .43 .34 .25 .08
0.377 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.22 -1.25 -1.16 -1.10 -1.14 -1.05 -1.00 	.06 -93 -97 -85 -84 -84 -70 -67 -64 -56	10 83 83 76 77 76 76 70 65 60 61	-20 -77 -77 -74 -73 -73 -70 -69 -69 -66	35 72 72 70 71 70 70 68 68 69 68	51 74 72 72 72 72 71 71 71 71 70 69	.61 .49 .30 .21 .14 .07 .02 .06 06	.66 .56 .59 .29 .23 .12 .06 06	.66 .60 .45 .35 .28 .19 .10 06	.66 .66 .51 .41 .34 .23 .14 .01 .05	.66 .70 .58 .48 .42 .29 .21 .05 .02	.63 .71 .61 .54 .46 .34 .26
0.44 8/2	0 1.5 à.0 7.0 10.0 15.0 20.0 30.0 è0.0 50.0 60.0 90.0 90.0	.15 92 -1.00 86 75 74 73 69 69 69 99 97 47	.03 71 76 71 66 66 66 66 64 58 25 46	11 65 66 66 64 64 61 55 55 47	26 66 67 66 66 66 67 66 61 57 53	43 65 65 65 65 65 66 66 63 59 56	60 69 69 69 69 70 69 61 61	.60 .61 .26 .04 .16 .13 .09 .07	.70 .68 .72 .35 .14 .09 .10 .06 .10	.70 .72 .58 .43 .23 .01 .07 .08 .10 09	.66 .74 .65 .49 .30 .05 06 10 10	.64 .80 .72 .77 .39 .20 .02 .08 .08	.76 .80 .76 .63 .46 .20 .06 .01

TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; PROPELLERS REMOVED - Concluded (b) α_u = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

	Per-			Upper	surface						Lover	surface		
Spanutse	cent				f attack						Angle o	f attack		
atations	chord	100	120	14 ⁰	16°	18°	20°	ŀ	10°	120	140	16°	18°	200
	0	0.34	0.25	0.15	0.05	-0.06	-0.20	_						
j	1.5	-1.00	-1.07	-1.20	-1.30	-1.46	-1.52		0.59	0.65	0.69	0.72	0.75	0.75
Ì	4.0	-1,20	-1.31	-1.45	-1.53	-1.61	-1.57		.39	.47	.54	.60	.69	-73
- (7.0	-1,23	-1.35	-1.47	-1.51	-1.55	-1.54							
(10.0	-1.24	-1.31	-1,42	-1,48	-1.55	-1.54		.22	.29	.36	.43	•51	-56
- 1	20.0	-1.31	-1.33 -1.28	-1.40 -1.37	-1.50 -1.45	-1.56 -1.51	-1.53 -1.50		.15	.22	.27	.34	.43	.47
0.56 b/2	30.0	-1.16	-1,05	-1.07	-1.16	-1.30	-1.35		.05	.13	.16	.21	•37 •29	3,
0,76 6/2	¥0.0	••0	64	69	-,80	-1.01	1.20		.05	.09	.12	.15	.21	.54
	50.0	4/	- 48	• • • • •	- 65	84	-1.04		.00	.0%	.08	.11	.15	.1,
ļ	60.0 70.0	43	46	47	54	63	79			:	• • •			
1	80.0	30	37	- 41	-,50 -,46	56 50	66 58		or .c1	0.01	0	.02 01	.05	90. راد.
	30.0	17	- 24	34	41	- 44	- 49	Ì	72	04	- 06	10	05	:6
	95.0	11	-,20	31	3 /	41	- 44)	∪3	06	11	15	- 14	15
	<u> </u>		 					⊢	 					
	1,5	.30 -1.05	.20	.07 87	%	21 94	35 99	l	.57	.60	.57	.50	.57	.99
İ	1.0	- 16	-1,01	. 11	93	07	-1.00		146	48	دود.	.54	.57	. 10 .54
	7.0	*)	86	83	88	93	17	l					[´.]	
	10.0	95	- 86	83	- Ru	-,05	- 19	ļ	.24	.3⊖	•35	.4C	.45	٠.4
	15.0 20.0	- 90 - 85	86 84	81	97	11	- 17		115	.21	• :26	•27	-35	.4.
0.66 6/2	30.0	75	77	81 *6	87 82	30 86	90		.07	.18	.1.	.24	.2) .1)	. 34. .75
0100 072	40.0	- 69	- 73	2.7	- 80	e•,	97	1	.05	1 . 5	.(*4	.11	.15	.16
	50.0	01	66	70	73	76	- 79	1						
	60.0	5'	50	67	++64	74	- 77		.0f:	.05	•05	.05	•07	• •
	70.0 80.ა	40		54	67	62	65	1	- (:la	.04	.∞	•01	•43	• -3
	90.0	29	46	41	57	61	64		.04 00	0%	0 11	01 12	-•15	15
	15.0	26	31	40		16	- x ²	1	11	12	25	23	26	54
	3	.17	.04	11	25	41	53	_	 	 				
	1.5	-1.18	-1.17	-1.13	-1.11	-1.07	1.00		.56	.59	.59	5.5	.57	-55
	4.0	-1,23	-1.17	-1,20	-1.16	-1.11	-1.05	i	.39	45	.50	-54	.55	56
	7.0	-1.16	-1.07	-1.10	-1.09	-1.05	-1.00	l			1			
	10.0	-1.11	-1.09	-1.11	-1.11	-1.06	-1.01	1	.24	.30	.34	.37	جه.	.45
	15.0 20.0	-1.12 -1.00	-1.02 98	-1.05 -1.00	-1.04	-1.01 -1.01	-1.00	1	.15	.20	.24 .20	.29 .23	•33 •28	.36 .30
o.84 b/2	30.0	86	- 88	90	1	- 94	94	ı	-08	1 .11	.14	.16	19	.22
	40.0	- 70	83	8"	89	92	75	i						
	50.0	 70	72	78	8≥	86	10	l	.05	.07	.07	.08	.04	.11
	60.0 70.0	62 52	-,66	71 66	78	80	85	Ì	.05	.06	.05	.05	.06	.06
	80.0	43	52	61	66	75	78 71	1	.07	.04	.01	01	01	04
	90.0	- 33		53	59	61	63	1	.03	- 02	- 06	09	11	13
	95.0	25	38	48	53	••55	59		03	10	14	18	20	23
	0	.29	.19	.05	10	25	•.25	_						
	1.5	-1.23	-1.10	-1.02	99	93	66	1	.51	.56	.57	.58	-57	-57
i	4.0	-1.11	-1.09	-1.09	-1.09	97	66	l	· · ·		l	[l	
i	7.0	-1.05	-1.01	98	95	88	64	1	.28	.34	.38	.41	-45	.45
i	10.0	-1.08 -1.06	-1.05	-1.01 93	-1.00	93	67	1	.19	.25 .16	.29	.33	.37	.38
ı	20.0	-1.00	91	90	91	87	65	1	.08	.13	.14	.19	.21	.22
0.94 6/2	30.0	80	79	79	81	81	62	1	.03	.06	.08	.10	.13	.13
i	40.0	67	73	74	76	81	61	1	.01	.04	.04	.04	.07	.05
1	50.0	56	65	68	71	••75	59	1	٥	.01	.01	.01	.02	.01
	60.0 70.0	49	59	65	69 6h	74	58	1	.02	0	03	05	06	10
	80.0	29	- 44	- 54	60	- 63	54	1	ã	01	05	09	10	16
	90.0	20	35	46	54	56	50		.01	-,05	u	15	13	25
	95.0	15	30	42	50	%	49	ĺ	03	11	20	25	19	30
		<u></u>			<u> </u>							•		

TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING M = 0.90; R = 1,000,000; PROPELLERS REMOVED

(a) α_u = -2°, 0°, 2°, 4°, 6°, 8°

Promites.	Per-				surface						eurface		
Spanwise Stations	cent chord	*50	0°	20	f attack	68	80	-20	00	Angle o	f attack	60	80
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.53 .43 .20 .06 0 .08 14 22 24 31 31 31	0.63 .30 .09 -05 -12 -20 -24 -30 -34 -39 -44 -47 -41 -21	0.70 .65 .06 .20 .35 .30 .35 .41 .45 .50 .59 .57	0.73 -:01 -:22 -:35 -:38 -:45 -:45 -:57 -:66 -:71 -:19 -:11	0.73 18 37 51 54 54 59 57 59 61 70 79 24	0.69 40 56 71 68 66 70 66 67 66 77 66	-0.17 -39 -39 -37 -39 -39 -39 -39 -22 -14	0.01 22 26 26 27 33 36 34 15	0.21 02 12 15 15 20 25 29 35 29	0.38 .14 .01 .03 .07 .11 .16 .24 .34 .26	0.51 .29 .14 .07 .04 .02 .07 .14 -17 .09	0.64 .43 .25 .18 .14 .07 .01 .04 .05 .01
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.65 .44 .15 -03 -15 -34 .05 -41 -,40 -38 -37 -35 -25 -20	.73 .28 01 17 30 49 .05 51 51 51 33 16	.76 .09 01 34 62 .05 70 60 61 76 76	.73 15 16 29 61 79 83 71 68 69 71	.67 40 65 71 75 93 79 75 75 75 75 75 75 75	555 - 68 - 88 - 955 - 109 - 112 - 84 - 81 - 81 - 81 - 81 - 81 - 81 - 81 - 81	17 34 41 50 48 43 46 51 46	.06 14 26 44 54 50 50 51 45	.29 .09 0 30 55 49 50 41 27	.46 .25 .06 .16 .51 .68 .48	.61 .41 .20 .02 37 .65 13 02 0	.70 .55 .33 .11 .24 .42 .05
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 60.0 70.0 80.0 90.0 95.0	.37 .30 .02 10 18 27 32 37 43 42 45 40	.45 .16 13 25 33 45 50 53 57 57 55 45 18 06	.52 .03 .28 .41 .47 .58 .69 .72 .70 .65 .72	.58 14 45 57 63 77 85 85 89 79 90 12	.60 31 62 70 76 86 89 91 91 79 57 45 31	-55 -51 -79 -39 -100 -1.00 -37 -1.00 -89 -68 -68 -53 -51		24 50 67 65 55 39 36 48 06 01	02 28 41 37 31 27 28 26 41 13	.18 .09 -18 .20 .18 .17 .20 .20	.47 .15 01 05 07 07 11 14 25 29	.52 .31 .13 .07 .05 .01 .05 .08
0.375 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.36 .36 .13 05 16 27 36 56 59 56	.48 .23 .01 .20 .31 .41 .51 .63 .67 .66 .65	.60 .03 20 49 62 66 79 75 67 37 15	.62 40 56 66 75 82 81 75 59 35 24	.60 47 56 74 83 90 94 76 66 55 43 36	.52 .72 .81 .90 .97 .93 .91 .80 .73 .66 .62	53 77 84 76 74 67 51 15 15	30 59 63 56 51 50 47 29 06	.01 24 33 33 34 36 38 36 31	.26 .02 12 18 20 25 30 31 37 03	.44 .20 .04 .04 .08 .14 20 36 36	.55 .34 .16 .07 .02 .06 12 31 36
0. 44 b /2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.52 .37 .11 09 20 12 65 65 59 57 50 24 28	.62 .20 05 36 57 66 82 76 72 70 45 23 22	.70 01 24 51 70 79 82 65 53 38 27 17	.70 29 46 63 73 82 81 73 54 54 54 28	-63 56 67 81 75 76 66 66 69 69 44	.50 77 83 76 78 72 70 66 67 67 68 50		10 41 40 53 50 34 36 43 43		.41 .16 .02 .16 .41 .66 .62 .50 .36 .19	.17 0 25 59 67 11 01	.66 .48 .30 .13 .49 .69 .07 .07

TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; PROPELLERS REMOVED - Continued (a) α_u = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface						Lover	surface		
Spanwise stations	cent			Angle o	f attack						Angle	of attack		
S CECTORS	chard	-20	00	20	10	вр	8º°		-5 ₀	ο°	20	ħo.	6°	Вo
	0	0.26	0.35	0.49	0.53	0.45	0.51							
	1.5 4.0	.25 .01	.10 15	.03	17 41	39 60	51 69		-0.55	-0.40	-0.09 37	0.09 16	0.18 06	0.42
	7.0	14	30	39	56	73	77]		1]
	10.0	25	43	49	65	80	85		89	91	49	27	-,20	.04
	15.0 20.0	34 37	-,55 -,56	66 69	81 86	95 -1.00	98 -1.01	1	84 84	75 67	44	30 26	24 21	01 02
0.56 b/2	30.0	4~	62	70	~.85	-1.00	-1.02		66	56	- 33	24	22	06
	40.0 50.0	45 37	60 54	64 60	80 72	96 93	-1.00 94		57 53	50 46	29 26	23 20	23 22	07 09
	60.0	35	41	29	32	54	55				i			
	70.0 80.0	26	20 17	1°	• .29 • .29	41	41 27		36 ∩5	23 06	12 .01	16 08	21 15	12 06
	90.0	06	05	.01	09	18	16	i	.01	01	.04	01	14	08
	95.0	.04	.01	.09	-01	11	13		.08	.05	.12	.05	10	06
	0	.10	-25	.51	-56	.49	.54							
	1.5 4.0	.45	.01	.15 21	06	29 61	50 82		79	57 79	24	.10 13	.26 .05	.41 .20
	7.0	.02	16	36	53	75	91							
	10.0 15.0	09 17	26 33	47 56	64 74	81 76	86 84		97	97 90	49 48	22 26	09 14	.04 03
- 10 - 1	20.0	-,24	40	61	76	74	83		89	76	41	23	13	06
0.68 b/2	30.0 40.0	31 30	45	64 57	75 72	75 61	77 66		64	69 14	33 18	19 12	14 11	09 06
	50.0	29	35	48	~.55	50	61							
	60.0 70.0	24 20	30 18	23 17	33 19	44	52		20 .0;	œ .03	02	02 .04	05 01	05 02
	80.0	16	12	11	11	30 31	41		.11	.10	.10	.09	.02	01
	90.0 95.0	.03 .14	.03	.04 .12	03 .01	26	34		.14	.12	.12	.08	01 08	06 15
						20	31				.13	.09	00	ļ
	0	.32 .50	.47	.61 .16	.63 11	.58 37	.49 61	. }	69	72	28	.11	.28	.41
	4.0	.29	.14	09	35	57	78		60	79	44	11	.08	.20
	7.0 10.0	.15	02	25 35	49 57	70 77	97 94		59	69	43	19	05	.04
	15.0	05	23	-,45	66	86	-1.00		57	58	38	20	10	01
0.80 b/2	20.0 30.0	12 18	28 29	52 43	73 65	85 80	96 92		52 46	58 27	32 25	16 11	08 08	02 05
-,-	40.0	20	30	40	65	79	[9 9]							
	50.0 60.0	21 19	29	39 33	58 30	71 50	74 60		36 29	10 03	04 .01	.01	03 .01	01 .01
	70.0	+.16	•.20	28	14	36	53		24	.02	.06	.10	-04	.04
	90.0 90.0	14 13	20 05	07 .03	04	21 10	43 33		19 11	.07	.10	.10	.07	.05
	95.0	11	.06	.11	.08	01	23		10	.11	.15	.10	.09	03
	0	.20	.28	.50	.63	.60	-55	\dashv						
	1.5	.51	. 42 . 24	.02	06	31 49	59 69		40	88	~.57	0	.24	.37
	7.0	.35	.09	12	27	-62	79		38	78	48	15	.02	.13
	10.0	.10	02	22	52	75	91		38	80	45	19	05	.04
	15.0 20.0	.01 05	11 18	29 34	55 60	74	81 79		36 36	70 65	40 35	20 16	11 08	01 0h
0.94 b/2	30.0	16	25	38	-,54	67	75		*.31	32	26	12	09	06
	40.0 50.0	20 26	26 27	36 32	51 47	65 46	61 51		•.27 •.30	18 10	09	09 06	06 04	07 06
	60.0	21	15	27	18	31	43							
	70.0 80.0	19 16	•.17 •.17	02	O4	20 12	36 31		25 20	.05	.08	.09 .12	0,04	02
	90.0	15	.02	.09	.09	04	22		19	.13	.16	.14	.08	.01
	95.0	15	.10	.14	.14	01	20		11	.15	.18	.18	.09	06
ســـــــــــــــــــــــــــــــــــــ													-	ACA Z

THE RESIDENCE THE RESIDENCE OF

TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm u}$ = 10.

	Per-		 Upper	eurface			 Lower	surface	 · · · · · ·
Spanvise stations	cent chord	100	 Angle o	f attack		roc	 Angle o	f attack	
0.10 6/2	0 4.00000000000000000000000000000000000	0.000				0.73 .52 .35 .77 .14 .09 .04 .11 .03			
0-2467	0	- 43 - 11 - 1.11 - 1.17 - 1.17 - 1.17 - 1.11 - 1.11 - 1.11 - 1.11 - 1.11 - 1.11 - 1.11 - 1.11 - 1.11				.7% .6% .7% .7% -19 -19 -77 -17 -17			
0.31 t/.	1.1 1.0 10.0 10.0 10.0 10.0 10.0 10.0 1	14 4				.66 .43 .75 .11 .14 .70 .77 .73			
0.575 b/2	1.7 4.0 10.0 15.0 15.0 20.0 50.0 40.0 50.0 40.0 90.0	.34 9 21 31 22 31 77 74 77 68 67 68				.63 .45 .27 .19 .11 .14 -25 -24 -26			
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.36 90 85 77 75 75 73 69 69 69 65 56				.72 .59 .44 .25 .01 .37 .50 .14 .12 .11			

TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm U}$ = 10° - Concluded

	Per-		Upy	er surface		T	 Lover	surface	
Spanwise stations	cent chord		Ang	e of attack			Angle o	f attack	
		100			 	100	 		
0.%6 b/2	0 15 0 0 15 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.47 66 85 92 97 -1.08 -1.09 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05				0.52 .30 .12 .06 .04 01 05 09			
0.68 b/2	0 1.5 10.0 15.0 20.0 20.0 50.0 50.0 70.0 95.0	.44 63 91 83 83 83 75 66 66 55 45				.46 .29 .11 .03 .01 06 06 09 09 09			
0.90 ь/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	.37 79 96 -1.04 -1.07 -1.01 -1.00 94 81 69 57 42				.10 .04 .04 .01 .03 03 01 03 01			
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.44 85 87 84 77 79 66 61 56 49 37				.43 .19 .10 .04 0 .06 07 10 08 12			

いたのないないのでは、 大きのないのでは、 大きのないのできないないできないないできないない。

TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED

(a) $\alpha_u = -2^\circ$, 0° , 2° , 4° , 6° , 8°

Spanwise	Per-			Upper	surface						eurface		
stations	cent chord	₽°	o ^o	Angle o	f attack	6 ⁸	80	-2°	o°	Angle o	f attack	6°	8°
0.10 ь/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0	0.14 .36 .08 .09 -117 -119 -116 -117 -114 -04	0.12	0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505	0.55	0.43 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.6	0 0.17 1.09 1.98 1.90 1.69 1.69 1.51 1.34 1.08 1.08	0.666 1.434 1.898 1.808 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108 1.108	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.06 13 19 19 19 16 14 10	0.30 .09 08 10 11 10 07 03	0.48 .27 .13 .06 .04 0	0.60 .43 .76 .18 .15 .09 .07 .06 .06
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	831.16 0.1.19 1.00 0.00 0.00 0.00 0.00 0.00 0.	.47 .20 07 18 27 32 31 27 24 20 16 06	25283827 1111110 202288887 255888250 201111111111111111111111111111111111	-51 -58 -66 -65 -66 -62 -44 -37 -31 -26 -19	17 1.12 1.02 1.91 1.88 1.78 1.51 1.52 1.29 1.20 1.08 1.01	1.73 -1.73 -1.39 -1.08 -1.08 -1.56 -1.37 -1.30 -1.08 -1.08 -1.08	91 88 78 73 31 31 32 05		.08 12 26 34 37 30 19 07 01	.40 .17 -02 -13 -20 -20 -12 -03 -02	.57 .40 .19 .0505050505050505	.62 .55 .36 .21 .10 .01
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	01 .36 .11 0 08 15 10 20 +.21 19 10 14 04	.33 .18 08 18 29 29 29 30 27 21 21 06	4911333942434339393939393929200601	.50 46 60 62 59 55 48 45 39 34 29 21	. 31 91 91 83 81 76 59 58 53 44 37 31 21	07 -1.43 -1.25 -1.14 -1.02 81 66 60 50 34 24 07	de 64 69 61 53 44 37 31 20	40 50 46 43 39 33 24 16	02 21 26 27 25 21 18 11	.27 .07 08 11 12 11 10 07	.47 .28 .10 .04 .01 0 03 03	.60 .45 -25 .17 .12 .09 .05 .04
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 99.0	21 .42 .22 .06 03 11 15 21 19 19 17 13 04	.28 .25 .02 14 20 26 29 27 24 20 16 04	.52 13 28 39 42 43 37 32 24 25 21 07	.51 56 60 62 63 58 38 32 26 19	-23 -1.12 94 89 80 72 36 29 29 06	-32 -1.80 -1.34 -1.22 -1.11 -97 -87 -61 -50 -40 -31 -22 -06	-1.06 92 70 60 54 43 34 18 10		-03 -19 -23 -25 -23 -21 -17 -09 -04	.30 .07 -03 -09 -10 -11 -09 -04 0	.50 .30 .30 .06 .02 01 01 .03 05	.57 .46
0.44 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	19 .46 .23 .05 04 15 19 24 23 21 19 16 13 03	.35 .20 0 18 30 32 34 30 27 24 19 14 04	.57 -19 -33 -46 -45 -50 -45 -37 -33 -28 -23 -217 -09	.51 72 66 76 69 68 60 53 45 39 26 19 05	.10 -1.33 -1.07 -1.04 84 75 63 28 28 19 06	64 -2.05 -1.52 -1.37 -1.18 -1.02 88 73 60 49 40 30 20 06	-1.25 -1.08 88 77 75 22 11 04	53 61 54 56 56 43 28 17 09 03	.05 -19 -25 -37 -38 -12 -05 0	.49 .15 0 -11 -19 -19 -13 07 02 .02	.59 .41 .09 01 07 09 02 0	.61 .56 .26 .15 .09 .04 .09

というのは、中間、大変ので、一個なないのでは、大変のないできるというできます。

TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_u = -2^\circ$, 0° , 2° , 4° , 6° , 8° - Concluded

	Per-			Upper	surface			1			Lover	eurface		
Spanvise	tgeo			Angle o	f attack			Ī			Angle o	f attack		
stations	oberd	-€ °	00	50	40	60	80		Ψ°	o°	50	40	60	вo
0.56 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	-0.22 .37 .16 .04 10 12 17 17 16 14 13 10	0.22 .21 02 19 23 24 24 25 23 19 17 13 04	0.45 08 26 39 39 34 34 34 29 21 21	0.48	0.27 94 91 83 83 73 63 96 96 35 20 06	-0.17 -1.49 -1.23 -1.12 -1.03 89 75 64 57 48 38 30 21 06		-1.07 90 72 62 52 33 27 07 07	-0.54 57 50 44 38 39 20 20	-0.11 26 27 24 20 17 14 08 02	0.23 0 11 11 10 08 03 03	0.67 .25 .07 .03 .01 0 01 01	0.59 .42 .16 .13 .09 .07 .05 .07
0.68 b/2	0 1.5 4.0 7.0 10.0 20.0 20.0 30.0 40.0 50.0 50.0 90.0 90.0	-66 -50 -50 -70 -70 -70 -71 -71 -71 -71 -71 -71 -71 -71 -71 -71	15 .36 .08 01 11 16 13 21 20 14 14	1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70	**************************************	59998887148774998877899	57 -1.49 -1.11 -1.12 -1.02918070564635271702		-1.45 -1.01 58 46 33 24 09 01	77 67 40 22 16 05 01 05 06	1 20 29 1 20 20 20 20 20 20 20 20 20 20 20 20 20	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$.45 .27 .11 .55 .55 .64 .67 .67 .69 .69	.54 .42 .26 .18 .15 .11 .10
0.80 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 70.0 80.0 90.0	-41 -52 -55 -61 -63 -61 -67 -67 -68 -68	.20 .37 .16 .82 -04 -11 -13 -18 -19 -19 -19 -10	53 68 11 126 68 136 136 136 136 136 136 136 136 136 136	\$##\$\$\$\$\$ ##888#88	-27 -86 -81 -72 -66 -58 -37 -30 -24 -13 -03	32 -1.49 -1.15 -1.03 95 81 72 51 43 26 17 03		-1.55 -1.01 69 55 44 08 08 08	47 48 30 32 22 11 05 0 . 06	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	198 5585 58587	.11 .27 .11 .06 .05 .03 .05 .05 .07 .09 .10	.35 .42 .34 .17 .15 .11 .09 .10 .10
0.94 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 80.0 50.0 60.0 70.0 90.0 95.0	-1.00 .51 .37 .23 .14 .07 .07 .07 .07	-15 .42 .27 .07 .08 -05 -03 -13 -15 -11 -07 .06	.36 .19 0 11 15 17 19 19 19 19 113 08	- 15 - 29 - 33 - 34 - 32 - 36 - 36 - 16 - 10 0 0	.48 -:59 -:62 -:63 -:57 -:51 -:40 -:34 -:30 -:24 -:19 -:12 0	.11 -1.09 97 85 75 95 52 40 34 20 13 0		-1.90 -81 -67 -57 -29 -19 -11	-1.10 -57 -49 -39 -30 -21 -14 -07 -09	-,45 -,30 -,29 -,24 -,19 -,08 -,04 -,04 -,06 -,08 -,09	0 -08 -14 -10 -06 -04 0 -07 -08 -10	.33 .01 .03 .00 0 .00 .00 .00 .00	.51 .25 .19 .12 .06 .05 .06 .07

TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (b) α_u = 10°, 12°, 14°, 16°, 18°, 20°

	Per-			Upper	urface					Lover	urface		
Spanwise stations	cent			Angle of	attack					Angle of		- 62	250
0.10 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 50.0 60.0 90.0 95.0	10° -0.27 -1.38 -1.15 -1.09 -1.15 -1.60 -1.60 -1.60 -1.60 -1.60 -1.60 -1.60 -1.60 -1.60	20 -0.78 -4.08 -1.67 -1.43 -1.26 -7.63 -7.63 -7.24 -7.95 -7.24 -7.26 -7.26	140 7.46 7.60 8.68 7.76 1.54 1.34 1.70 1.75 1.75 1.75 1.75	160 -0.16 -3.27 -1.92 -1.33 -1.17 -90 -70 -55 -34 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05	180 4.88 13.65 4.10 1.12 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86 1.86	20° -3.97 -4.13 -2.93 -2.27 -1.84 -1.47 -1.17 -1.09 -80 -63 -47 -29 -3.98 -1.71 -1.71 -1.55	10°	12°	14° 0.59 .70 .70 .46 .40 .327 .23 .20 .11 .06	16° 0.50 .7462 .53 .47 .33 .29 .29 .29 .20 .1052	180 	20°
0.19 b/2	7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-1.46 -1.34 -1.10 74 62 51 40 31 08 03	1.59 1.28 1.88 1.43 1.08 1.05	11.43 11.43 11.43 11.43 11.43 11.43 11.50 11.50 11.50	435 975 82 8758 447 11111158	-1.65 -1.66 -1.66 -1.95 -1.95 -27 -27 -20 -1.17	1344 48554 \$ 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	.51 .36 .22 .10 .07 .06 .08	.68 .48 .39 .19 .13	.70 .59 .46 .27 .70	.75 .67 .55 .35 .25 .16 .16	.79 .70 .57 .37 .27 .17 .17 .17	.61 .74 .62 .42 .31 .19 .16
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	67 -2.05 -1.67 -1.45 -1.27 -1.12 96 73 55 45 24 07	-1.40 -2.75 -2.11 -1.61 -1.54 -1.33 -1.14 84 74 60 46 37 07	-2.36 -3.53 -2.57 -2.11 -1.51 -1.28 97 81 65 50 39 25 07	-3.34 -3.01 -3.01 -2.40 -1.66 -1.39 -1.03 86 55 45 45 45	-3.97 -4.66 -3.21 -2.53 -2.10 -1.70 -1.39 -98 77 60 50 14 35 27	4.74 -3.48 -3.48 -2.21 -1.42 -99 -80 -72 -59 -80 -72 -89 -89 -89 -89 -89 -89	.61 .57 .37 .29 .23 .18 .12 .10	.56 .65 .49 .40 .34 .27 .21 .16	.42 .70 .5% .51 .44 .35 .29 .25	.26 .70 .67 .59 .51 .42 .34 .28	.12 .70 .71 .64 .56 .46 .36 .30	05 .68 .76 .69 .61 .51 .34 .21
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 60.0 90.0 95.0	-1.16 -2.59 -1.82 -1.59 -1.40 -1.18 -1.03 54 54 54 54 22 05	-2.27 -3.48 -2.34 -1.98 -1.71 -1.43 -1.22 	-3.63 -4.49 -2.88 -2.35 -2.00 -1.63 -1.37 82 64 49 36 24 07 01	-4.75 -5.15 -3.23 -2.54 -2.14 -1.67 -1.38 -88 -80 -73 -32	-5.45 -5.42 -3.30 -2.46 -2.09 -1.20 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03	-6.03 -5.09 -2.96 -2.00 -1.73 -1.52 -1.43 -1.23 -1.09 94 76 59 44 39	.53 .55 .40 .30 .25 .17 .15 .11 .11	.37 .59 .50 .40 .35 .26 .22 .16 .15	.09 .58 .57 .49 .43 .35 .29 .21 .19	15 .56 .59 .49 .39 .32 .21 .17	-34 .53 .66 .59 .53 .42 .34 .21 .17	53 .50 .68 .63 .57 .45 .37 .23 .17
0.44 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-1.76 -2.90 -2.04 -1.79 -1.21 -1.05 67 53 42 06 01	-3.18 -3.86 -2.61 -2.15 -1.81 -1.22 -90 -1.56 -1.30 -1.56 -1.30 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1	-4.94 -4.91 -3.18 -2.54 -2.10 -1.62 -1.34 99 76 59 45 30 18		-3.71 -1.75 -1.45 -1.24 -1.07 -1.06 -93 -79 -60 -49 -36 -31	-3.63 -1.49 -1.41 -1.33 -1.27 -1.10 -1.12 -1.15 -1.94 79 60 49 37	.42 .63 .41 .30 .15 .10 .09 .09 .09	.08 .62 .64 .53 .42 .25 .17 .14 .12 .19	-\$1 .52 -71 .62 .54 .35 .23 .19 .16 .15 05	-30 .60 .75 .65 .75 .35 .19 .14 .11	28 .59 .76 .68 .57 .37 .25 .19 .13 .10	-, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -, \(\) -,

TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Concluded (b) α_u = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

	Per-			Upper	surface							surface		
Spanwise stations	cent chord				fattack]				fattack		
	0	-0.84	12° -1.73	_2.83	-3.33	-3.93	20° -4.71 -1.80	1	10°	120	140	16°	180	200
0.56 b/2	1.5 10.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	44444444444444444444444444444444444444		-3.74 -3.62 -1.85 -1.51 -1.97 -1.48 -1.36 -1.00 -1.00	4.05 4.25 4.25 4.25 4.25 4.25 4.25 4.25 4.2	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-4.80 -3.17 -2.54 -2.08 -1.65 -1.33 99 77 41 32 29 19		0.61 .55 .37 .29 .24 .18 .15 .11	0.55 .62 .49 .40 .34 .26 .22 .19 -14 .10	0.39 .68 .59 .50 .43 .35 .29 .24 .16 .11	0.27 .69 .54 .47 .38 .32 .27 .20 .18	0.14 .68 .58 .52 .36 .30 .30 .19 .12	-0.05 .66
0.6H b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 40.0 50.0 60.0 70.0 90.0 90.0	69	91.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55 11.55		1.59 1.27 1.27 1.14 1.14 1.59 1.53 1.10 1.00 1.00	-5. rd -5. 29 -1. 64 -2. 79 -2. 52 -1. 44 -1.52 -1.11 79 54 34 20 14 10	7.13 7.99 7.99 7.99 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.5		.53 .53 .53 .28 .25 .19 .16 .15 .11 .13	.36 .56 .56 .37 .32 .26 .21 .18 .16 .15 .11	.08 .57 .52 .14 .39 .31 .27 .21 .18 .16 .12	-20 -53 -56 -49 -43 -35 -30 -23 -20 -16 -11	50 .46 .57 .52 .46 .40 .33 25 .21 .17 .10	87 .37 .59 .55 .51 .43 .36
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	-1.24 -2.27 -1.62 -1.39 -1.24 -1.03 89 48 35 27 16 02	-2,45 -3.05 -2.15 -1.77 -1.56 -1.28 -1.09 53 40 29 15 02	-3.92 -3.87 -2.67 -2.14 -1.83 -1.47 -1.22 -73 -58 -42 -28 -14 -04 -03	-5.27 -4.60 -3.09 -2.83 -2.05 -1.63 -1.34 76 59 42 26 13 08 06	-6.72 -5.35 -3.50 -2.72 -2.25 -1.78 -1.44 80 58 40 26 13 12	-1.63 -1.64 -1.62 -1.64 -1.57 -1.57 -1.2 99 86 73 59 44 37		.56 .52 -36 .27 .24 .18 -14 .14 .13 .12 .11	.42 .55 .36 .31 .25 	.19 .57 -50 .43 .37 .30 	09 .53 55 .48 .43 .35 .25 .22 .19 .11		
0.94 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	61 -1.62 -1.34 -2.43 -1.0084674639302212 0 .05	-1.61 -2.28 -1.81 -1.28 -1.04 85 53 43 23 12 01	-2.88 -3.02 -2.27 -1.83 -1.51 -1.21 -97 -39 -45 -34 -23 -11 -01		-5.61 -4.36 -3.09 -2.41 -1.93 -1.50 -1.21 65 48 -33 -20 -112 -09 08	-5.48 -3.94 -2.65 -1.88 -1.18 -1.05 79 66 57 40 33 29		.56 	.52 	.33 -51 .42 .37 .30 .21 .16 .14 -09 .07	.11 -55 .51 .42 .35 .27 .19 .16 -10 .07	-18 -57 -54 -46 -40 -30 -22 -17 -10 -06 -03 -01	21 21 57 -54 -46 -40 -31 -23 -19 09 -09 -09

大丁の一般の 一次大丁の大田 田田 こうこうち

TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED (a) α_u = -2°, 0°, 2°, 4°, 6°, 8°

0	Per-			Upper	surface			П				aurface		
Spanwise stations	cent chord	-20	00	Apgle 20	of attach	60		[-5 ₀	O ^O	Angle o	f attack	1 20	80
0.10 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.42 .39 .16 .03 -05 -13 -19 -25 -26 -26 -26 -26 -26	0.55 .04 .01 -119 -25 -30 -35 -35 -35 -35 -35 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36	0.64 -06 -16 -29 -34 -39 -42 -43 -43 -35 -35 -36 -01	0.67 16 36 49 50 54 56 57 37 37 37 37	0.65 41 60 70 69 68 70 77 68 66 61 39 30 09	8° 0.587082959086848678767736281106		-0.35 -53 -53 -45 -43 -41 -35 -27 -27 -22	-0.10 31 36 34 34 32 30 26 19	0.14 09 21 22 25 26 19 01	0.34 .10 03 06 09 13 15 11 04	60 	0.63 .42 .24 .17 .15 .08 .04 .03 .01 .05
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.52 .41 .11 -08 -21 -34 -38 -34 -31 -29 -24 -14	.65 .02 .09 .26 .39 .52 .41 .33 .29 .20	.70 04 33 49 60 78 55 52 44 37 31 22 07	64 37 63 73 82 1.00 48 55 43 34 22 09	-53 -73 -97 -99 -1.04 -1.23 -99 -57 -63 -48 -36 -23 -09 -03	.37 -1.02 -1.31 -1.33 -1.45 -1.25 76 61 65 32 20		42 57 56 45 49 59 39 39	09 28 55 59 51 59 33 17	.20 .01 .22 .79 .46 .32	.43 .21 01 24 61 26 14 04 .01	.59 .40 .17 .05 .36 .20 .09 .01	.69 .55 .34 .11 .13 .11 .05
0.31 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 90.0	.29 .29 .01 10 26 31 33 34 33 27 29 01	14 -16 -26 -34 -44 -45 -39 -35 -30 -29 -01	54 -07 -38 -49 -54 -61 -58 -53 -45 -37 -31 -24 -07	.56 35 67 79 81 87 88 81 70 49 43 35 25	.52 64 94 -1.03 -1.05 -1.16 -1.11 99 \$1 34 25	45 87 -1.18 -1.28 -1.30 -1.36 -1.37 -1.30 -1.07 81 51 37 27 16		58 81 90 78 59 50 38 24	31 54 50 50 45 40 37 34 25	23 30 31 30 27 26 21	.26 .03 11 15 15 16 17 16	.04 .04 .01 .01 .04 .06 .08	.58 .39 .20 .13 .10 .05 .01
0.375 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.23 .39 .16 .02 .13 .23 .30 .37 .37 .32 .29	- 45 - 22 - 03 - 21 - 31 - 45 - 45 - 49 - 44 - 36 - 30 - 22 - 08 - 01		.59 - 61 - 80 - 86 - 97 - 96 - 61 - 36 - 31 - 21 - 02	.50 91 90 -1.06 -1.19 -1.25 -1.26 52 41 36 06	.35 -1.15 -1.27 -1.31 -1.29 -1.25 -1.22 84 71 63 56 50 31		80 -1.06 98 75 61 55 32 17	38 60 59 51 45 35 20 15	.01 23 34 35 35 35 35 06	.30 .06 09 15 18 21 22 15 01		.59 .59 .51 .22 .13 .08 .01 .01 .04 .02
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 60.0 90.0 95.0	.38 .40 .14 07 18 36 40 34 30 25 18	. 56 . 19 - 06 - 28 36 56 54 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 38 - 38 - 38 - 38 - 38 - 38 - 38 - 38 -	.64 14 36 65 84 86 70 48 44 38 18 03	.64 76 73 91 -1.01 -1.15 -1.21 -1.06 40 46 39 18 04	.49 97 -1.09 -1.16 -1.24 -1.22 -1.21 -1.05 89 69 92 36 25 14	.32 -1.18 -1.24 -1.14 96 86 83 80 75 67 77 90 39		66 95 80 71 29 37 13 15 15 12	26 51 60 49 35 44 45 43 34	.14 14 26 59 71 75 38 20 06 01	01 19 45 66 16 08 01 05	.60 .40 .20 .03 .22 .36 .35 .05 .05	.68 .54 .35 .17 .06 .21 .11 .06 .07 .01

TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_{\rm u}$ = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

Spanvise	Per-				eurface			Γ				surface		
stations	cent chord	ەن-	a0		f attack	7.0	- 0		-20	50		of attack		00
0.56 b/2	0 1.5 1.0 10.0 15.0 20.0 40.0 50.0 70.0 80.0 90.0	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	00 0.43 110 110 113 113 113 113 113 113 113 11	0.51 31 35 35 35 36 36 32 32 32 32 32	0.55 35 70 77 82 82 31 31 31 31 35 31	60 0.51 55 74 85 93 -1.00 -1.09 89 81 32 24 01	8° 0.45 1.79 1.19 1.19 1.19 1.19 1.19 1.38 1.38 1.36 1.36 1.36 1.36 1.36 1.36 1.36 1.36		-22 -0.88 -1.00 -1.88 -1.00 -1.88 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1.49 -1	0° -0.37646961524333250403	20 30 30 35 37 27 22 20 11 0	0.24 01 14 15 14 12 11 08 01	0,40 .16 04 05 05 05 05	80
0.68 b/2	0 1.5 7.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19	1000 1000 1000 1000 1000 1000 1000 100	100 100 100 100 100 100 100 100 100 100	STORY SEE SEES SEE	- 70 - 23 - 57 - 71 - 84 - 78 - 84 - 75 - 75 - 75 - 75 - 75 - 75 - 75 - 75	-552 -184 -1.91 -1.01 -1.01 -1.98 -1.85 -1.24 -1.05 -1.05	175 175 199 199 199 1199 1199 1199 1199		-1.10 -1.25 -1.10 -1.01 -1.86 30 08	73 92 79 70 54 3- 21 05 .01	20 35 35 31 24 7	-,27 -,01 -,15 -,13 -,11 -,07 0 -,05 -,12 -,12	.40 .20 01 02 03 01 04 .06 .10	150 150 150 150 150 150 150 150 150 150
0.80 b/2	0 10.0 10.0 15.0 20.0 30.0 50.0 50.0 50.0 50.0 50.0	20 10 10 10 10 10 10 10 10 10 10 10 10 10		1446.1446.1496.1000 111111111111111111111111111111111	- 28 - 25 - 25 - 25 - 25 - 25 - 25 - 25 - 25	-52 -62 -90 -90 -97 -94 -88 -76 -42 -30 -119 -111 -01	-39 -8" -1.04 -1.01 -1.12 -1.02 -1.01 -38 80 42 49 27 11		80 74 74 70 74 54 54 35 27 18 10 03	89 86 69 52 25 10 04 03 .08 .10	35 35 31 25 18 02 .03 .06 .10	.23 .02 09 10 09 06 .04 .04 .06 .13	.42 .22 .06 .01 .02 .01 .07 .07 .09 .10 .10	.50 .50 .50 .50 .50 .50 .50 .50 .50 .50
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.51 .35 .20 .09 .01 06 15 18 21 17 14	.20 .42 .24 .10 01 16 21 21 22 16 13 12 06	.50 .22 .01 12 21 28 31 33 31 26 21 18		.59 53 66 79 89 81 75 69 21 16 11 03			-,48 -,45 -,44 -,41 -,34 -,34 -,28 -,24 -,19 -,16	-1.07 94 89 5t 32 26 14 07 .05 .09 .11	504137322721060108 -13 -15 -16	.10 06 12 13 11 09 04 02	.36 .04 .04 .00 .02 .02 .06 .06 .12	.47 22 .14 .08 .05 .03 .03 .03 .03 .05 .06 .06

TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm u}$ = 10°, 12°, 14°, 16°, 18°, 20°

Spanwise	Per-			Upper	ur face			Г			Lower	urface		
stations	cent chord	100	120	Angle of	160	180	200		10 ⁰	120	Angle of	attack 16 ⁰	18°	a. U
0.10 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	10° 0.49 -1.01 -1.05 -1.17 -1.11 -1.099495575471412218	0.39 -1.19 -1.25 -1.34 -1.27 -1.27 -1.04 99 79 63 71 61 39 39	0.26 -1.37 -1.49 -1.40 -1.40 -1.40 -1.90 94 94 74 54	0.14 -1.41 -1.41 -1.30 -1.21 -1.19 -1.10 -1.01 33 97 45 70 61	180 0.01 -1.29 -1.27 -1.21 -1.20 -1.17 -1.16 -1.12 -1.07 -1.02 97 90 73	20° 0.11 -1.44 -1.43 -1.37 -1.37 -1.34 -1.32 -1.76 -1.71 -1.16 -1.04979876	!	0.73 .54 .35 .28 .23 .15 .11 .09 .06 .09	0.79 .64 .36 .31 .24 .14 .14 .14	0.84 .72 .53 .43 .38 .19 .14 .13	0.89 .79 .60 .50 .44 .35 .29 .25 .19	0.91 .85 .56 .51 .41 .35 .29 .23 .20	0.94 .91 .73 .66 .57 .46 .46 .24 .24 .24
0.19 b/?	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	.18 -1.71 -1.40 -1.27 -1.25 -1.18 -0.4 -1.13 -1.04 -1.74584433	.01 -1.30 -1.32 -1.07 -1.07 -1.08 -0.33 -1.08 -1.06 96 96 96 96 41	01 -1.05 -1.15 -1.00 -1.00 -1.00 -1.00 -1.00 -1.05 09 99 99 59 59	37 -1.14 -1.04 % /3 .01 % /6 /91 % /93 60	55 -1.07 -1.00 98 98 98 -1.00 -1.00 -1.00 92 91 75 06	77 -1.19 -1.15 -1.11 -1.11 -1.11 -1.11 -1.12 -1.13 -1.11 -1.00 33 36 86		.74 .666 .07 .04 -03 C .09 .04	.75 .73 .56 .32 .10 .04 .04	.74 .78 .85 .86 .10 .67 .67	.74 .72 .55 .36 .19 .12 .04 .33	.63 .84 .03 .44 .16 .05 .04	.64 .87 .84 .70 .90 .32 .22 .10 .77
0.31 t/2	0 1.5 4.0 7.0 10.0 15.0 20.0 80.0 50.0 60.0 70.0 80.0 90.0	.36 -1.02 -1.34 -1.43 -1.44 -1.38 -1.37 -1.19 -1.00 91 61 49 34 25	.29 -1.10 -1.36 -1.29 -1.31 -1.22 -1.15 -1.0149750560534040	.1' -1.24 -1.24 -1.18 -1.13 -1.14 -1.11 -1.0201775066594350	.10 -1.25 -1.26 -1.15 -1.14 -1.10 -1.0093817974677676	04 -1.14 -1.17 -1.10 -1.04 -1.04 -1.03 94 93 91 91 76 76 76	51 95 31 92 82 81 70 77 75 75 68 69		.66 .44 .27 .27 .11 .01 .03 05	.70 .57 .34 .29 .25 .18 .10 .10 .10	.75 .65 .36 .30 .24 .11 .10	.50 .70 .53 .45 .30 .31 .14	.83 .78 .53 .45 .35 .45 .45 .45 .45	.81 .83 .67 .52 .40 .35 .35 .08
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.22 -1.30 -1.32 -1.26 -1.21 -1.06 -1.01 .03 .81 72 66 55 42	.07 87 38 95 95 95 75 76 70 66 56 56	10 81 30 79 79 79 90 .02 76 74 66 60	23 80 75 76 76 77 77 77 75 75 75 66 65	41 81 81 75 75 75 75 74 74 71 71 71	51 74 75 74 73 73 72 72 72 72 72 70 69		.64 .49 .30 .21 .15 .07 .03 .04 .05	.65 .56 .38 .28 .22 .13 .06 .05	.67 .61 .45 .35 .29 .19 .09 .09	.66 .66 .66 .41 .34 .24 .15 .01	.64 .69 .57 .47 .40 .29 .20 .04	.63 .72 .62 .64 .46 .36 .26 .01
0.44 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 60.0 90.0	.14 91 93 86 75 75 75 75 75 76 59 59 55 43	.03 75 74 72 71 69 69 68 66 66 54 44	13 74 75 75 69 69 67 67 61 57 50 47	29 73 73 72 68 69 69 70 68 66 66 59 52	- 45 - 70 - 70 - 69 - 69 - 69 - 69 - 70 - 69 - 67 - 63 - 60 - 55	61 69 70 69 69 69 70 69 65 64 61		.70 .61 .42 .27 .05 -14 -11 -08 -07 -06	.70 .67 .51 .35 .14 .09 -10 -10 09	.69 .71 .58 .42 .23 .01 .08 .08 .11 .10	.67 .75 .64 .49 .31 .06 .03 06 10	.63 .78 .70 .26 .39 .13 .01 .04 .08	.59 .90 .76 .63 .46 .20 .01 05 08

TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED - Concluded (b) α_u = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

	Per-			Upper	surface			П			Lover	surface		
Spenvise	cent			Angle	f attack						Angle o	of attack		
stations	chord	10°	120	14°	16°	18 ⁶	200		10°	120	140	16°	180	50 ₀
	0	0.34	0.26	0.15	0.05	-0.05	-0.19							
	1.5	-1.04	-1.10	-1.22	-1.31	-1.46	-1.64		0.59	0.64	0.68	0.72	0.75	0.76
	4.0	-1.25	-1.34	-1.50	-1.59	-1.60	-1.69		•39	.46	٠53	-59	.66	-73
	7.0 10.0	-1.27 -1.26	-1.36 -1.34	-1.54 -1.50	-1.61 -1.56	-1.56 -1.56	-1.63 -1.63		.21	.28	.35	.41	.49	.56
J	15.0	-1.36	-1.39	-1.51	-1.56	-1.50	-1.58		.12	.20	.26	.34	.40	.48
	20.0	-1.31	-1.33	-1.42	-1.46	-1.41	-1.53		.ii	.16	.22	.28	-35	.42
0.56 b/2	30.0	-1.14	-1.06	-1.02	-1.20	-1.26	-1.42		.07	.10	.15	•55	.27	.34
	40.0	61	62	64	80	-1.00	-1.21		.04	.07	.11	.15	.19	.26
1	50.0	47	46	51	64	84	-1.02	ŀΙ	.02	-04	.07	.11	.15	•10
	60.0 70.0	41 36	41 38	48	55 50	66 58	76 65	i I	01	01	0	.03	.05	.08
	80.0	29	33	40	45	- 51	55	ΙI	.01	.01	õ	.01	.02	.04
	90.0	16	24	33	39	- , 44	45	ΙI	02	05	08	08	08	06
	95.0	11	20	29	35	39	40	Н	02	06	11	14	14	14
	0	.29	.19	.06	07	21	38	Н						
	1.5	-1.08	-,99	99	-1.00	93	-1.00	ΙI	.56	.59	-59	-59	.57	.54
	4.0	-1.11	-1.02	89	89	- 92	-1.01	ΙI	-40	.45	.50	٠53	-57	-59
	7.0	-1.09	91	84	87	90	96	il				•••		la la
1	10.0 15.0	-1.09 99	91 86	85 83	87 86	90 87	99 96	!	.24	.29 .19	.34	.39	.43	.47
	20.0	91	- 85	83	95	88	96	ΙI	.ii	.16	.20	.24	.28	.31
0.68 b/2	30.0	79	78	76	8ó	83	91	H	.07	.10	.13	.16	.20	.24
	40.0	71	74	74	76	81	89	ll	.06	.07	.09	.11	.14	.17
1	50.0	63	66	65	-,64	74	80	ΙI						
	60.0	54 46	61	56 51	61 54	73 62	80 64		.08 .06	.06	.06	.06	.07 .01	.08
	70.0 80.0	38	51 45	49	- 52	- 60	62		.06	.04	رن.	01	03	04
1	90.0	26	34	37	40	-,44	42	H	0.	05	10	12	15	17
	95.0	24	• 30	37	41	47	49	П	06	14	17	22	25	29
	o	.16	.05	11	25	39	55	H						
	1.5	-1.21	-1.27	-1.05	96	-1.01	-1.03		-57	-59	.60	-59	.58	- 55
	4.0	-1.35	-1.25	-1.06	98	-1.03	-1.04	1	.40	.45	.49	-53	.54	.56
	7.0	-1.26	-1.19	-1.05	95 96	-1.01 -1.01	-1.01 -1.01	1	.25	.29	.34	.37	.40	.44.
	10.0	-1.27 -1.20	-1.16 -1.01	-1.02 97	90	97	99		.16	.20	.25	.29	.32	.34
	20.0	-1.06	98	- 96	90	97	99		.14	.16	.20	.24	.27	.29
0.80 b/2	30.0	87	68	86	84	- 92	94		.09	.10	.13	.15	.18	.20
	40.0	79	82	83	85	90	94			• • •	• • •			• • •
	50.0	69	74	76	81	84	89		.07	.06	.07	-08	.09	.09
	60.0 70.0	61	67 60	72 66	79 73	81 74	85 76		.08	.06	.06 .05	.06	.07 .03	.06
1	80.0	51 38	51	61	66	66	69	ı	.08	.04	رن،	01	02	05
	90.0	26	- 42	54	57	59	61	ı	.05	02	08	10	11	15
	95.0	19	36	49	52	54	%	lí	.01	09	16	18	20	22
	0	.28	.19	.04	11	25	35	H						
	1.5	-1.34	-1.29	-1.15	-1.04	- 95	80	ŀ	.52	.56	.56	.56	-55	.52
	4.0	-1.28	-1.23	-1.20	-1.11	-1.00	82	l	• • •		• • •			
1	7.0	-1.20	-1.22	-1.11	-1.03	94 96	80 81	l	.29 .20	.33 .24	.37 .28	.40	, 44 , 35	.45
I	10.0 15.0	-1.20 -1.16	-1.18 -1.01	-1.07 96	-1.03 95	90 91	76	l	.12	.15	.20	.30	.35 .26	.29
	20.0	-1.04	94	93	93	91	77	l	.10	ü	.14	.18	.20	.21
0.94 b/2	30.0	61	61	63	82	81	72	l	.05	.05	.07	.10	.10	.13
	40.0	66	75	78	81	80	72		.03	.01	.02	-04	-05	.05
	90.0	51	64	71	74	75	69		.02	.01	.01	.01	.01	01
	60.0		58 49	67	72 65	72 67	67 63	l	.04	.01	02	05	06	10
	70.0 80.0	26 17	39	59 52	59	61	60		.06	.01	+.05	07	10	16
	90.0	09	29	43	51	55	54		.05	02	10	14	18	24
	95.0	05	24	36	51 46	51	51	H	.03	07	16	22	27	32
		·	L											

TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED

(a) α_u = -2°, 0°, 2°, 4°, 6°, 8°

Supposed on	Per-			Upper !	rface					Lover 1	urface		
Spanwise Stations	cent chord			Angle of	attack 40	60	80	Ŷ	00	Angle of	attack ko	60	80
0.10 b/2	0 1.5 4.0 7.0 10.0 20.0 20.0 30.0 50.0 70.0 80.0 90.0	0.50.7.9.5.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	0 5 9 8 8 2 8 2 8 2 8 2 8 2 8 2 8 2 8 2 8 2	68 158 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.72 01 23 36 39 47 52 53 57 67 76 20 15	0.72 21 31 54 55 57 60 61 61 61 75 27	0.68 11 76 71 69 67 79 65 79 66 79	9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.01	0.184	0.36 .13 0 04 06 11 16 23 36 27	0.51	0.64 .41 .24 .17 .13 .06 .02 04 05 .01
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	9925 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	**************************************	7523398 75233382136	.74 17 44 54 62 83 67 70 71 73 32 17	-66 -170 -170 -180 -198 -178 -178 -180 -178 -180 -180 -180 -180 -180 -180 -180 -18	5.66 8.96 8.12 1.75 8.68 8.55 8.68 8.55 8.68 8.55 8.55 8.5	1.36	.06 11 25 59 58 51 51 51 51	ं ने स्टूडिंग १०० व	.45 .25 .06 16 53 86 37	1989 5 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	.69 .54 .33 .11 23 46 05 04 0
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	. 35 . 26 . 13 . 13 . 13 . 13 . 13 . 13 . 13 . 13	- 15 - 15 - 15 - 15 - 15 - 15 - 15 - 15	.51 -01 -33 -51 -68 -75 -76 -76 -76 -76 -29 -30	.57 15 47 60 67 77 82 89 91 93 90 61 24 13	.58 35 66 76 81 97 -1.04 -4.09 -1.04 91 56 42 22	553 153 153 153 153 153 153 153 153 153	-80 -80 -87 -76 -76 -79 -46	-23 -50 -66 -63 -51 -38 -37 -35 -49	11 11 11 11 11 11 11 11 11 11 11 11 11	.16 -06 -18 -20 -19 -17 -20 -20 -34 -30 -10	.36 .14 .03 .06 .06 .08 .11 .14	.50 .30 .30 .07 .05 .01 04 07
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	. 35 . 33 . 33 . 129 . 137 . 159 . 1	.48 .22 -01 -21 -33 -51 -51 -64 -76 -69 -66 -66 0	.59 .03 -40 -50 -68 -68 -83 -66 -17 -01	63 -120 -130 -130 -130 -130 -130 -130 -130 -13	-59 -52 -59 -76 -89 -1.00 -1.84 -69 -1.42 -35	576858866 BP88855	~85 ~85 ~85 ~85 ~54 ~15 ~15 ~12	~28 ~55 ~63 ~35 ~43 ~43 ~44 ~09	.01 -23 -134 -134 -135 -135 -135 -135 -135 -135 -135 -135	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	.44 .21 .04 08 14 20 36 42	.54 .35 .16 .07 .02 -05 -11 -30 -36
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 50.0 90.0 90.0	-54 -36 -10 -10 -21 -43 -70 -70 -64 -21 -23 -23 -23 -23	.64 .20 -25 -27 -27 -28 -28 -76 -76 -29 -19 -29	70524567784 		.63 -29 -71 -81 -83 -83 -66 -67 -66 -66 -69 -43		-34 -62 -72 -35 -37 -47 -47	107 6 7 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5	200 200 200 200 200 200 200 200 200 200	.41 .16 .01 -14 -78 -77 -78 -77 -78 -71	.58 .35 .01 .01 .29 .86 .02 .02	.66 .49 .11 .12 .60 .60 .60 .60 .60 .60 .60 .60 .60 .60

TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_u = -2^\circ$, 0° , 2° , 4° , 6° , 8° - Concluded

_	Per-			Upper	surface				· · · · · · · · · · · · · · · · · · ·	Lover	surface		
Spanvise stations	cent chord			Angle o	f attack					Angle	of attack		v=
***************************************	cnord	_00	O _O	ဥ၀	¥0	60	go	e°	O°	20	μo	6°	80
0.56 b/2	0 1.5 4.0 70.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	0.25 01 01 37 38 41 52 35 25 25 25 25	0.38 -115 -150 -143 -57 -56 -63 -156 -156 -174 -174 -102 -06	0.47 02 29 44 73 77 80 72 12 12 11 01	0.54 1.149 1.156 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1.189 1	0.54 35 55 68 75 91 96 -1.02 36 36 36 36 36 36 36 3	0.51 53 71 79 86 -1.00 -1.04 -1.09 1.05 89 51 41 29 18	-0.60 80 89 99 99 59 59 59 57	-0.34 60 72 63 53 54 54 64 64	-0.11 39 51 45 36 33 24 15 03 .06	0.10 15 26 27 23 23 20 19 14 04	0.28 .04 10 14 13 14 14 17 05 .01	0.41 .17 .01 .04 04 06 09 10 12 07 10 08
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0	.11.44 .15.09 .15.45 .15.88 .16.104 .104 .11.04	99577962954954 111111111111111111111111111111111	- 48 - 13 - 19 - 150 - 159 - 155 - 155 - 156 - 126 - 120 - 120 - 120	.57 08 41 56 66 77 81 80 70 49 29 17 10	.58 31 63 76 85 87 86 52 45 36 31	.53 51 84 99 99 99 75 65 68 51 41	8; 99 -1.05 -1.10 -1.10 -1.5; 65 04 .07	-54 -75 -84 -85 -42 -14 -00 -09 -12	21 42 43 44 37 :3 15 01 .04	.10 12 26 26 19 11 .01 .06 .06	.27 .06 07 14 13 03 01 .04 .05	.49 .19 .04 .05 .07 .07 .06 .01 .01 .01 .05 .01
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.41 .49 .28 .13 .04 06 14 16 21 23 20 18 16	45771389188899188991919199	.62 -13 -12 -28 -37 -39 -35 -35 -34 -13 -13 -13	.65 14 36 56 70 77 73 71 59 29 15 04	58 - 42 - 573 - 89 - 93 - 86 - 59 - 37 - 24 - 39	.49 65 40 96 -1.06 -1.01 74 61 51 40 28 17	73 80 61 55 50 45 24 20 14 10	73 75 76 74 64 23 01 04 09	हिंदी विस्तर है है है है से स	निहास है		.43 .64 .66 .00 .03 .01 .05 .06 .07
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.11 .50 .34 .19 .09 01 08 19 22 29 26 21 17	.28 .42 .23 .07 -01 -18 -26 -29 -29 -19 -06 .07	.49 .21 01 16 27 31 37 37 39 08 08	.61 09 30 48 55 57 69 30 14 10	-59 -38 -53 -69 -82 -81 -74 -70 -45 -30 -18 -19 0	.54 61 74 86 87 86 87 51 51 36 30 21	-57 -54 -49 -40 -40 -29 -27 -16 -11 -06	99 99 95 57 24 10 04 07 -12 -15 -17	751 745 745 739 733 720 710 705 711 715	701 715 720 720 716 714 710 704 707 711	.24 .01 09 09 10 09 10 09 09 09 09 09 09	

TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm u}$ = 10°

Spezwiee	Por-		Upper	surface of attack		T	Lover	surface of attack	
Stations	cent	10°	Angu-	a accaex		100	- Angere	OI ACCREA	
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 60.0 70.0 80.0 90.0 95.0	0.61 66 75 87 89 83 81 76 74 74 94				0.72 .53 .27 .22 .14 .09 .05 .01			
0 .19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.39 86 -1.12 -1.17 -1.19 -1.29 -1.31 -1.10 95 85 41 33 27				.75 .64 .86 .24 08 11 04 02 0			
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.50 69 96 -1.10 -1.11 -1.10 -1.96 88 84 77 73 64				.61 .43 .24 .16 .14 .06 .02 02			
0.373 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 47.0 50.0 60.0 70.0 80.0 90.0	.40 91 -1.09 -1.09 -1.03 -1.03 77 70 66 64				.61 .45 .26 .16 .10 .02 05 25 26			
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0	. 386 -1.00 -1.00 -1.069 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.066 -1.06				.70 .58 .41 .24 -01 -37 -58 -10 -14 -,12			

TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPEILERS REMOVED - Concluded (b) $\alpha_{\rm U} = 10^{\rm O}$ - Concluded

	Per-		 Upper	surface	 			 Lover	surface	
Spanwise stations	cent		 	f attack					f attack	
Benelons	chard	10°				\Box	100			
0.56 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 60.0 70.0 90.0	0.46 69 87 94 98 -1.10 -1.12 -1.16 -1.14 -1.10 71 50 40				-	0.50 .77 .10 .04 .01 03 05 08			
0.68 b/2	0 1.5 4,0 7,0 10,0 15,0 20,0 30,0 40,0 50,0 60,0 70,0 80,0 90,0					-	.47 .27 .03 .03 .001 05 06			
0.30 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	.37 81 99 -1.06 -1.05 -1.05 -1.05 -1.05 -1.50 71 50 71 51 45				-	.48 .28 .11 .04 .02 03 04 01 0			
0.9h b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 90.0	44 91 99 99 99 79 79 79 79 75 75				-	.18 .10 .04 0 05 07 08 06 09 08			

TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED

(a) $\alpha_u = -2^\circ$, 0° , 2° , 4° , 6° , 8°

	Per-	γ						_						
Spanvise stations	cent			pper surf glo of at				1			over surf			
	chore	⊸°	00	20	40	I 6º	80	1	⊸°°	l o°	20	100	6°	A°
0.10 ь/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	0.16 .3k .1k .02 09 1k 21 21 21 15 15 11 03	0.kg .17 0k 13 22 29 31 30 26 20 20 17 13 05	0.54 04 27 36 40 42 36 31 25 23 20 16 04	0.54 33 46 52 52 51 45 39 31 26 24 17 16	0. 45 65 66 66 66 66 66 62 35 34 35 20 20 05	0.22 -1.02 94 86 84 77 61 50 40 34 29 06		-0.69 61 50 41 32 25 20 12 06	-37 -37 -36 -30 -25 -19 -14 -07 -02	0.01 13 21 25 19 11 09 04 .01	0.25 .07 07 11 09 07 04 .01 .04	0.43 .25 .06 0 .01 0 .01 .05 .06	0.55 .39 .19 .10 .10 .07 .06 .09 .10
0.19 b/2	0 1.5 k.0 7.0 10.0 15.0 20.0 30.0 90.0 90.0 90.0 90.0	.06 .37 .08 .02 04 15 23 24 19 16 15 11 01	.39 .22 12 16 20 30 31 24 21 17 13 03	14 37 39 43 36 29 24 20 15 03	.52 53 66 56 56 58 35 27 27 23 15 03	.30 99 97 77 75 73 56 51 40 31 25 27 03	10 -1.55 -1.34 -1.03 97 72 65 57 35 35 28 18		75 65 52 43 37 26 20 08 02	31 36 32 30 25 21 14 05 .01	.04 10 16 16 15 11 08 0 .04	.30 .11 01 04 05 05 03 .03 .06	.47 .28 .12 .07 .04 .03 .04 .05 .06	.55 .41 .24 .15 .13 .09 .08
0.31 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	.05 .13 .16 .05 03 11 14 17 20 20 17 15 11	.39 .22 03 15 20 27 27 27 26 22 14 02	.54 09 30 36 39 40 40 37 36 31 26 21 15	.50 47 59 59 57 52 45 37 31 24 16 01	-35 -95 96 86 79 74 66 51 43 26 19 02	23 -1.49 -1.30 -1.15 -1.03 90 65 57 49 38 28 18 01		76 68 50 45 35 27 20 11	30 36 31 29 25 18 13 07	.06 07 13 15 12 10 06 06 09	.35 .16 .03 02 02 02 02 01 .07	.50 .33 .15 .08 .07 .04 .06 .09	.55 .45 .19 .15 .11 .10 .10
0.377 3/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 70.0 80.0 90.0	.02 .31 .21 .05 03 15 15 15 15 15 15 15	39 1901 100 100 100 100 100 100 100 100 1	54.77.99.33.34.0 1.1.2.3.3.3.3.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	\$79866884 425887465	.20 -1.11 91 83 75 69 49 49 33 26 18 04	32 -1.7k -1.29 -1.18 -1.06 93 8k 96 46 36 36 29 19 04		24 67 51 36 36 36 26 02	29 35 30 28 28 28 18 19 03 01	.06 09 13 12 10 06 06 06 07	.36 .15 .04 01 01 01 0 .05 .06	.51 .35 .11 .10 .06 .06	.56 .45 .29 .21 .17 .13 .11 .11 .12
0.44 b/R	0 1.5 3.0 7.0 10.0 20.0 20.0 80.0 70.0 60.0 70.0 90.0 90.0	05 00 00 114 129 129 129 130 14	.37 .17 09 13 19 26 27 26 21 19 14 09	-54 39 39 49 49 34 36 26 26 27 26	.50 56 66 55 54 35 35 35 35 35 35	.21 -1.11 -989 -833 -76 -98 -140 -150 -150 -150 -150 -150 -150 -150 -15	31 -1.71 -1.33 -1.80 -1.09 93 83 86 46 36 27 16 00		83 70 51 35 87 80 11 06 01	32 40 32 28 23 17 14 07 03 .03	.09 08 13 14 19 09 07 01 .01 .09	.38 .14 .04 01 01 01 01 01 .04 .06	.53 .34 .18 .12 .10 .07 .07 .08 .09 .21	.96 .46 .29 .22 .18 .11 .11 .11 .13

TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_u = -2^\circ$, 0° , 2° , 4° , 6° , 8° - Concluded

	Per-			Upper	surface			Γ			Lover	surface		
Spanwiee stations	cont				of attack]			Angle	of attack		
	0	-0.11 .44 .23	0.3h .21 02	0.52 12 29	0.46 58 61	0.11 -1.12 95	-0.51 -1.78 -1.36		-2° -0.99 72	-0.41 43	0.04	0.35	0.52	0.56 .48
0.56 b/2	7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.10 0 08 09 14 17 17 15 13 10 01	12 18 22 23 23 24 22 20 16 11 01	35 40 39 36 33 29 24 20 14 02	61 59 56 44 40 35 28 15 05	89 83 74 56 57 40 32 25 16 06	-1.21 -1.09 93 79 63 55 45 35 26 16 01		53 45 35 26 18 11	36 29 23 18 11 06	14 15 12 09 05 02 07 .09 .10	.04 01 0 .01 .03 08 .10 .10	.18 .11 .10 .07 .08 .09	.30 .21 .20 .14 .13 .12
0.48 ъ/ 2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	.50 .26 .13 .05 02 09 13 14 15 11 09	.30 .01 07 11 15 20 24 22 21 17 15 11	026 30 36 34 33 34 30 26 21 18 02					-1.13 82 57 46 37 26 20 05 01 .03 .06	51 49 35 30 25 19 12 02 .01 .05	04 15 16 12 09 05 01 .04 .06	.30 .11 .02 02 01 01 01 01 05 .06 .08	.4A .32 16 .10 .09 .05 .05 .07 .07	.54 .48 .29 .20 .13 .11 .11 .11 .11 .10
0.80 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 70.0 80.0 95.0	18 .50 .31 .17 .09 .01 08 11 10 08	.72 .09 .08 .11 .11 .11 .11 .11 .11 .11 .11 .11 .1	.57 .02 17 29 29 27 27 27 18 12 19	- 149 - 149 - 149 - 147 - 145 - 135 - 131 - 121 - 15 - 105	199878716559573730251604	- 155 -1.55 -1.19 -1.06 97 84 74 51 43 34 26 03		-1.32 89 61 50 39 28 13 01 01	669 969 1.34 1.34 1.35 1.36 1.36 1.36 1.36 1.36 1.36 1.36 1.36	- 15 - 22 - 21 - 21 - 21 - 21 - 21 - 21 - 21		.13 .33 .07 .06 .04 .05 .08 .09 .10	.55 .42 .27 .18 .15 .11 .09 .09 .10 .10
O.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	82 .52 .36 .22 .13 .06 .03 0 08 11 09 06	07 .39 .19 .05 0 06 08 09 15 11 11	.40 .16 05 15 15 15 13 21 21 21 21 21	.5% 19 33 36 39 35 31 27 27 27 21 11	- 57 - 59 - 63 - 56 - 50 - 32 - 35 - 30 - 25 - 12 - 12 - 01	.09 -1.1h -1.01 79 66 97 42 41 34 29 13 01		-1.73 64 51 60 27 18 10	97 52 36 28 20 14 08	39 26 29 22 17 13 09 05 05	.07 06 10 10 06 05 05 01	.36 .36 .01 .01 .02 .03 .05 .05 .05 .05 .05	.53 .26 .19 .12 .10 .05 .05 .05

TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm U}$ = 10°, 12°, 14°, 16°, 18°, 20°

Doggarine	Por-			Upper							ourface		
stations	cent chord				f attack	18 ⁸			8	Angle o	f attack	180	20 ⁰
0.10 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	10 10 10 12 10 10 10 10 10 10 10 10 10 10 10 10 10	\$555728682525258868	14:25 -1:25 -1:88 -1:57 -1:39 -1:08 -1:50 -1:50 -1:50 -1:51 -1:06 -1:01	10 -1.92 -2.93 -2.19 -1.76 -1.31 -1.14 70 54 23 07 02	47.50 47.50 47.73 74.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73 77.73	-3.76 -4.15 -4.33 -1.96 -1.36 -1.36 99 75 45 10 05	0.62 .50 .30 .20 .15 .13 .11 .13 .14	.60 .40 .30 .28 .22 .20 .16 .17	0.60 .66 .39 .37 .28 .22 .22 .22	0.53 .70 .57 .45 .41 .34 .26 .29 .24 .25	0.40 .73 .64 .51 .48 .39 .33 .30 .29 .26	0.24 .73 .69 .59 .54 .44 .38 .33 .30
0.19 b/2	0 1.5 k.0 7.0 10.0 15.0 20.0 30.0 k0.0 50.0 60.0 70.0 80.0 90.0	66 -2.16 -1.69 -1.29 -1.26 -1.048473648736291603	-1.50 -2.93 -2.16 -1.66 -1.44 -1.25 -1.01 69 52 40 29 17 02	4.83 9.89 9.80 11.13 1.55 1.32 1.55 1.32 1.04 1.05		15.37 15.37 15.37 16.37 16.38 16.38 1.36 1.36 1.36 1.36 1.36	6.88 9.89 9.49 1.75 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.8	.56 .50 .26 .22 .16 .17 .11	.57 .43 .39 .30 .24 .20	.32 .59 .50 .43 .37 .30 .25 .20 .20	.10 .57 .59 .49 .42 .35 .30 	-17 -53 -59 -53 -59 -53 -49 -41 -35 -28 -25 -15 -06	53 .45 .63 .59 .54 .45 .40 .31 .29
0.31 b /2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 90.0 95.0	57 -2.13 -1.70 -1.44 -1.26 -1.05 93 75 62 26 28 15 0	-1.81 -2.91 -2.39 -1.81 -1.31 -1.11 86 99 99 97 10	-2.55 -3.68 -2.65 -2.13 -1.81 -1.48 -1.24 75 76 25 10	-1.03 -1.10 -2.11 -1.64 -1.34 -1.99 -77 -57 -39 -21 -05	-5.46 -5.40 -3.63 -2.81 -2.30 -1.82 -1.49 -1.05 79 56 35 21 15 09 10	-7.09 -6.10 -1.17 -2.01 -1.61 -1.76 -1.76 -1.79 -1.09 -1.19	.57 .54 .37 .29 .21 .19 .19		.16 .56 .52 .43 .39 .31 .24 .24	1h .50 57 .49 .44 .35 .30 .26		
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 70.0 60.0 90.0 90.0	-1.07 -2.42 -1.70 -1.47 -1.30 -1.11 96 63 50 39 39 19 04	-2.09 -3.29 -2.21 -1.83 -1.60 -1.34 -1.14 -82 -71 94 42 31 20 05	-3.82 -1.15 -2.68 -2.19 -1.96 -1.92 -1.97 -57 -57 -57 -39 06 0		-5.07 -3.60 -2.85 -2.85 -1.84 -1.90 -1.00 60 46 37 29 14	7.78 4.98 4.00 7.66 7.66 7.66 7.66 7.66 7.79 7.66 7.79 7.70 7.70 7.70 7.70 7.70 7.70 7.70		.36 .57 .45 .38 .33 .26 .22 .19 .17	.13 .54 .53 .43 .40 .32 .27 .21 .20	18 .50 57 .51 .85 .37 .31 26 .24	-,56 ,81 -,59 ,53 ,89 ,81 ,36 -,36 -,26 -,17	-1.00 .28 .60 .51 .52 .45 .39 -31 .27
0.44 9/2	1.5 4.0 7.0 10.0 15.0 20.0 30.0 60.0 70.0 80.0 90.0 97.0	-1.07 -2.37 -1.76 -1.72 -1.33 -1.11 97 79 63 39 16 01	-2.10 -3.21 -2.29 -1.92 -1.66 -1.31 -1.17 90 76 42 16 02	-1.85 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95		-6.16 -5.82 -3.75 -2.43 -1.89 -1.94 64 44 29 19 11	-7.55 -6.75 -1.27 -3.29 -2.68 -1.58 -1.64 -1.64 -1.61 -1.62 -1.62 -1.63 -1.63 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64 -1.64	.3 .3 .3 .3 .2 .2 .1 .1 .1 .1	.32 .78 .56 .57 .36 .36 .36 .36 .36 .21 .20 .19 .18	.06 .76 .73 .47 .39 .26 .27 .21	31 .50 .56 .70 .46 .37 .31 .29 .26 .24	76 .40 59 .54 .50 .48 .35 .31 .38 .26 	-1.31 .27 .78 .78 .54 .46 .39 .31 .88

TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Concluded (b) α_u = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

	Por-			Upper	surface			_			Lower	surface		
Spanwise stations	cent				of attack						Angle	of attack		
30201023	oheri	100	120	140	160	180	200	L	100	120	110	160	180	20°
0.56 b/2	0 1.5 10.0 10.0 15.0 20.0 30.0 80.0 90.0 90.0	-1.38 -2.49 -1.79 -1.53 -1.34 -1.11 95 75 62 51 39 28 16 01	-2.56 -3.40 -2.34 -1.54 -1.66 -1.35 -1.11 89 69 55 40 31 16	4.99 4.99 4.99 4.99 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1	-5.37 -5.15 -3.30 -2.61 -2.17 -1.69 -1.01 79 61 31 09 04	-7.12 -6.16 -3.85 -2.98 -2.44 -1.90 -1.50 83 63 37 26 15 09	-8.99 -7.14 -4.36 -3.32 -2.72 -2.04 -1.61 -1.1488715946352010		0.51 .55 .39 .31 .26 .20 .18 .16	0.30 .57 .46 .39 .34 .26 .23 .20 .19 .16	0.02 .58 .45 .40 .37 .27 .25 .21 .19	-0.3h .51 .57 .57 .51 .45 .37 .33 .29 .20 .15 .10	-0.82 .41 .59 .54 .50 .42 .36 .31 	-1.37 .28 .58 .57 .54 .39 .39 .35 .25 .16
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 70.0 70.0 95.0	-2.26 -1.79 -1.48 -1.31 -1.11 96 64 51 37 27 17 01	-3.09 -2.34 -1.63 -1.55 -1.55 -1.90 -1.69 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.89 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80 -1.80	1988 188 188 188 188 188 188 188 188 188	175724 15724 15724 1079 1080 1080 1080 1080	-5.69 -3.86 -2.95 -2.43 -1.91 -1.57 -1.13 78 51 19 14 12	-6.65 -1.39 -3.28 -2.64 -1.64 -1.08 -71 -34 -39 -29 -20		.52 .54 .38 .29 .25 .20 .16 .13 .12	.34 .57 .46 .37 .34 .26 .21 .19 .16 .15	.08 .58 .53 .46 .39 .31 .26 .21 .18 .15	27 -53 -56 -50 -54 -37 -31 -24 -20 -17 -11	71 .44 .58 .54 .48 .41 .34 .26 .22 .18 .10	-1.22 .31 .57 .56 .53 .45 .37 .29 .24 .19 .10
0.80 ъ/2	0 1.5 k.0 7.0 10.0 20.0 30.0 k0.0 50.0 60.0 70.0 80.0 90.0	-1.38 -2.86 -1.61 -1.30 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03 -1.03			5454335336F5536485866666666666666666666666666666666	7.53 7.52 7.52 7.52 7.80 7.80 7.80 7.80 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.5	-9.53 -6.44 -1.07 -3.09 -2.52 -1.96 -1.95 -1.96 -78 -36 -36 -36 -29 -24		.37 .28 .24 .18 .13 .12 .11	. 18 . 15 . 36 . 31 . 25 . 18 . 16 . 15 . 10 . 10	.21 .58 .51 .43 .38 .30 .22 .19 .17 .14	-07 -51 -49 -43 -35 -26 -23 -19 -10 -08	-, 11 -, 17 -, 59 -, 53 -, 18 -, 39 -, 28 -, 29 -, 21 -, 15 -, 10 -, 06	92 .36 .56 .56 .51 .46 .31 .28 .24 .18
0.94 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 50.0 60.0 90.0	60 -1.61 -1.36 -1.15 99 70 77 39 39 39 39	-1.86 -1.86 -1.87 -1.03 -87 -693 -1.31 -1.03 -1.31 -1.03 -1.31 -1.03	44.39 44.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39	-1.28 -3.64 -2.71 -2.10 -1.71 -1.33 -1.10 76 46 33 21 10 00	\$2.225588855228266 \$4.74.74.71.11.11.11	-7.73 -7.22 -3.68 -2.75 -1.65 -1.65 -1.89 46 35 26 26 26		.56 .38 .32 .21 .17 .11 .09 .06	.51 .48 .38 .30 .26 .18 .11 .11	.35 .52 .46 .36 .30 .22 .16 .14	.12 .55 .52 .43 .36 .27 .20 .17	21 28 29 46 39 31 24 18 10 06 02	60 57 .59 .59 .46 .35 .21 01

TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED (a) $\alpha_u = 2^{\circ}$, 4° , 6° , 8° , 10° , 12°

Spannine	Per-	T			Surface		·	Γ			Lover	Surface		********
stations	chord	20	1 10		of attack	γ		1				of attack		
0.10 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	0.56 -30 -46 -49 -59 -50 -48 -45 -41 -41 -41 -45	0.49 60 67 66 61 56 52 15 45 45 45	0.23 -1.04 -97 -95 -84 -76 -73 -58 -52 -59 -50 -49	-0.15 -1.52 -1.29 -1.16 -1.03 94 85 57 57 55 53 52 50	-0.69 -0.77 -1.62 -1.40 -1.23 -1.10 -1.00 -1.00 73 58 56 51	12° -1.40 -2.72 -2.03 -1.71 -1.45 -1.27 -1.12796861575550		0.23 .03 .03 05 05 04 .01 .04 .10	0.43 .23 .09 .07 .05 .08 .10 .14 .20	0.59 .41 .25 .20 .16 .14 .114 .17 .20 .25	.30 .26 .54 .37 .20 .22 .22 .22 .25 .30	0.66 .63 .47 .40 .30 .30 .29 .28 .30	0.61 .70 .56 .48 .43 .35 .35 .35 .39
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	- 49 - 65 - 72 - 73 - 74 - 71 - 58 - 55 - 51 - 49 - 46 - 46 - 41 - 41	.27 -1.17 -1.07 99 93 83 63 63 54 54 51 49	44 -1.85 -1.51 -1.21 -1.25 -1.02 79 69 61 56 54 50	-1.37 -2.62 -1.87 -1.55 -1.42 -1.20 88 77 68 51 56	-2.55 -3.52 -2.37 -1.89 -1.70 -1.41 98 85 73 59 59 59	-3.98 -4.18 -4.91 -4.87 -1.97 -1.99 -1.90 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88 -7.88		.00 .20 .01 07 10 08 .01		.62 .58 .40 .38 .19 .13 .14	.49 	.93 .69 .69 .55 .43 .29 .27 .27	07 59 72 .65 .54 .39 .33 34
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	- 60 - 74 - 75 - 75 - 75 - 75 - 75 - 75 - 75 - 75	.23 -1.07 -1.07 -1.01 97 82 71 68 55 53	21 -1.66 -1.46 -1.34 -1.15 -1.07 97 83 76 67 57 51	**************************************	-1.76 -1.18 -1.98 -1.70 -1.51 -1.06 81 56 56	-2.86 -4.06 -4.85 -4.00 -1.73 -1.50 -1.19 -1.01 87 74 66		.29 .11 02 05 03 01 .04 16	.49 .31 .15 .09 .10 .08 .08 .10	.60 .49 .30 .23 .20 .18 .16 .18	.46 .61 .61 .35 .31 .26 .24 .24	.52 .67 .54 .45 .41 .30 .30	.34 .70 .56 .56 .32 .44 .39
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 60.0 70.0 90.0		.03 -1.43 -1.19 -1.13 -1.00 91 86 61 59 53 50 44	64 -e.19 -1.57 -1.30 -1.16 -1.05 68 60 55 51 43	-1.66 -3.08 -2.08 -1.82 -1.81 -1.27 88 75 66 79 43 39	9.564 9.1663 9.1664 9.1664 1.1663 1.1664 1.1663 1.1664 1.1663 1.1664 1.1663 1.1664 1.1663 1.1664 1.1663 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1664 1.1			.39 .18 .05 .01 .04 .08 .27	.22 .16 .14 .12 .15 .21 .31	.58 .52 .36 .27 .20 .20 .20 .34	.53 .46 .59 .48 .40 .29 .28 .30 .36	.25 .60 .56 .49 .37 .35 .40 .39 .39	.59 14 .59 .62 .56 .56 .49 .43 39 .45
D.\$4 B/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 90.0	.34 -1.05 95 85 85 85 67 60 55 59 46 46	-25 -1.75 -1.41 -1.13 -1.01 68 55 55 55 34	1.20 -2.57 -1.82 -1.44 -1.22 -1.69 67 67 67 47	-2.58 -3.60 -2.41 -2.76 -1.76 -1.76 -1.85 -1.85 74 56 50 35 39	1.8 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	-6.41 -3.70 -2.95 -1.92 -1.60 -1.21 98 70 56 34		.53 .33 .16 .06 .01 .01 .06 .11 .19 .26	.61 .53 .24 .17 .10 .13 .17 .22 .28	.51 .64 .39 .31 .21 .21 .22 .30	.82 .65 .64 .53 .46 .89 .89 .89 .89 .89 .89	27 27 .57 .73 .64 .56 .40 .33 .30 .31 .35	93 93 75 72 66 48 40 37 36 39

TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_{11} = 2^{\circ}$, 4° , 6° , 8° , 10° , 12° - Concluded

	Per-	Upper surface							Lower surface						
Spamvise stations	cent	Angle of attack							Angle of attack						
stations	cherd	2º	J.P	6°	€	10	12°		2	40	6°	80	10°	120	
0. 5 6 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 50.0 60.0 70.0 90.0 95.0	0.46 71 73 67 57 38 33 30 10	29958282828532482 04441111110	-0.33 -1.71 -1.46 -1.33 -1.15 -1.65 55 46 26 10	1.11 4.84 1.87 1.45 1.45 1.24 1.05 1.24 1.05 1.24 1.25 1.26 1.27 1.03	4.14 -3.37 -4.37 -4.47 -1.47 -1.47 -1.48 -1.48 -1.48 -1.48 -1.05	74 9.4.66 9.4.66 9.4.96 9.4.73 1.73 1.73 1.73 1.73 1.73 1.73 1.73 1		0.29 .05 .07 .09 .09 .09 .09 .09 .09 .09	0.51 .28 .10 .07 .04 .01 .02 .01	0.60	0.60 .57 .40 .32 .25 .18 .13 .13	0.49 .66 .51 .42 .36 .23 .19	0.28 .69 .52 .46 .40 .30 .26	
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 60.0 90.0 95.0	587888799884785	336881788889388838 1111111111111111111111111111	177771111111111111111111111111111111111	-1.05 -2.39 -1.88 -1.40 -1.21 -1.06 55 55 55 55 55 55 55 5	-2.27 -3.37 -4.44 -1.74 -1.46 -1.26 -1.20 -77 60 32 18 01	-3.78 -4.16 -3.45 -3.45 -3.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45 -1.45		.21 .02 07 09 07 06 03 05 .08	.146 .27 .11 .06 .04 .01 .07 .08 .10	.56 .43 .26 .18 .15 .10 .10 .10 .10	.51 .54 .38 .29 .24 .18 .15 .15 .11 .12 .10	.32 .57 .46 .36 .32 .24 .20 .16 .14 .14	01 .55 .46 .41 .32 .26 .21 .19	
0.80 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	- 39 - 36 - 36 - 46 - 45 - 39 - 39 - 39 - 39 - 24 - 20 - 103 - 04	277 -77766 -77766 -77545 -304 -103 -04	-24 -1.18 -1.18 -1.06 94 80 70 57 50 42 34 27 18 03	-1.13 -2.16 -1.55 -1.36 -1.23 -1.05 89 70 59 19 36 28 28 16 02	-2.38 -3.08 -2.10 -1.75 -1.26 -1.26 -1.26 53 40 28 15 05 03	-3.88 -3.85 -2.64 -4.14 -4.81 -4.87 -1.89 -72 -72 -1.40 -1.06 -1.06		.12 05 12 09 07 07 03 .05 .07	.41 .21 .07 .02 .02 .01 .04 .06 .07 .08	.56 .39 .22 .24 .13 .10 .09 .10 .10	.56 .50 	.42 .56 .34 .30 .22 .16 .15 .14 .11	.19 .56 .51 .38 .30 .20 .16 .13 .09	
0.9 4 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.504 - 209 - 209 - 331 - 209 - 331 - 209 -	.53 -53 -53 -53 -53 -54 -54 -64 -64 -64 -64 -64 -64 -64 -64 -64 -6	.24 94 87 82 71 49 37 28 28 20	- 36 -1.20 -1.10 -96 -67 -53 -47 -37 -31 -13 -13	-1.32 -2.19 -1.67 -1.41 -1.99 80 51 51 33 22 12 0	4.52 4.55 4.15 4.15 4.15 4.15 6.54 6.33 6.30 6.30 6.30 6.30 6.30 6.30 6.30		-16 -17 -20 -16 -15 -09 -05 -01 -03 -06 -08	.22 .04 .04 .04 .06 .06 .07	. 20 .13 .07 .05 .04 .05 .06 .07 .08	.53 .34 .25 .16 .13 .10 .07 .07 .06 .06	.49 .35 .25 .21 .14 .11 .10 .07 .06	.34 .51 .44 .36 .28 .20 .15 .13 .06 .06	

TABLE XIX. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_U = 14^{\circ}$, 16° , 18° , 20°

Spagwise	Per-	Upper surface						Lower surface						
	cent	Angle of attack						Angle of attack						
stations	chord	140	16°	180	200			140	160	160	20			
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 90.0	-2.86 -3.37 -2.38 -3.97 -1.40 -1.60 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50 -3.50	4.90 -3.97 -4.71 -4.81 -1.92 -1.92 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -1.95 -	3% 82 2 8 3 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	14.33 14.33 14.33 14.33 14.33 14.39 14.39 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35 16.35			0.50 .72 .62 .53 .50 .42 .39 .38 .41	0.38 .73 .58 .55 .45 .45 .44 .42 .41	0.21 .73 .73 .58 .48 .47 .45 .44 .46	0.04 69 -76 67 .64 53 53 548 469 -75 .63			
0.19 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 90.0 95.0	-5.43 -5.17 -3.27 -2.20 -1.75 -2.20 -1.75 -3.00 -70 -63 -51 -30 -31	-6.86 -3.78 -3.78 -2.86 -1.86 -1.97 -70 -70 -70 -70 -70	5.86 -7.94 -1.68 -1.68 -1.59 -7.73 57 36	-6.01 -2.83 -1.79 -1.63 -1.69 -1.72 -1.71 -1.43 -1.77 -62 -77 -52 -48			-,48 .47 .76 .71 .60 .44 .38 35 .39	92 .35 .77 .67 .50 .42 38 .42	79 -81 89 59 59 59 40 43 48	-91 -83 -83 -82 -73 -54 -47 -40 -44			
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	-3.90 -3.87 -3.27 -2.69 -2.88 -3.61 -3.06 -3.06 -7.06 -7.06 -67	15353838668885856688856688856688856688856668885666885666885666666	5.5% 5.5% 5.5% 5.5% 5.5% 5.5% 5.5% 5.5%	5.99 -5.04 -3.23 -4.55 -4.55 -4.55 -4.55 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13 -4.13			.12 .68 .70 .63 .58 .50 .43 .40	05 .67 .75 .69 .64 .55 .47 .43 42	-23 -65 -78 -73 -69 -58 -49 -46 -44	-27 .67 -83 .76 .70 .60 .52 .46			
0.375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 90.0 90.0	5.68 -6.00 -3.76 -2.79 -2.35 -2.35 -2.10 -2.10 -2.10 -2.77 -2.79	-6.11 -6.01 -3.36 -2.45 -2.45 -2.45 -2.20 -2.99 -1.03 -1.04 -1.02 -2.99 -384 -381	-6.45 -5.33 -4.84 -1.13 -1.11 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00	1.99 1.15 1.15 1.15 1.15 1.15 1.15 1.15			43 50 66 50 50 45 41 45	-55 -50 -66 -66 -60 -53 -45 -40 -44 -39 -50	-70 .46 .71 .69 .64 .77 .49 .41 .44	. 43 .51 .72 .69 .56 .56 .50			
0.44 6/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 50.0 60.0 70.0 80.0 90.0	4.88 4.73 4.59 4.43 4.43 4.43 4.32 82 82 83 83	-3.13 -4.14 -99 -99 -99 -1.04 -4.00 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04 -1.04	4.59 99 99 	-1.80 87 87 87 98 98 98 98 98			-,60 -,71 -,72 -,63 -,63 -,63 -,37 -,36 -,39 -,39	-24 -64 -79 -73 -69 -190 -190 -190 -190 -190 -190 -190 -19	- 23 .63 .63 .70 .68 .70 .37 .37 .35	- 18 .63 .63 .69 .53 .38 .35 .36			

TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm u} = 14^{\circ}$, 16° , 18° , 20° - Concluded

	Per-			Upper	our face	 	Lower surface						
Spanwise stations	cent			Angle o	fattack		Angle of attack						
STATIONS	cherd	140	160	185	200		140	160	180	20°			
0. 5 6 b/2	0 1.5 1.0 7.0 15.0 20.0 30.0 50.0 50.0 60.0 90.0	######################################	3988887777111111111111111111111111111111	1.69 1.78 1.78 1.78 1.78 1.79 1.79 1.79 1.79 1.79 1.79 1.79 1.79	-5.05 -3.25 -2.01 -2.14 -1.74 -1.42 -1.11 88 74 63 55 47		0.15 .66 .63 .50 .40 .33 .29	0.10 .66 .57 .52 .33 .30 .30	-0.06 .69 .62 .56 .46 .39 .33 .01	1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126 1.126			
0.68 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 70.0 90.0 90.0	552888498884488 1179917711111111	४५०० ४५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५	30907.1288.656.657.458.888.88	882455448886558 \$1411111111			63 .41 .57 .52 .49 .39 .39 .39 .20 .16 .10	99 .31 .57 .55 .51 .42 .36 .21 .17	- 595 - 60 - 56 - 51 - 48 - 100 - 66			
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	54.54.563.555.555.555.555.555.555.555.555.555	\$2258888258884882 \$5.55888258884882	72.55.55.74.55.55.55.85.84.86 51.44.77.77.77.77.77.77.77.77.77.77.77.77.	-3.82 -1.74 -1.46 -1.39 -1.30 -1.26 -1.11 -1.99 87 76 56 51			-,42 ,44 .56 .50 ,46 ,38 .27 ,24 ,19 ,14 ,08	-,48 ,46 ,59 ,52 ,48 ,40 ,24 ,18 ,11 ,04 ,04				
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-3.80 -3.21 -2.53 -2.03 -1.55 -1.31 -1.06 -76 -79 -133 -131 -106 -06	-5.12 -3.85 -2.93 -2.93 -1.85 -1.44 -1.16 83 45 24 16 15	57965515787865555 57977777767865555	-2.29 -1.18 -3.18 -3.61 -7.71 -59 -57 -57 -57 -53		.12 .57 .49 .41 .34 .18 .14	14 56 .53 .45 .37 .29 .20 .16	-20 -57 -54 -56 -39 -28 -21 -16 -04 -04	.20 .54 .49 .41 .38 .24 .18 .10			

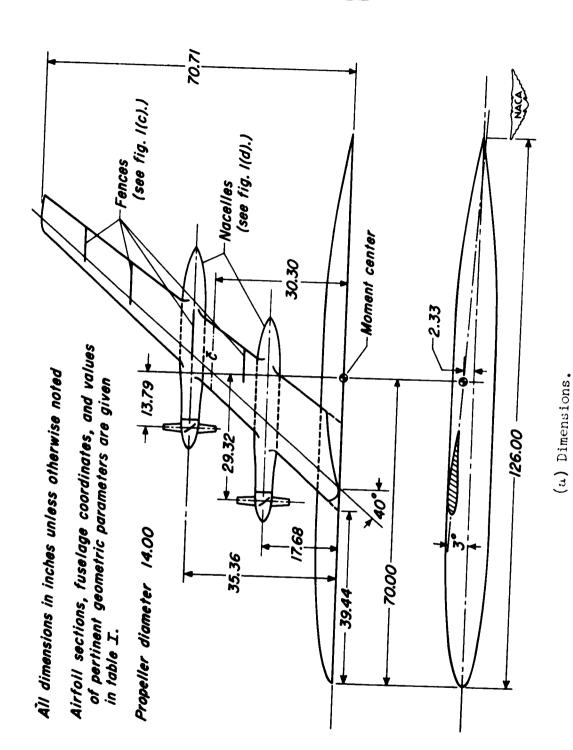
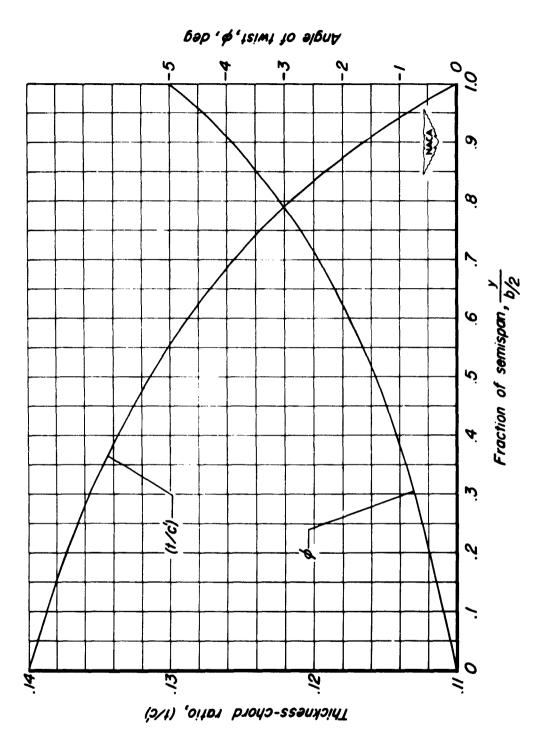
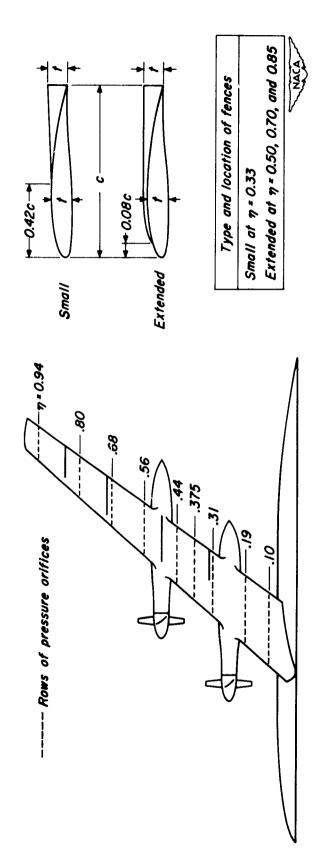


Figure 1.- Geometry of the model.



(b) Wing twist and thickness-chord ratio.

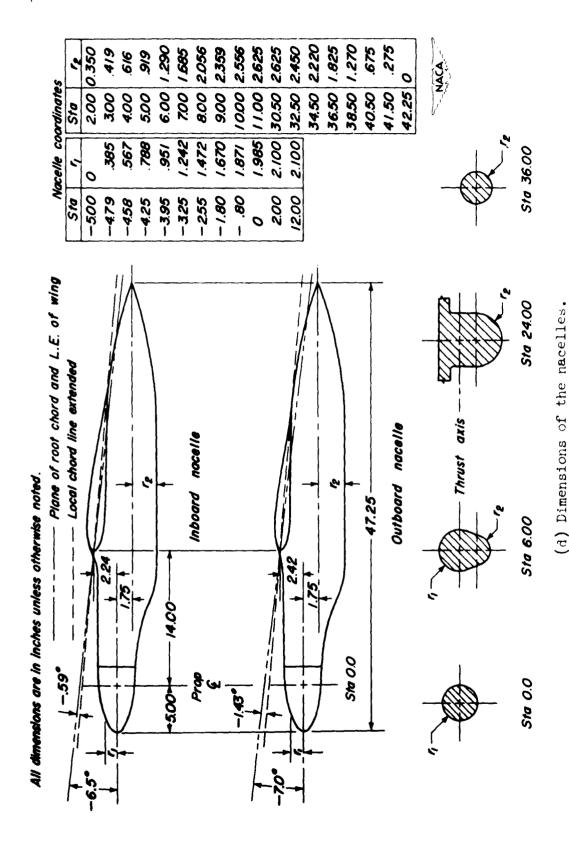
Figure 1.- Continued.



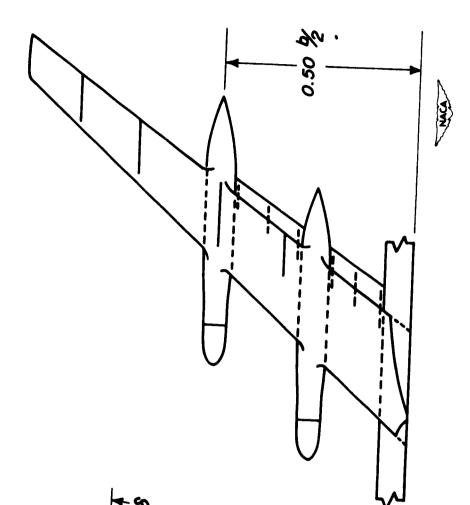
(c) Location of pressure-orifice stations and details of the four-fence configuration.

Figure 1.- Continued.

Figure 1.- Continued.



CONFIDENTIAL



(e) Flap details.

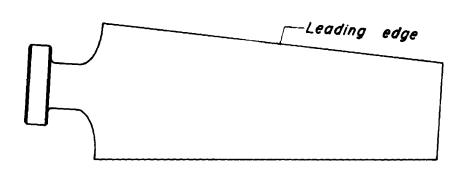
Figure 1.- Concluded.

normal to reference sweep line

Typical section through flap and

0.125 in. -

Developed plan form



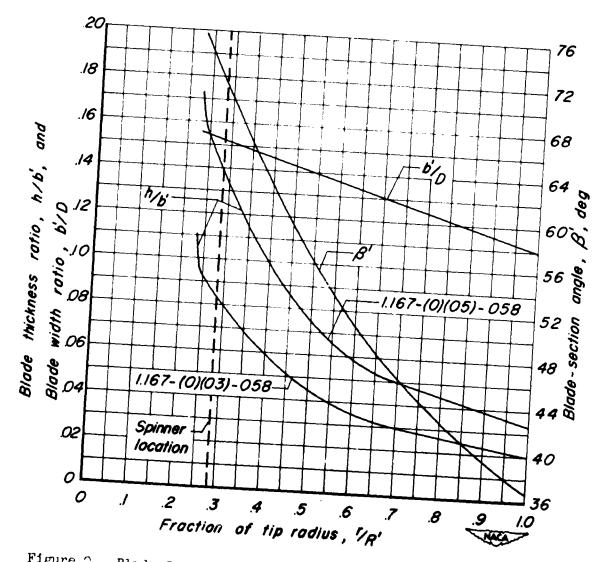


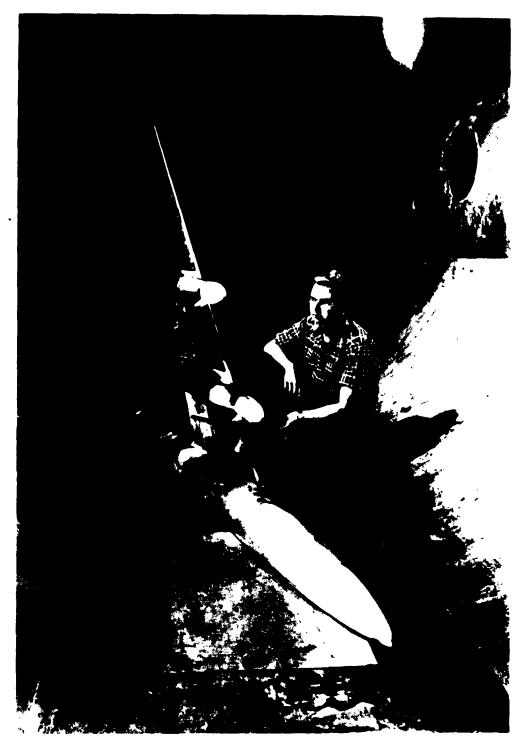
Figure 2.- Blade-form curves for the NACA 1.167-(0)(05)-058 and the NACA 1.167-(0)(03)-058 three-blade propellers.



A-17525.2

Figure 3.- Model mounted in the wind tunnel.

NACA RM ABBLES CONFIDENTIAL 81



A-17525.2

Figure 3.- Model mounted in the wind tunnel.

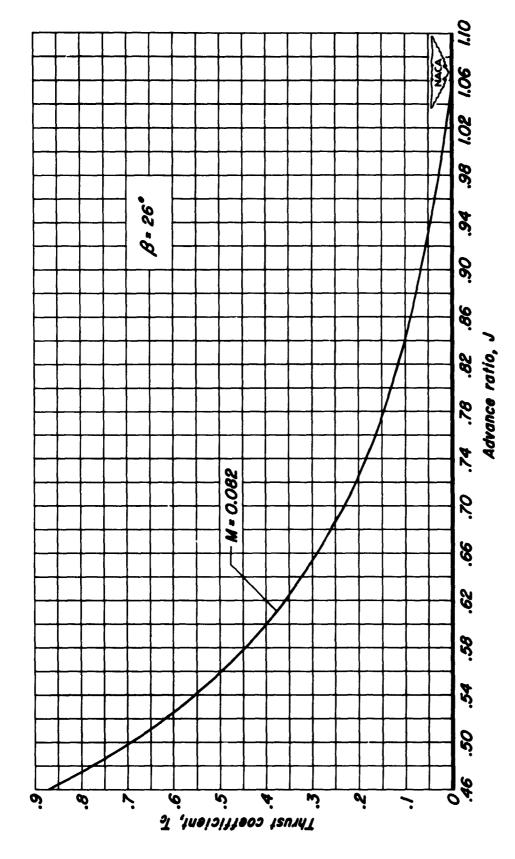


Figure 4.- The variation of thrust coefficient with advance ratio for the NACA 1.167-(0)(05)-058 propeller. Thrust axis parallel to the air stream. M = 0.082, R = 4,000,000.

٨,

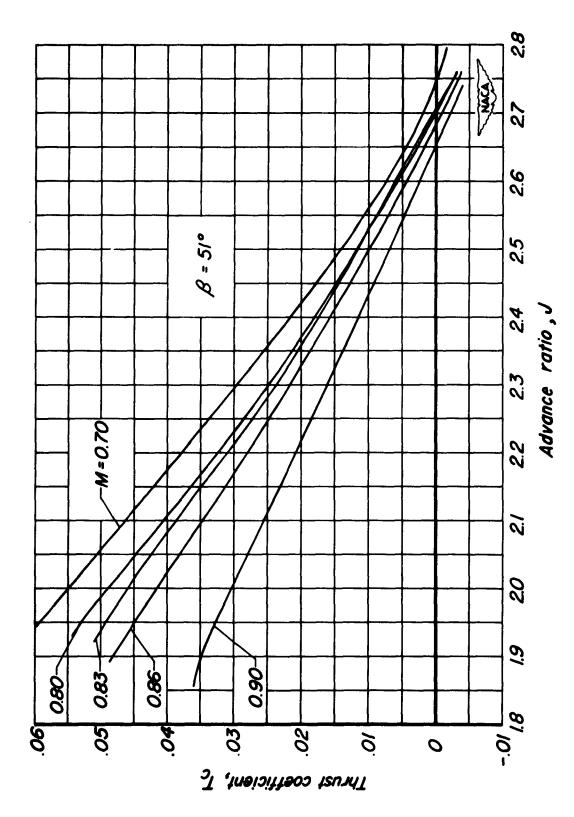


Figure 5.- The variation of thrust coefficient with advance ratio for the NACA 1.167-(0)(03)-058 R = 1,000,000propeller for several Mach numbers. Thrust axis parallel to the air stream.

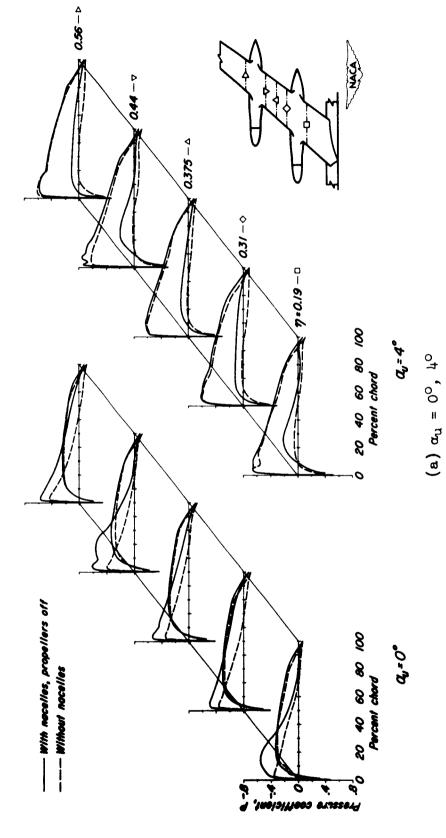
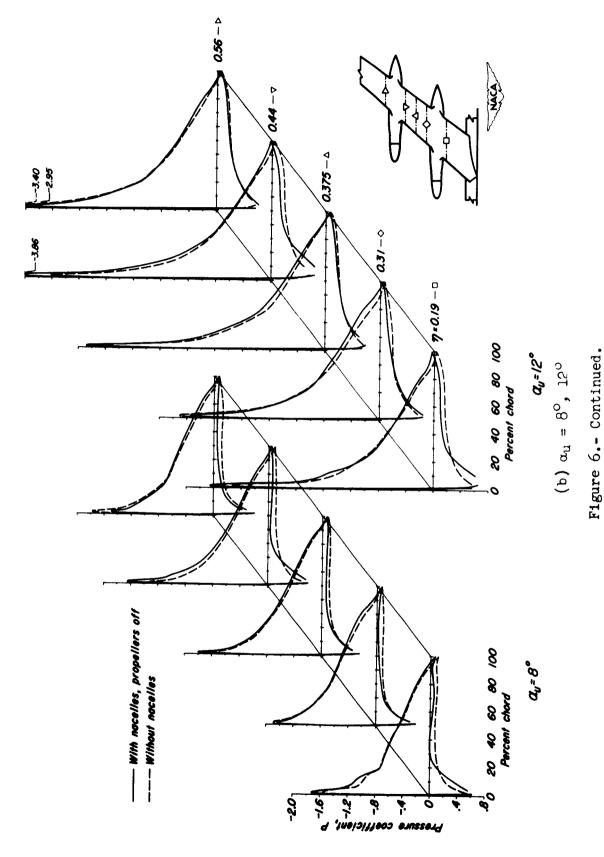
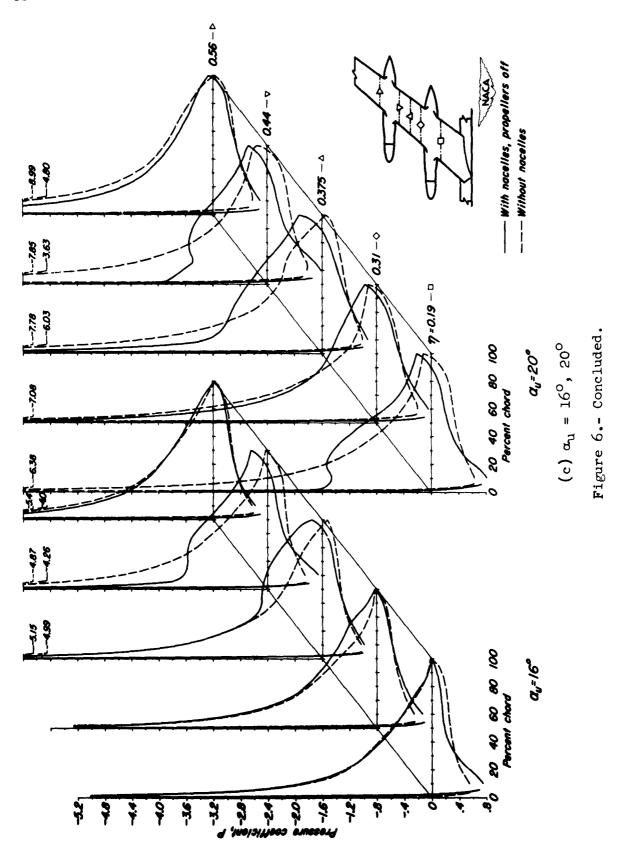


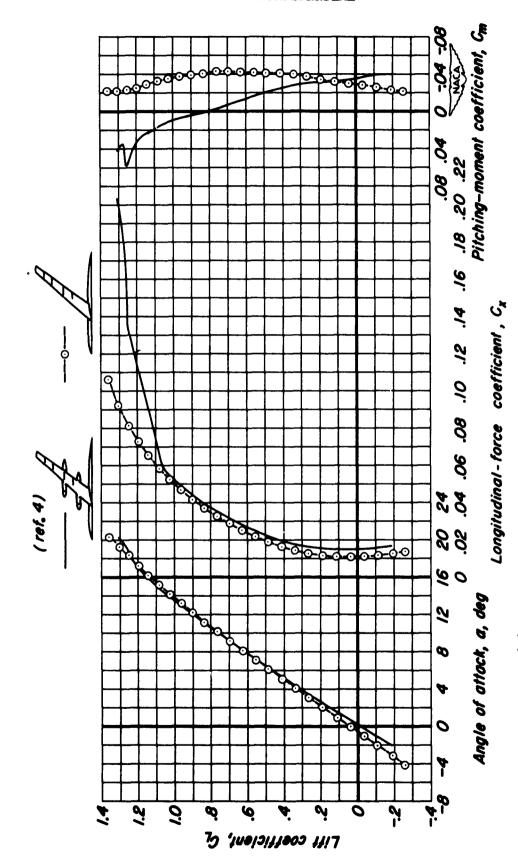
Figure 6.- A comparison of the chordwise distributions of pressure coefficient at five semispan stations of the wing for the wing-fuselage and the wing-fuselage-nacelles configurations. M = 0.165, R = 8,000,000.



CONFIDENTIAL

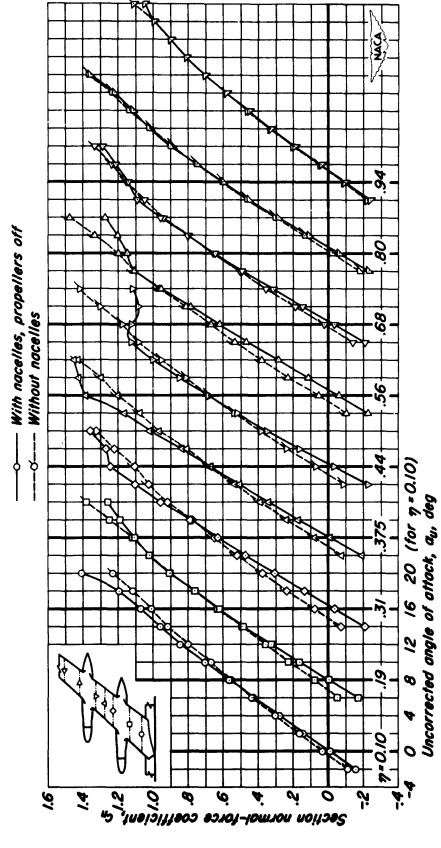


CONFIDENTIAL



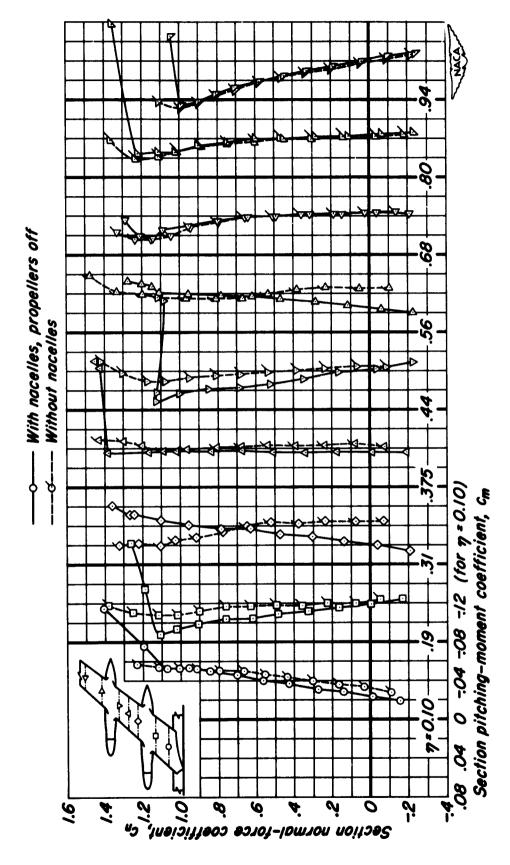
(a) Lift, longitudinal force, and pitching moment.

Figure 7.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-fuselagenacelles configurations and their corresponding section normal-force and section pitchingmoment characteristics at nine semispan stations of the wing. M = 0.165, R = 8,000,000.



(b) Section normal force.

Figure 7.- Continued.



(c) Section pitching moment.

Figure 7.- Concluded.

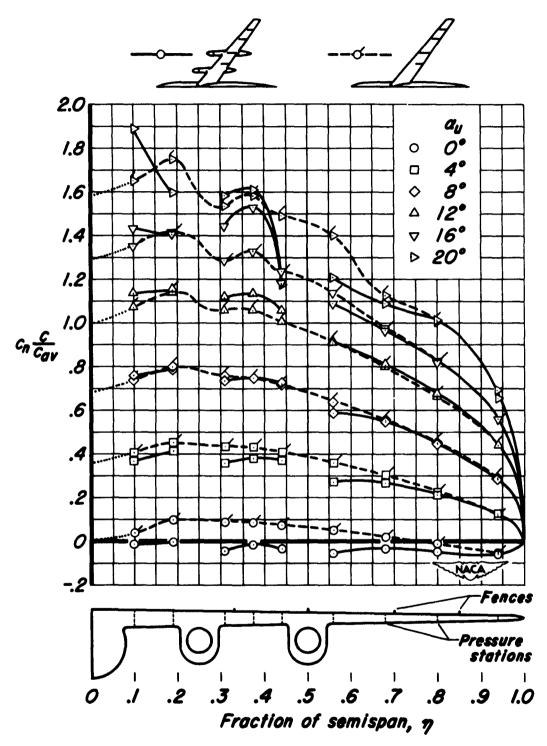


Figure 8.- The spanwise distribution of $c_n \frac{c}{c_{av}}$ as affected by the addition of nacelles to the wing-fuselage combination for several angles of attack. M = 0.165, R = 8,000,000.

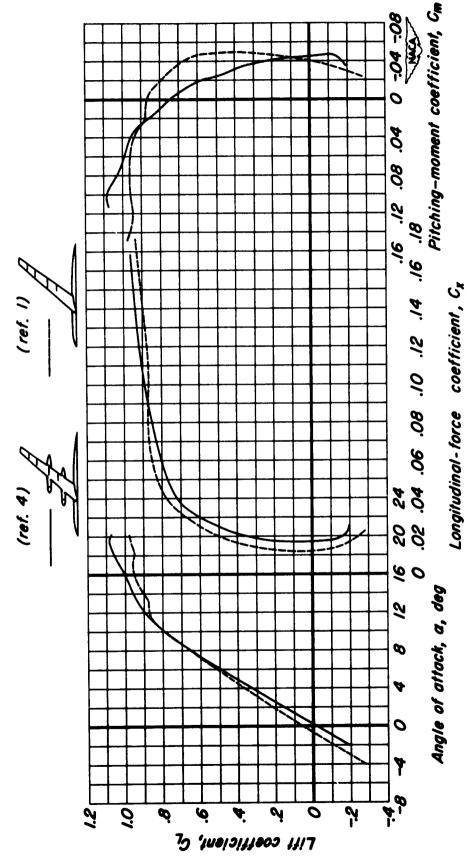
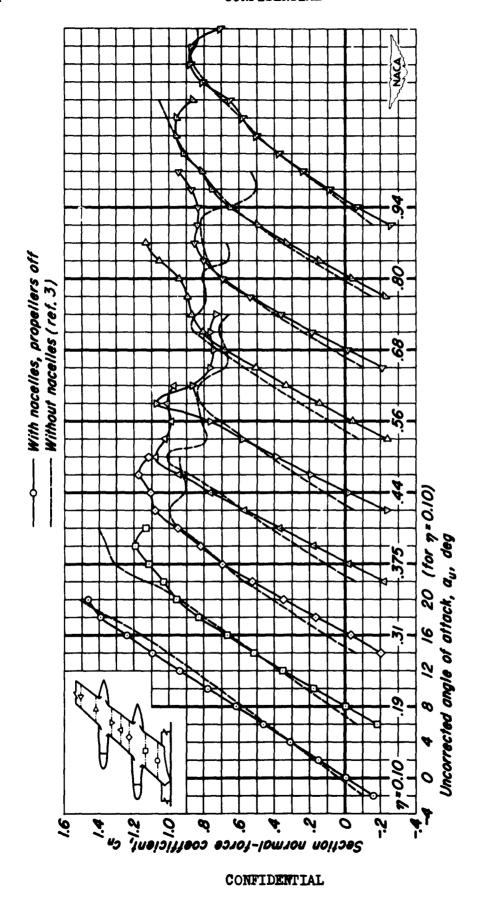


Figure 9.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-fuselagenacelles configurations and their corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M=0.60, R=2,000,000.

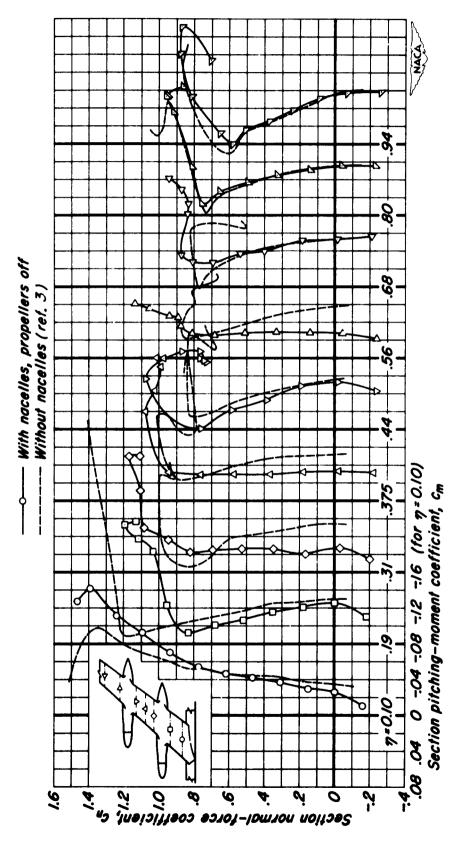
(a) Lift, longitudinal force, and pitching moment.

CONFIDENTIAL



(b) Section normal force.

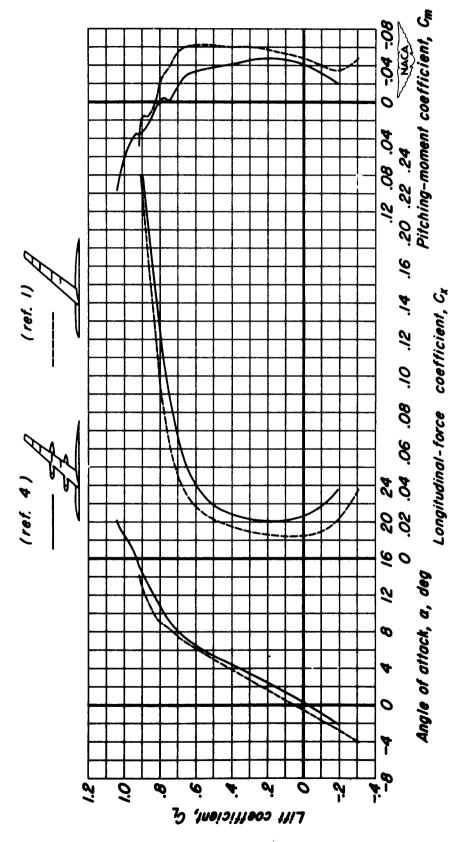
Figure 9.- Continued.



(c) Section pitching moment.

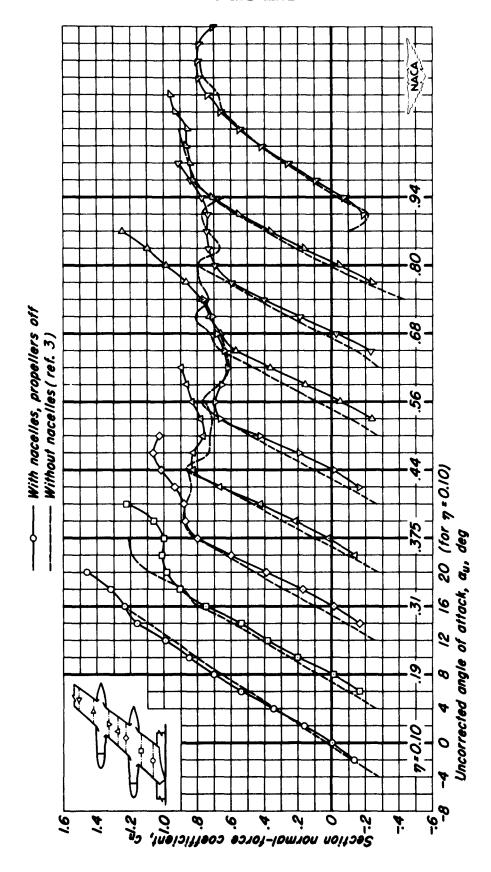
Figure 9.- Concluded.

CONFIDENTIAL



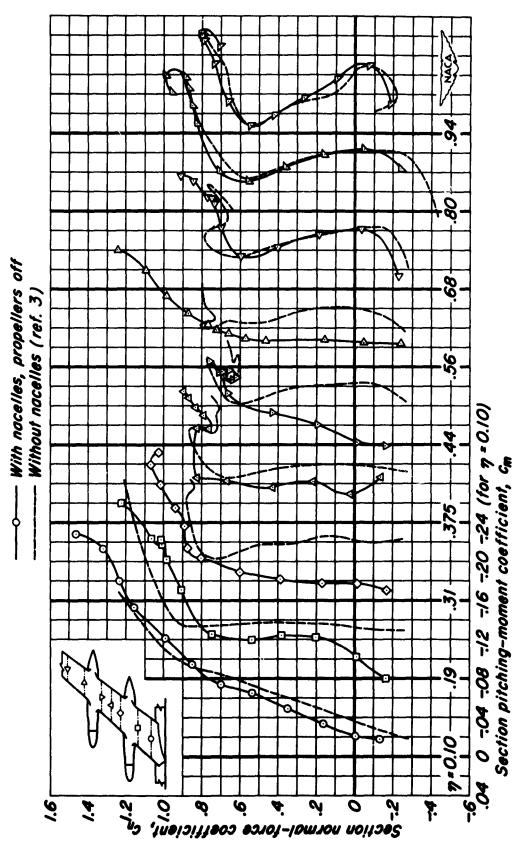
(a) Lift, longitudinal force, and pitching moment.

fuselage-nacelles configurations and their corresponding section normal-force and section Figure 10.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-M = 0.80pitching-moment characteristics at nine semispan stations of the wing. R = 2,000,000.



(b) Section normal force.

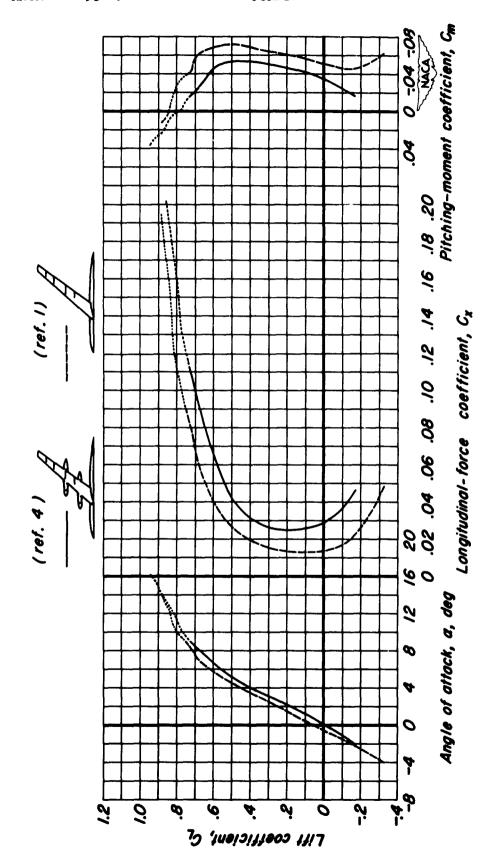
Figure 10.- Continued.



(c) Section pitching moment.

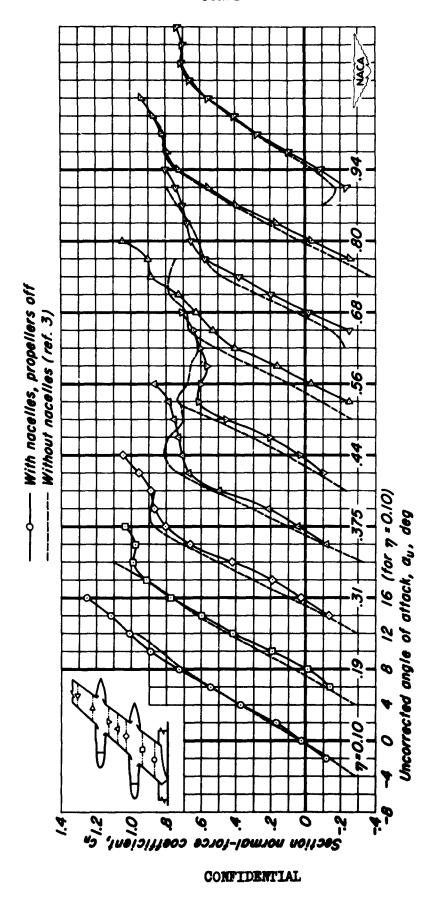
Figure 10.- Concluded.

G



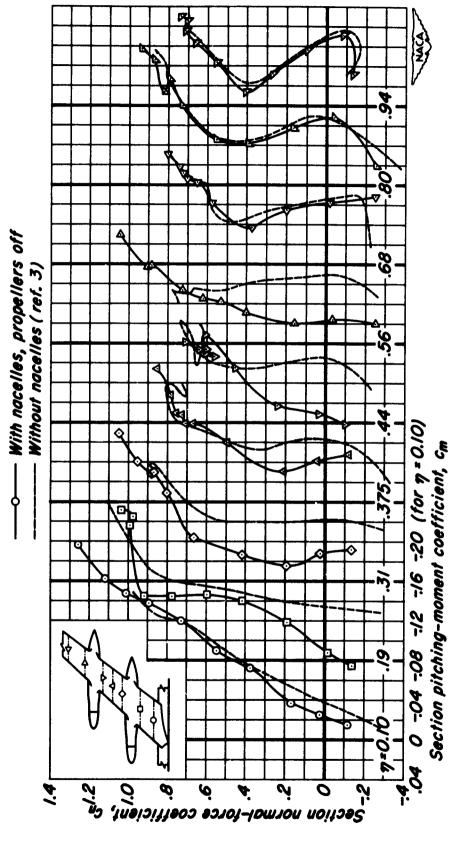
(a) Lift, longitudinal force, and pitching moment.

fuselage-nacelles configurations and their corresponding section normal-force and section Figure 11.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-M = 0.86pitching-moment characteristics at nine semispan stations of the wing. R = 2,000,000



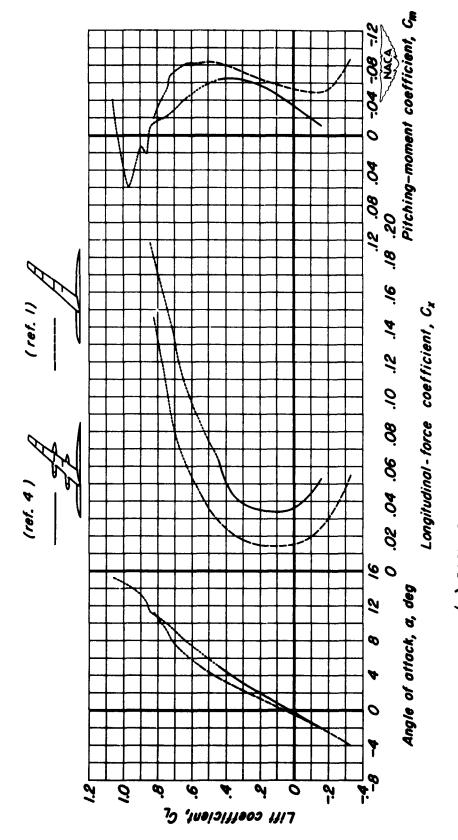
(b) Section normal force.

Figure 11.- Continued.



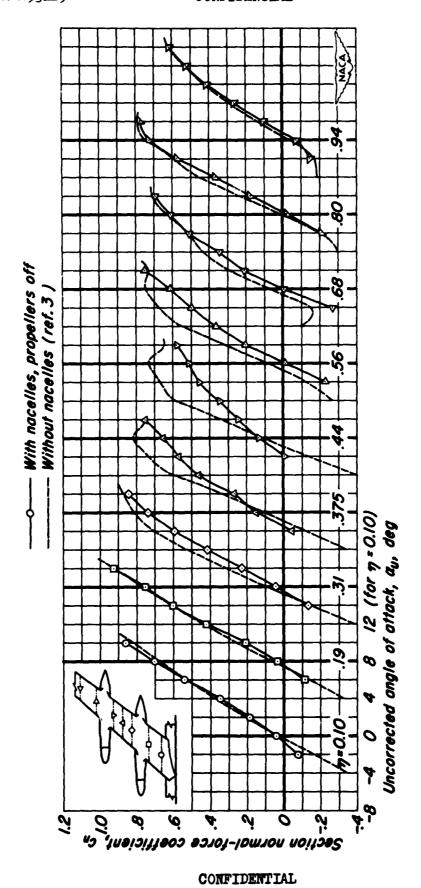
(c) Section pitching moment.

Figure 11.- Concluded.



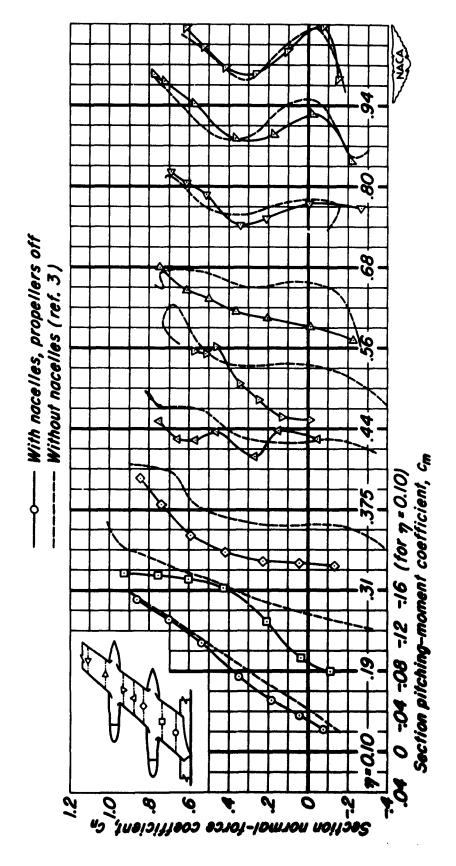
(a) Lift, longitudinal force, and pitching moment.

fuselage-nacelles configurations and their corresponding section normal-force and section Figure 12.- A comparison of the aerodynamic characteristics of the wing-fuselage and wingpitching-moment characteristics at nine semispan stations of the wing. M = 0.90, R = 2,000,000



(b) Section normal force.

Figure 12.- Continued.



(c) Section pitching moment.

Figure 12.- Concluded.

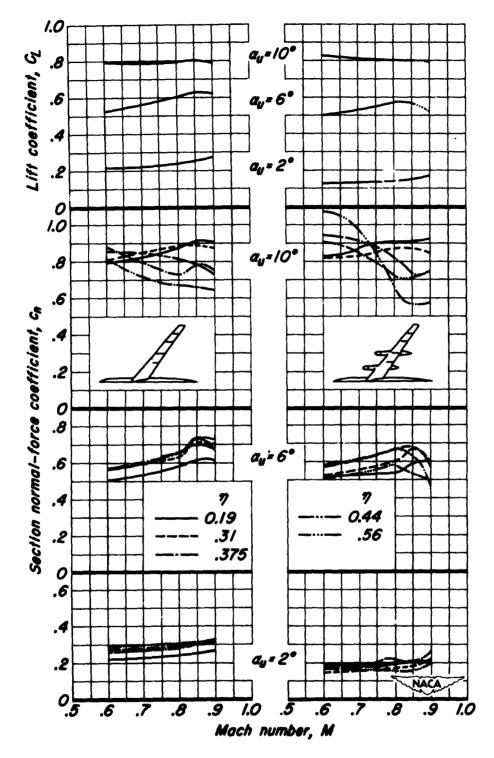


Figure 13.- The variations with Mach number of the lift coefficient and the section normal-force coefficient for several angles of attack of the wing-fuselage and the wing-fuselage-nacelles combinations.

R = 2,000,000.

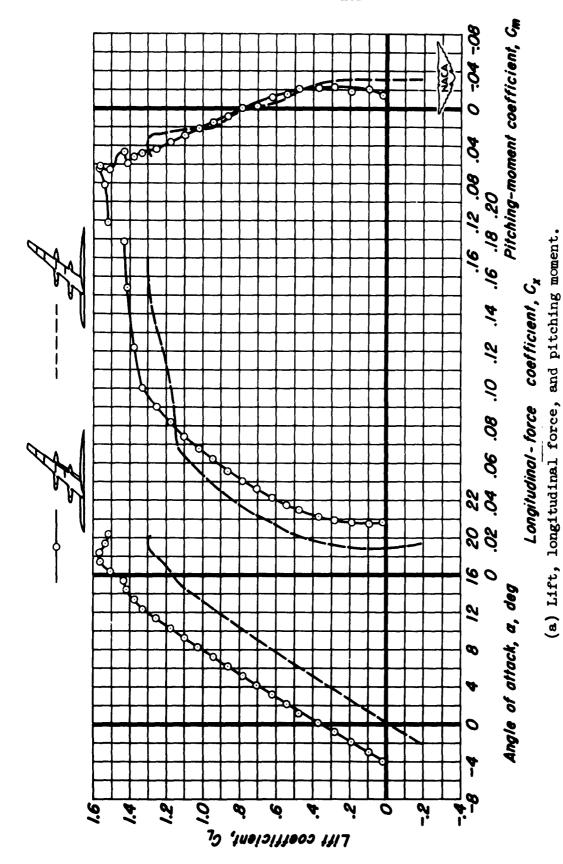
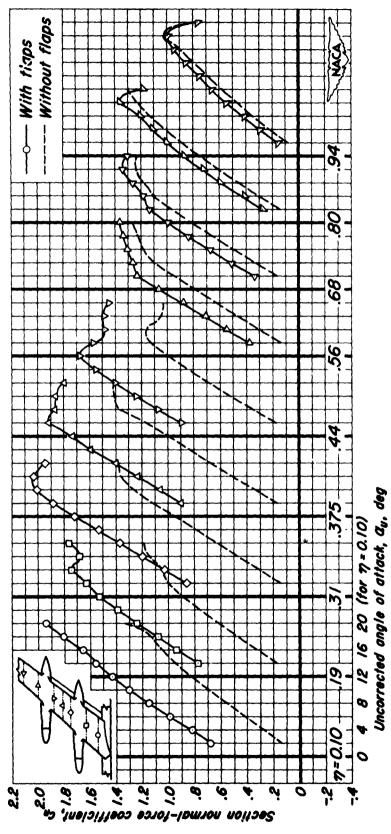


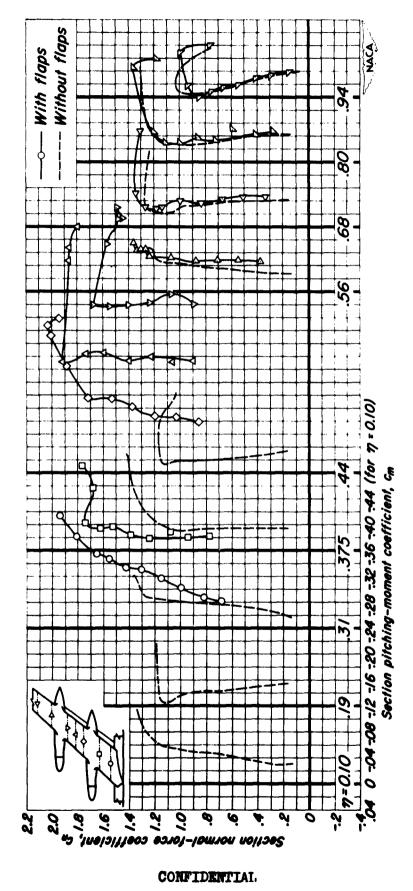
Figure 14.- The effect of flaps on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and on the corresponding section normal-force and section pitching-moment char- $\delta = 30^{\circ}$, M = 0.082, R = 4,000,000. acteristics at nine semispan stations of the wing.



(b) Section normal force.

Figure 14.- Continued.

CONFIDENTIAL



(c) Section pitching moment.

Figure 14.- Concluded.

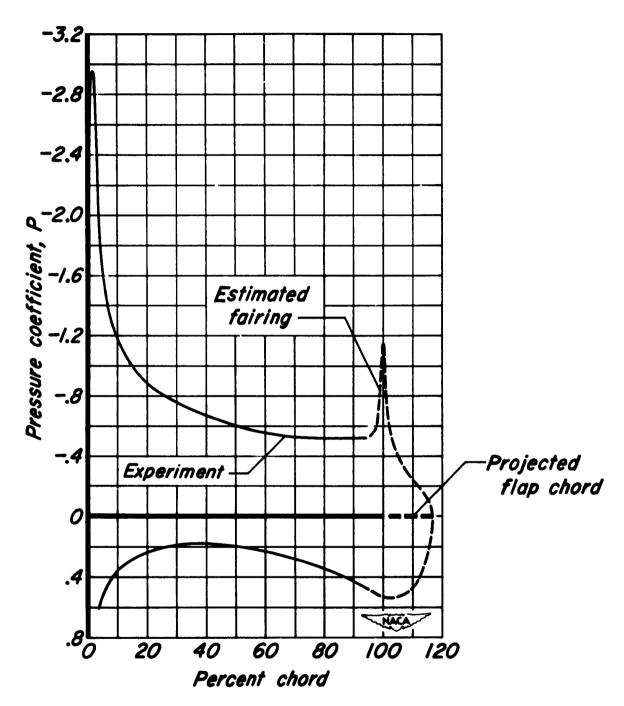


Figure 15.- Representative distribution of pressure coefficient for sections having a trailing-edge flap. $\delta = 30^{\circ}$, M = 0.082, R = 4,000,000.

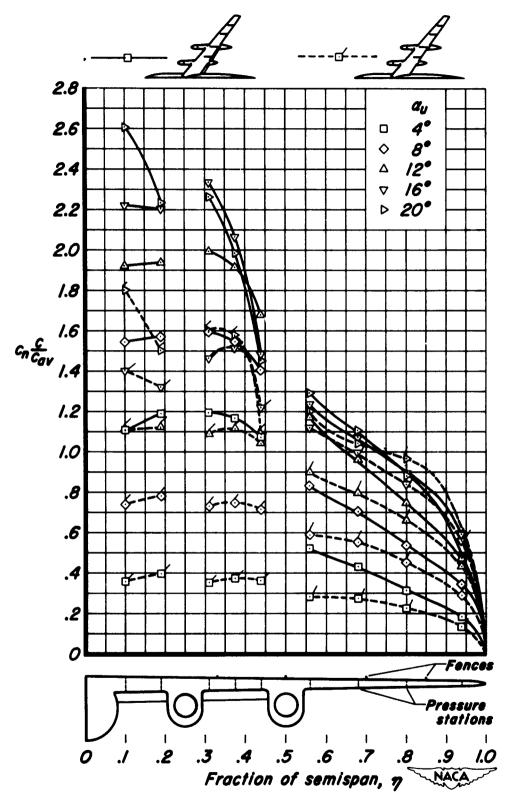


Figure 16.- The effect of flap deflection on the spanwise distribution of $c_n \frac{c}{cav}$ for the wing-fuselage-nacelles configuration at several angles of attack. M = 0.082, R = 4,000,000.

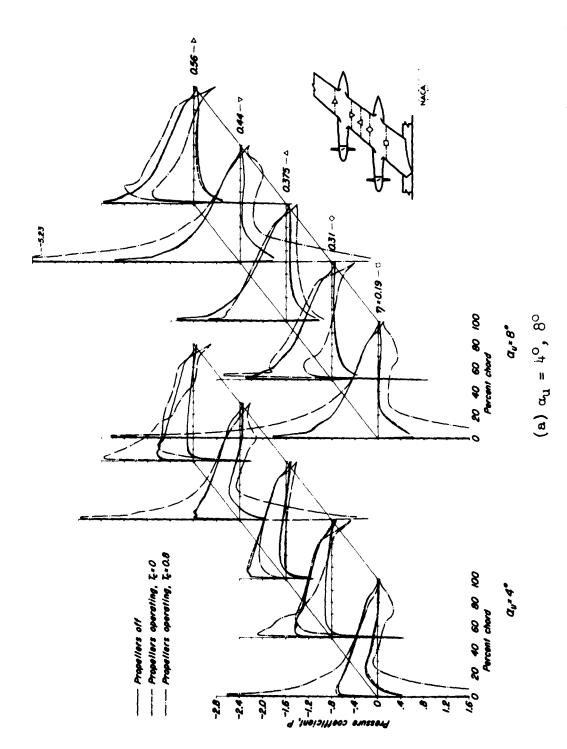
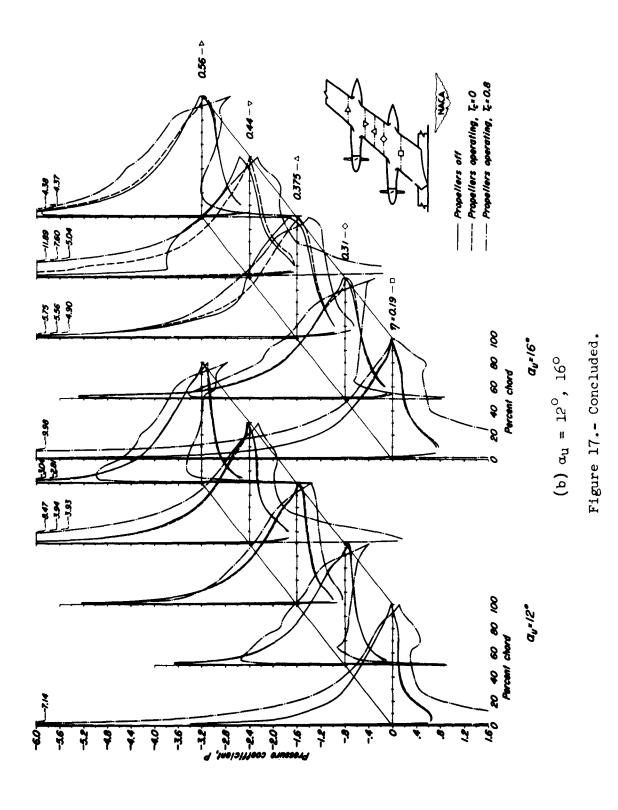
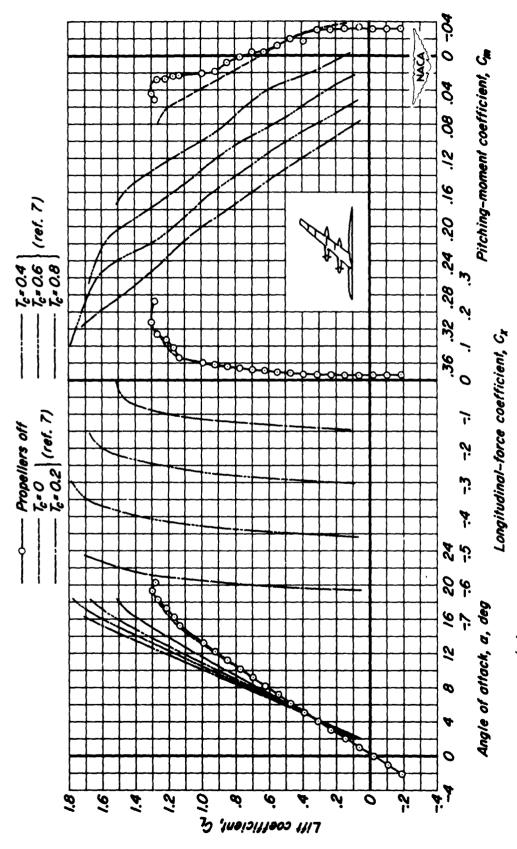


Figure 17.- The effect of increasing thrust coefficient on the chordwise distributions of pres-M = 0.082, R = 4,000,000. sure coefficient at five semispan stations of the wing.

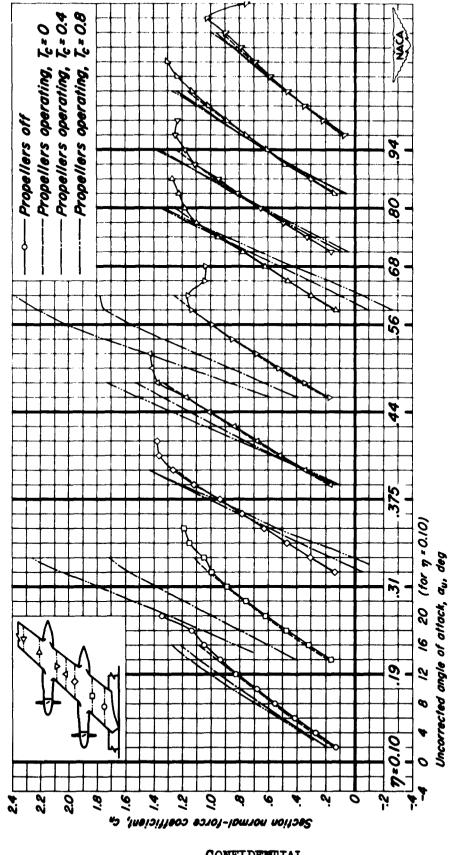


CONFIDENTIAL



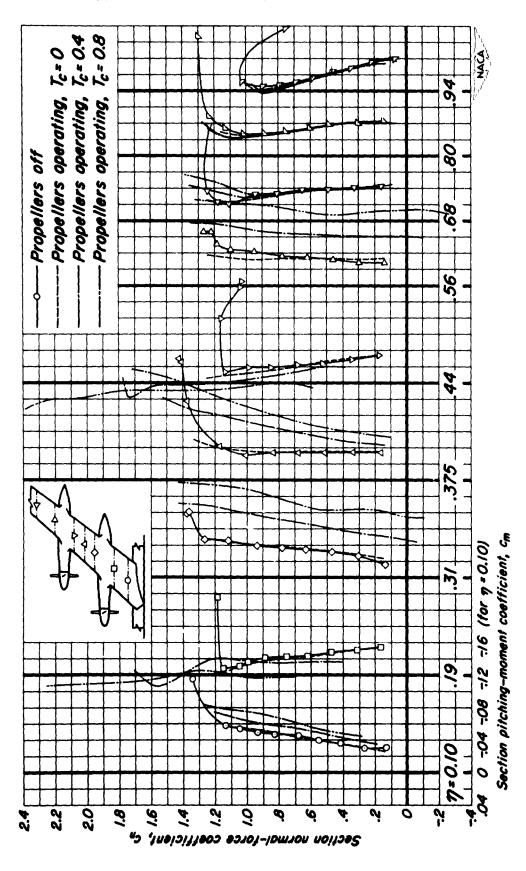
(a) Lift, longitudinal force, and pitching moment.

pitching-moment characteristics at nine semispan stations of the wing. M = 0.082, R = 4,000,000. Figure 18.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section



(b) Section normal force. Figure 18.- Continued.

CONFIDENTIAL



(c) Section pitching moment.

Figure 18.- Concluded.

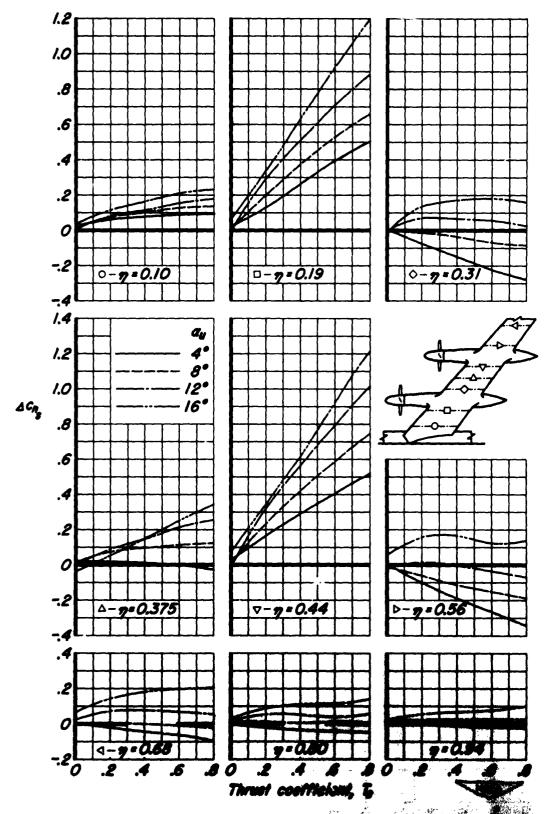


Figure 19.- The variations with thrust coefficient of the section normal-force coefficient.

COMPANIES

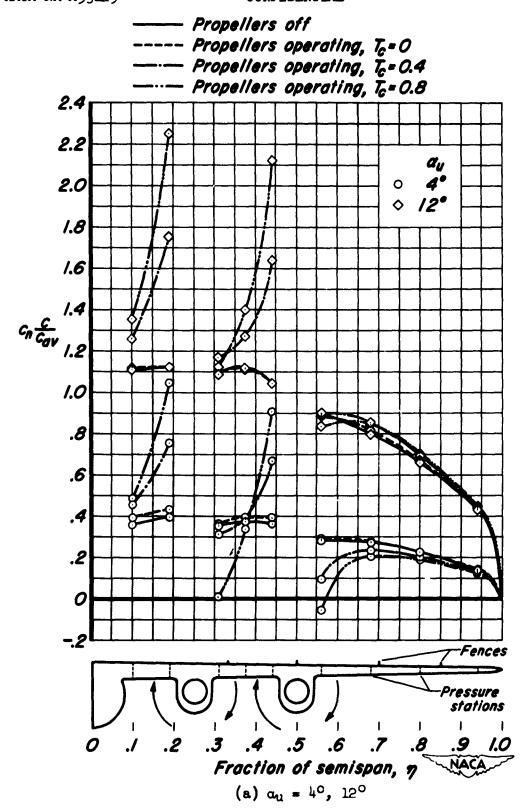


Figure 20.- The spanwise distribution of $c_n \frac{c}{c_{av}}$ as affected by thrust coefficient for several angles of attack. M = 0.082, R = 4,000,000.

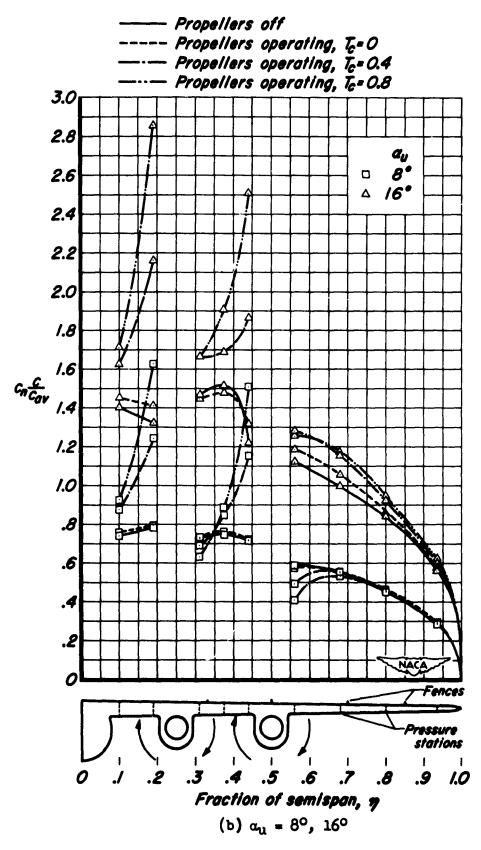


Figure 20.- Concluded. CONFIDENTIAL

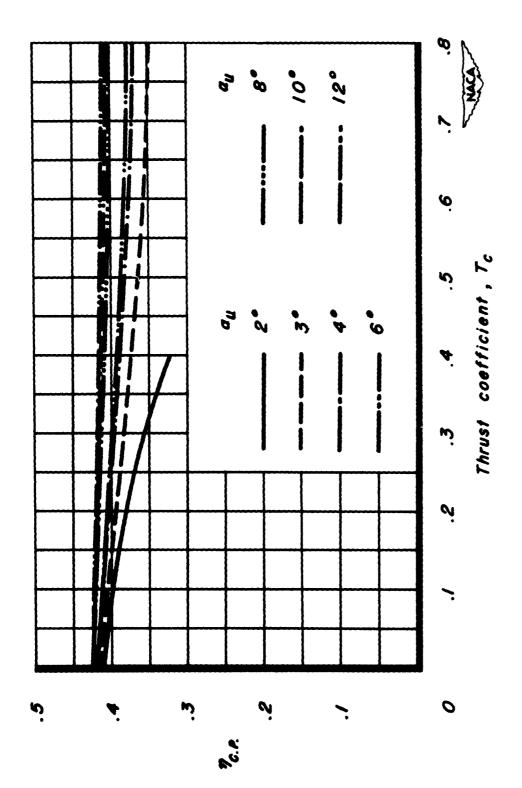


Figure 21.- The variation of the spanwise location of the center of pressure with thrust coefficient. M = 0.082, R = 4,000,000.

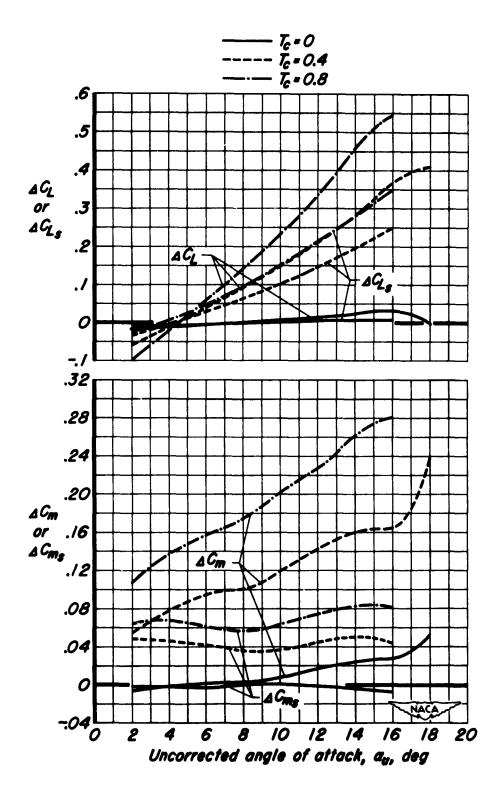
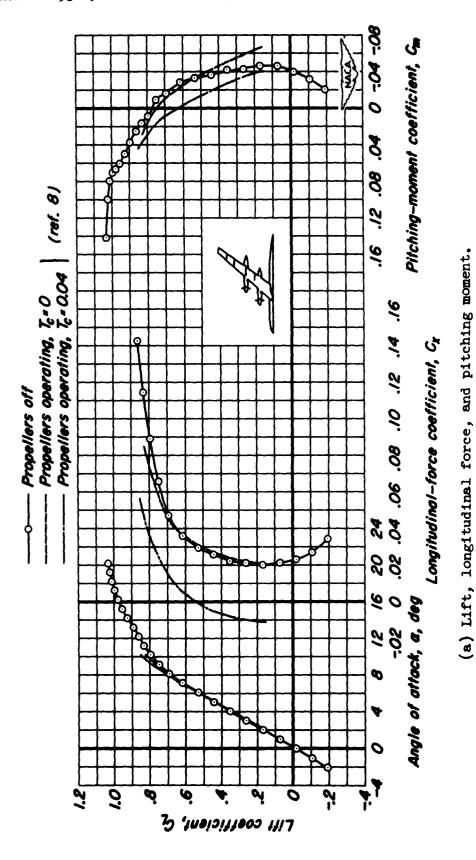
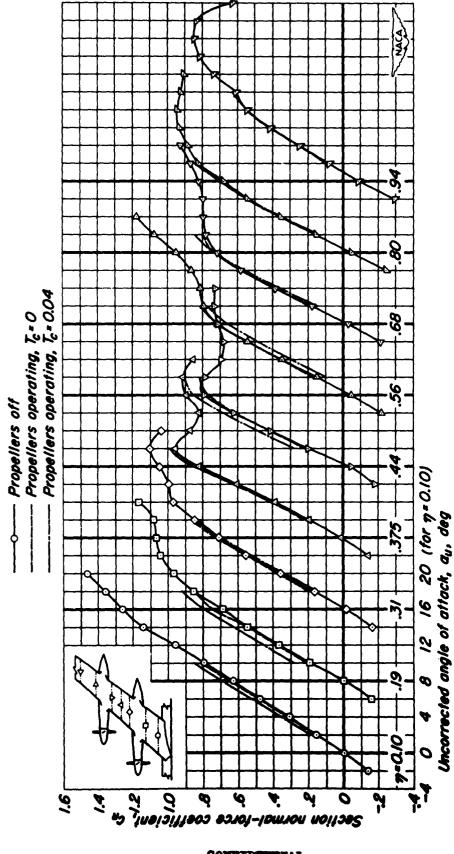


Figure 22.- The variation with angle of attack of the changes in the lift and pitching-moment coefficients due to increasing thrust coefficient and that due to propeller slipstream. M = 0.082, R = 4,000,000.



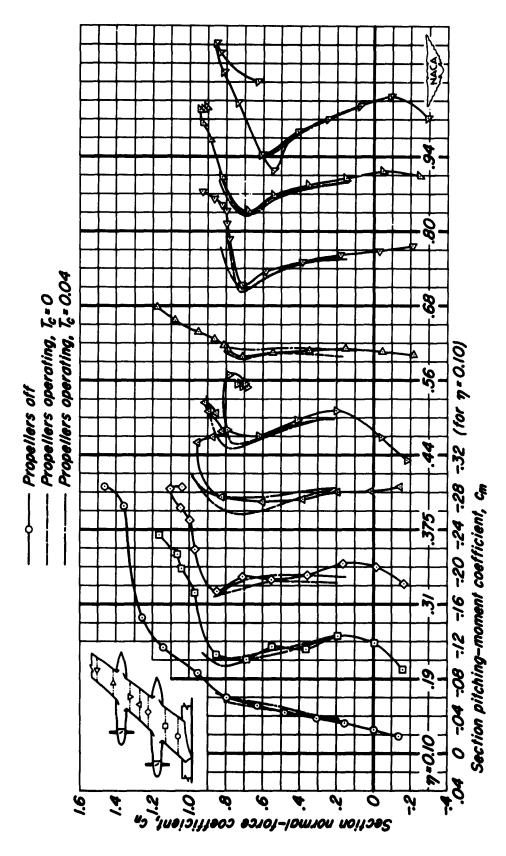
pitching-moment characteristics at nine semispan stations of the wing. M = 0.70, R = 1,000,000. Figure 23.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section



(b) Section normal force. Figure 23.- Continued.

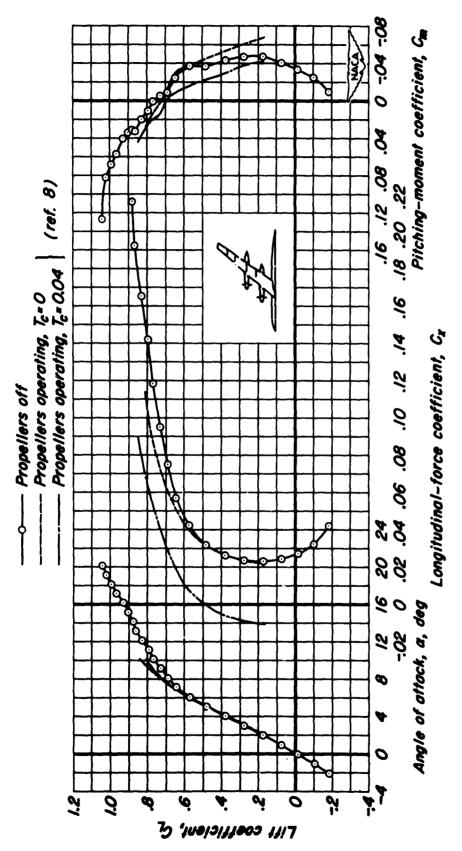
CONFIDENTIAL

G



(c) Section pitching moment.

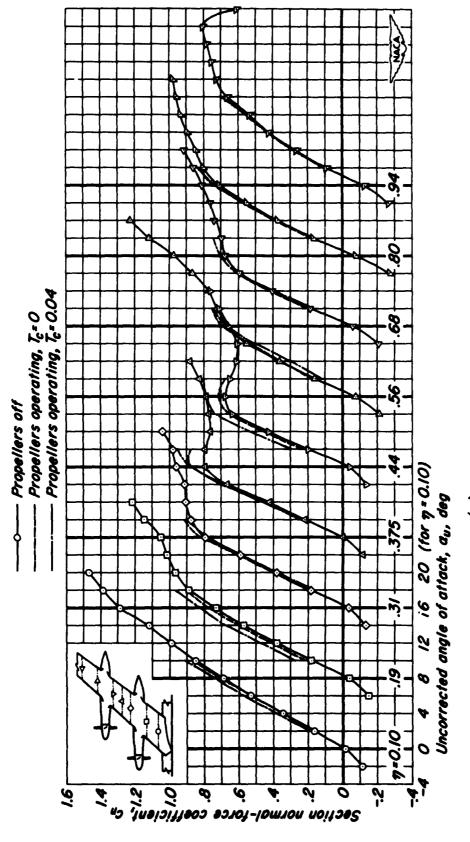
Figure 23.- Concluded.



pitching-moment characteristics at nine semispan stations of the wing. M = 0.80, R = 1,000,000. Figure 24.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section

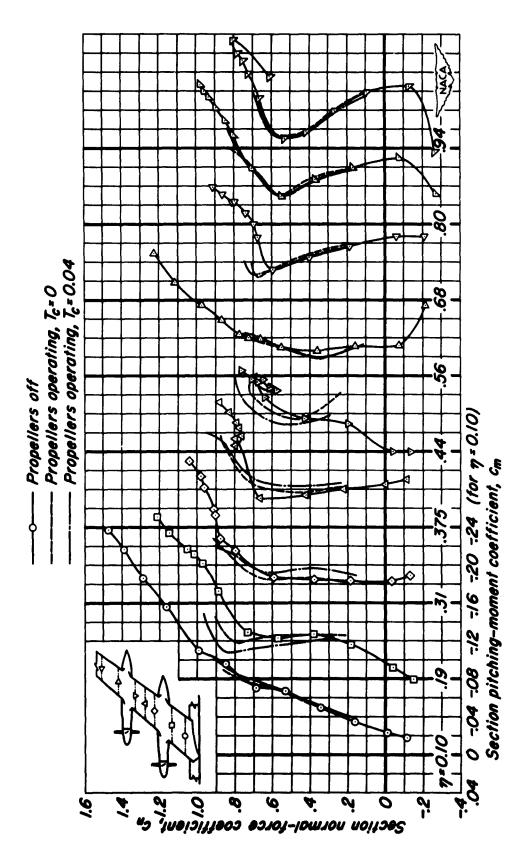
(a) Lift, longitudinal force, and pitching moment.

CONFIDENTIAL

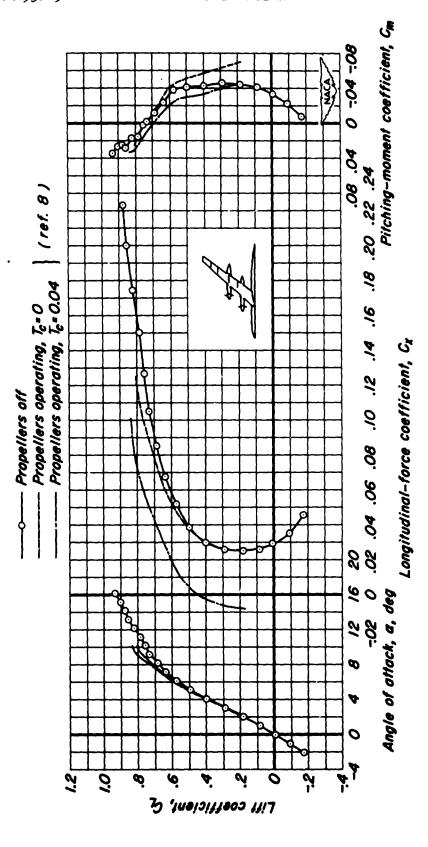


(b) Section normal force. Figure 24.- Continued.

CONFIDENTIAL



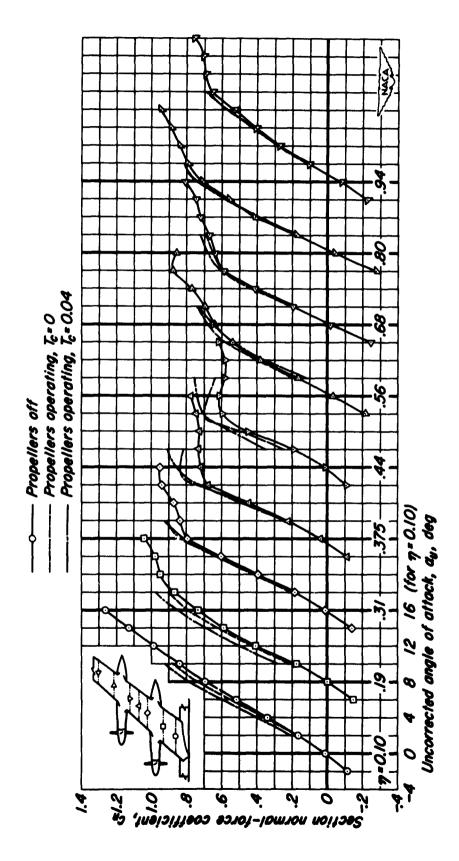
(c) Section pitching moment. Figure 24.- Concluded.



(a) Lift, longitudinal force, and pitching moment.

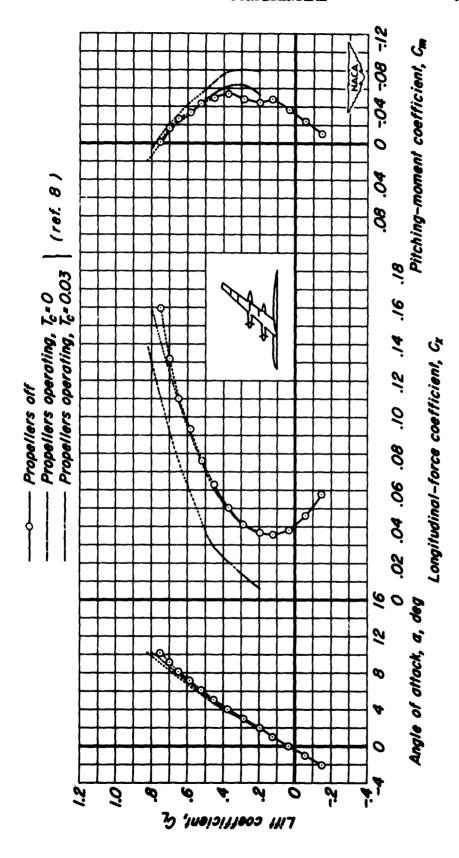
M = 0.83, R = 1,000,000. Figure 25.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing.

The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s



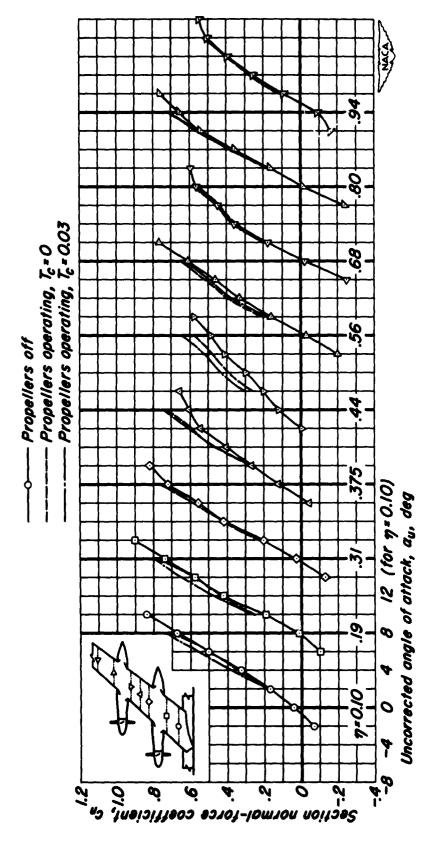
(b) Section normal force.

Figure 25.- Continued.



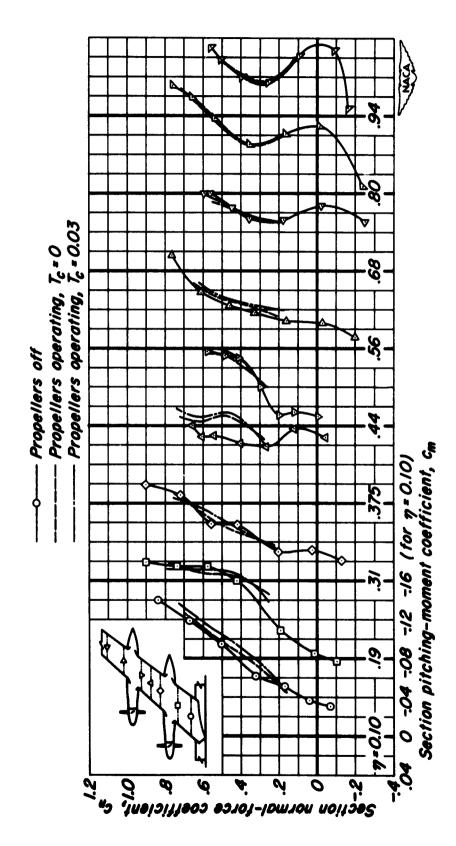
(a) Lift, longitudinal force, and pitching moment.

M = 0.90, R = 1,000,000. Figure 26.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing.



(b) Section normal force.

Figure 26.- Continued.



(c) Section pitching moment.

Figure 26.- Concluded.

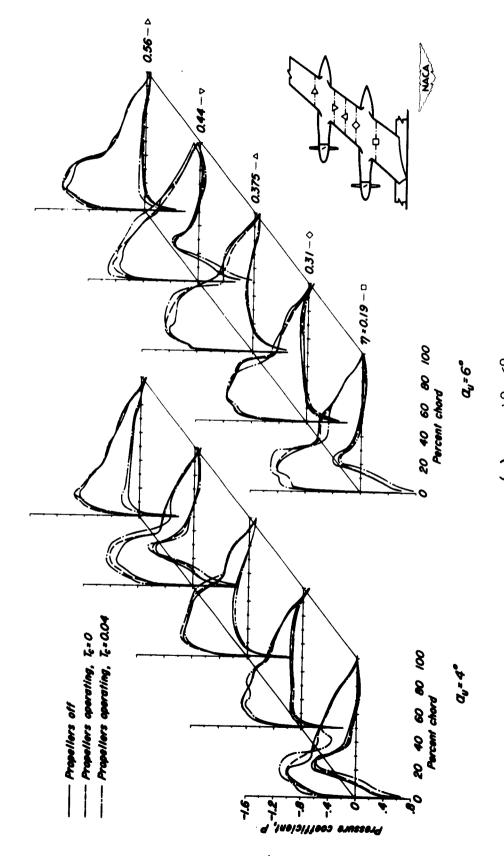
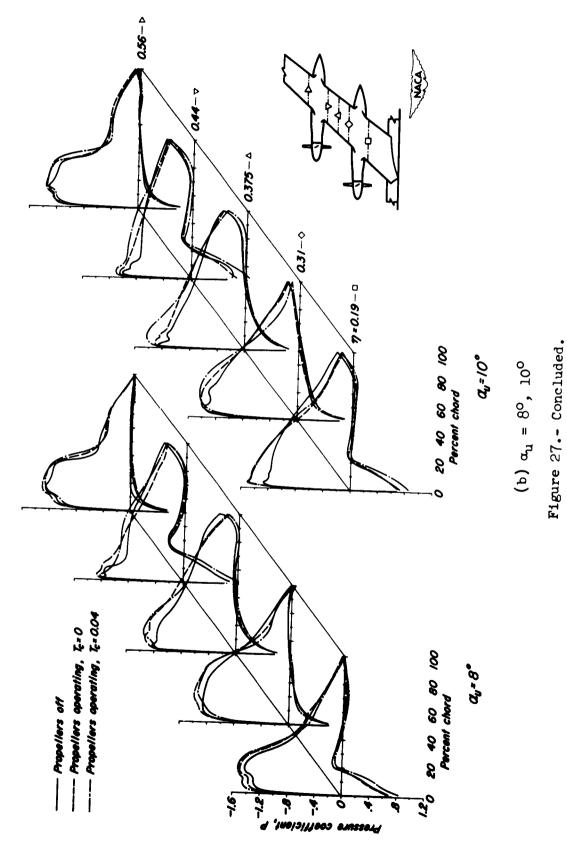


Figure 27.- The effect of thrust coefficient on the chordwise distributions of pressure coeffi-0.80, R = 1,000,000. II X cient at five semispan stations of the wing.

CONFIDENTIAL



CONFIDENTIAL

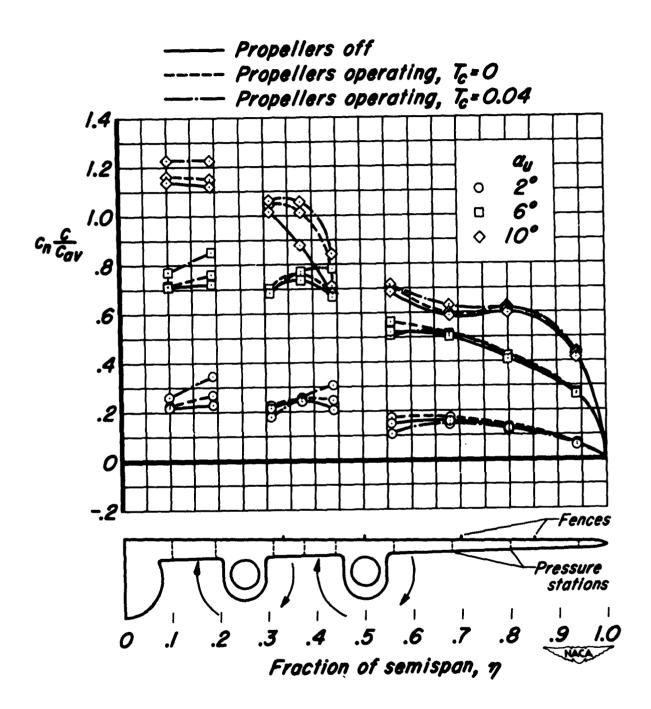


Figure 28.- The effect of thrust coefficient on the spanwise distribution of $c_n \frac{c}{c_{av}}$ for three angles of attack. M = 0.80, R = 1,000,000.

WING WITH 40° OF SWEEPBACK. Carl D. Kolbe and Frederick W. Boltz. April 1954. 133p. diagrs., photo., 19 tabs. (NACA RM A53L29) CONFIDENTIAL National Advisory Committee for Aeronautics. EFFECTS OF OPERATING PROPELLERS ON THE WING-SURFACE PRESSURES OF A FOUR-ENGINE TRACTOR AIRPLANE CONFIGURATION HAVING A VACA RM ASSL29

and the spanwise distribution of loading are presented for selected conditions. Comparative plots of the Measurements have been made to evaluate the effects engine tractor airplane configuration in the Ames 12foot pressure wind tunnel. Tabulated pressure data nine spanwise stations on the wing are presented for the model with the propellers operating and with operating propellers and of nacelles on the wingcoefficients, section pitching-moment coefficients, surface pressures on a semispan model of a four-The tests propellers removed. Section normal-force overall force data are also presented.

Copies obtainable from NACA, Washington

(over)

CONFIDENTIAL

NACA

CONFIDENTIAL

- (1.2.2.2.3)Flaps, Trailing-Edge -Wings, Complete Sweep
- (1.2.2.3.1)Mach Number Effects es;

photo., 19 tabs. (NACA RM A53L29) CONFIDENTIAL

and Frederick W. Boltz. April 1954. 133p. diagra.,

WING WITH 40° OF SWEEPBACK. Carl D. Kolbe

National Advisory Committee for Aeronautics.
EFFECTS OF OPERATING PROPELLERS ON THE WING-SURFACE PRESSURES OF A FOUR-ENGINE TRACTOR AIRPLANE CONFIGURATION HAVING A

NACA RM A531.29

Measurements have been made to evaluate the effects

operating propellers and of nacelles on the wing-

surface pressures on a semispan model of a four-

engine tractor airplane configuration in the Ames 12-

foot pressure wind tunnel. Tabulated pressure data nine spanwise stations on the wing are presented

for the model with the propellers operating and with

Š

Complete V'ings

- (1.2.2.6)Slipstream - Propellers Complete Wings
- (1.5.4) Wing-Fuselage Combi-÷ က်

nations - Airplanes

(1.7, 1.1, 1)(1.7.1.1.2)Wing-Nacelle Combinations - Airplanes &

and the spanwise distribution of loading are presented

or selected conditions. Comparative plots of the

overall force data are also presented.

Copies obtainable from NACA, Washington

4.5

The tests

coefficients, section pitching-moment coefficients,

the propellers removed. Section normal-force

over) CONFIDENTIAL

NACA RM A531.29

CONFIDENTIAL

and Frederick W. Boltz. April 1954. 133p. diagrs., photo., 19 tabs. (NACA RM A53L29) CONFIDENTIAL TRACTOR AIRPLANE CONFIGURATION HAVING A National Advisory Committee for Aeronautics. EFFECTS OF OPERATING PROPELLERS ON THE WING-SURFACE PRESSURES OF A FOUR-ENGINE WING WITH 40° OF SWEEPBACK. Carl D. Kolbe

(1.2.2.3.1)

Mach Number Effects -

m

Complete Wings

(1.2.2.6)

Slipstream - Propellers

÷ 'n

Wing-Fuselage Combi-

nations - Airplanes

(1.2.2.2.3)

Wings, Complete

_;

Sweep

Flaps, Trailing-Edge -

Complete Wings

Flaps, Trailing-Edge -

Sweep

Complete Wings

CONFIDENTIAL

Wings, Complete

(1.2.2.6)(1.5.4)

Mach Number Effects -

₩.

Complete Wings

Slipstream - Propellers

÷

Wing-Fuselage Combi-

Š

nations - Airplanes

and the spanwise distribution of loading are presented Measurements have been made to evaluate the effects engine tractor airplane configuration in the Ames 12foot pressure wind tunnel. Tabulated pressure data for nine spanwise stations on the wing are presented for the model with the propellers operating and with of operating propellers and of nacelles on the wingsurface pressures on a semispan model of a fourcoefficients, section pitching-moment coefficients, for selected conditions. Comparative plots of the overall force data are also presented. The tests the propellers removed. Section normal-force

(1.7.1.1.1)

Wing-Nacelle Combina-

ø.

tions - Airplanes

(1.7.1.1.2)

(over)

Copies obtainable from NACA, Washington

CONFIDENTIAL MACA

(over)

(over)

(1.7.1.1.2)

Wing-Nacelle Combina-

9

tions - Airplanes

NACA RM A531.29

WING WITH 40° OF SWEEPBACK. Carl D. Kolbe and Frederick W. Boltz. April 1954. 133p. diagrs., photo., 19 tabs. (NACA RM A53L29) CONFIDENTIAL TRACTOR AIRPLANE CONFIGURATION HAVING A WING-SURFACE PRESSURES OF A FOUR-ENGINE EFFECTS OF OPERATING PROPELLERS ON THE National Advisory Committee for Aeronautics.

and the spanwise distribution of loading are presented Measurements have been made to evaluate the effects engine tractor airplane configuration in the Ames 12foot pressure wind tunnel. Tabulated pressure data for nine spanwise stations on the wing are presented of operating propellers and of nacelles on the wingfor the model with the propellers operating and with coefficients, section pitching-moment coefficients, surface pressures on a semispan model of a fouror selected conditions. Comparative plots of the The tests the propellers removed. Section normal-force overall force data are also presented.

Copies obtainable from NACA, Washington

CONFIDENTIAL

- (1.2.2.2.3)Wings, Complete -Sweep
 - Flaps, Trailing-Edge -Complete Wings ~
- (1.2, 2.3, 1)Mach Number Effects -က်
 - (1.2.2.6)Complete Wings
 - Slipstream Propellers ÷
- (1.7.1.1.1)Wing-Fuselage Combinations - Airplanes 'n.
 - (1.7.1.1.2)Wing-Nacelle Combinations - Airplanes œ.

(over) CONFIDENTIAL NACA A

and a range of thrust coefficients (up to 0.8 per propeller) at Mach numbers from 0.082 to 0.90 for were conducted through a range of angles of attack Reynolds numbers ranging from 1,000,000 to 8,000,000.

Loads, Steady - Wings CONFIDENTIAL

(4.1.1.1)Frederick W. NACA RM A53L29 Carl D. Kolbe, Boltz, 그러분

8,000,000.

NACA RM A53L29

and a range of thrust coefficients (up to 0.8 per propeller) at Mach numbers from 0.082 to 0.90 for were conducted through a range of angles of attack Reynolds numbers ranging from 1,000,000 to

CONFIDENTIAL

 $\{4, 1, 1, 1, 1\}$ Loads, Steady - Wings

Boltz, Frederick W. Kolbe, Carl D.

NACA RM A53L29 ۲.

Copies obtainable from NACA, Washington

NACA RM ASSL29

and a range of thrust coefficients (up to 0.8 per propeller) at Mach numbers from 0.062 to 0.90 for were conducted through a range of angles of attack Reynolds numbers ranging from 1,000,000 to 8,000,000

CONFIDENTIAL

CONFIDENTIAL

(4.1.1.1) Loads, Steady - Wings

Boltz, Frederick W. NACA RM A53L29 Kolbe, Carl D. 그러럼

NACA RM A53L29

Copies obtainable from NACA, Washington

and a range of thrust coefficients (up to 0.8 per propeller) at Mach numbers from 0.082 to 0.90 for were conducted through a range of angles of attack Reynolds numbers ranging from 1,000, 003 to 8,000,000.

CONFIDENTIAL

CONFIDENTIAL

(4.1.1.1)Loads, Steady - Wings

۲.

Boltz, Frederick W. NACA RM A53L29 Kolbe, Carl D. 그리텀

> Copies obtainable from NACA, Washington CONFIDENTIAL

CONFIDENTIAL

Copies obtainable from NACA, Washington